



ONE of the most interesting items of news during the month concerns the waning popularity of color TV in the United States.

As far as I know, color TV does not exist anywhere else except experimentally. But I cannot imagine a better place to try it out commercially than in America, with its avid acceptance of new things and its rapid reaction to them.

The history of color TV is very closely bound up with the activities of the Radio Corporation of America, and its colossal effort to achieve this modern

miracle. Even when the FCC gave its premature blessing to the CBS color-wheel system some years ago, RCA merely dug in its heels and reiterated its faith in the electronic method. By doing ten years work in two it produced a tri-color picture tube, now considered to be the only satisfactory color medium in sight.

It has announced its intention to persevere, "going it alone" if need be until the proposition becomes a practicable one.

In the face of this confidence, and the vitality behind it, lack of public acceptance is a poser.

The only obvious explanation seems to be that color is here before we are ready for it.

I believe quite firmly that eventually every form of picture presentation must include not only color but 3-D as well. John Logie Baird expressed this view to me nearly 20 years ago, when TV was a crude thing. He said that eventually TV would be displayed in color and full stereoscopic presentation. That's the way we see things in real life.

In a recent lecture in Sydney, Mr. J. E. Benson, one of our leading TV engineers, compared the achievement of color TV with that of the atom-bomb as one of the most amazing developments of modern times.

Perhaps this is the clue. It is amazing, and it is at least three times as expensive as the normal system. Maybe it is too early for the public to pay more for a better system, when the initial impact of the cheaper and easier method has not been absorbed.

The efforts of RCA may have brought us color TV before its time. A simpler method may be essential before it finds full acceptance. But no matter how long delayed, some day it will come.

John Boyle

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A NATIONAL MAGAZINE OF RADIO, TELEVISION, HOBBIES AND POPULAR SCIENCE

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OUR COVER PICTURE—

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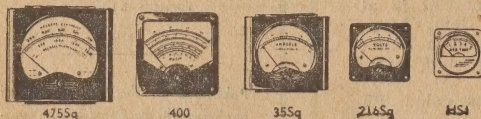
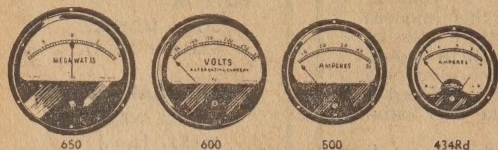
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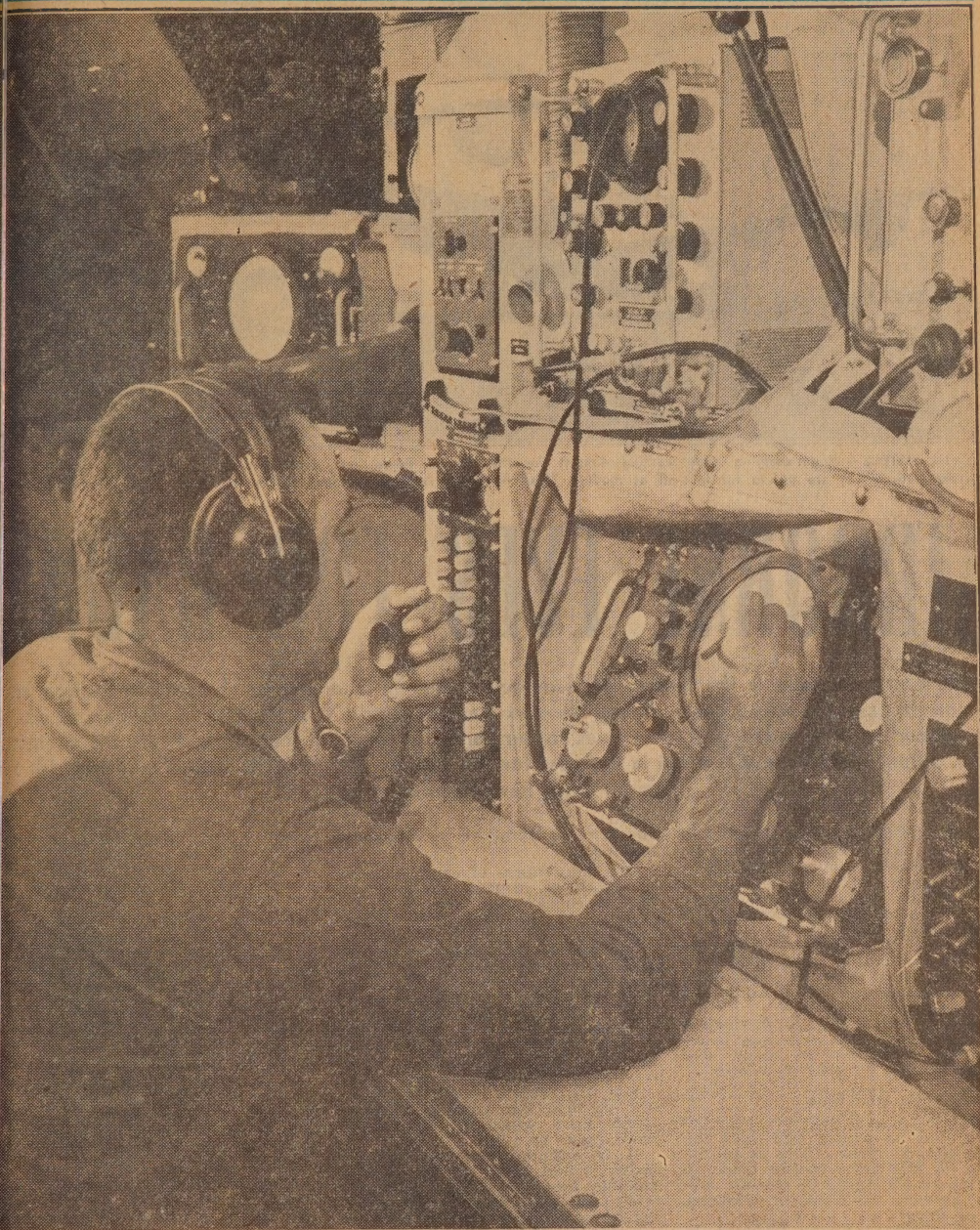
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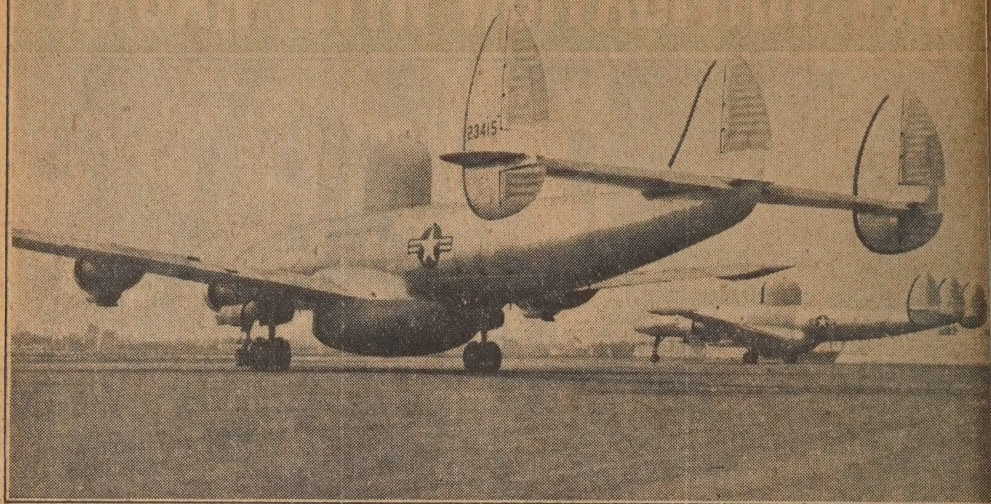
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SKY NAVIGATION WITH RADAR



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TWIN SISTERS—Radar-carrying early warning aircraft for the U.S. Air Force (left, designated RC-121) and U.S. Navy (right, designated WV-2) are poised for take-off as modern "Paul Revere" versions of the well-known civil Super Constellation.

AIRBORNE EYES FOR RADAR

The story of radar is the history of a miracle in human ingenuity which came to fruition in time to save the Allied cause during the dark days of World War II. Born in silence and developed in utter secrecy, it gave eyes to our forces. It enabled them to frustrate the enemy in defence and to seek him out in darkness for the attack. Without its help, the British Isles might easily have been overcome.

ALTHOUGH the secrets of radar in those early days is a secret no longer, modern equipment has reached a unique peak of perfection not only in the design and manufacture of the radar sets themselves, but their tactical employment.

Much of this employment has no direct relationship with war, unless the safety of aircraft and ships at sea can be considered as always having a bearing on war.

Today, radar aids to navigation are commonplace in both these fields. Suitable equipment is made and manufactured all over the world.

ESSENTIAL DEFENCE

But a nation's defences must be developed no matter how rosy the international scene. This is inevitable, as the giant strides made in the speed and range of aircraft, and the potency of modern weapons, races ahead.

Radar was initially designed to provide early warning of air raids when it was realised that the first attack in modern war would come from the air. Despite the many other uses for it, this early warning has remained a first requirement. The demands on the speed and ac-

curacy of its work have never ceased to grow.

The importance of early warning of attack is, in fact, so important that it could easily win or lose a war by its effectiveness or otherwise.

The terrific destruction made possible by weapons such as the hydrogen bomb could easily mean that, if an enemy were permitted to strike a first effective blow, there might be little left for us to defend. Or, at best, industry and society could be so frightfully crippled as to make retaliation ineffective or impossible.

For this reason, speed and range are perhaps the primary requirements upon which a modern defence radar is built.

It is essential that the defence forces should know at the earliest possible moment of an imminent attack, the position of the threatening forces and the direction of their movement. Only then can be planned the best possible deployment of countermeasures to render the attack impotent at the earliest possible moment, and at the greatest distance from our shores.

To this end, every refinement of radar and allied techniques are as-

sembled and co-ordinated, and the information they supply integrated to give the necessary answers with complete accuracy immediately they are obtained.

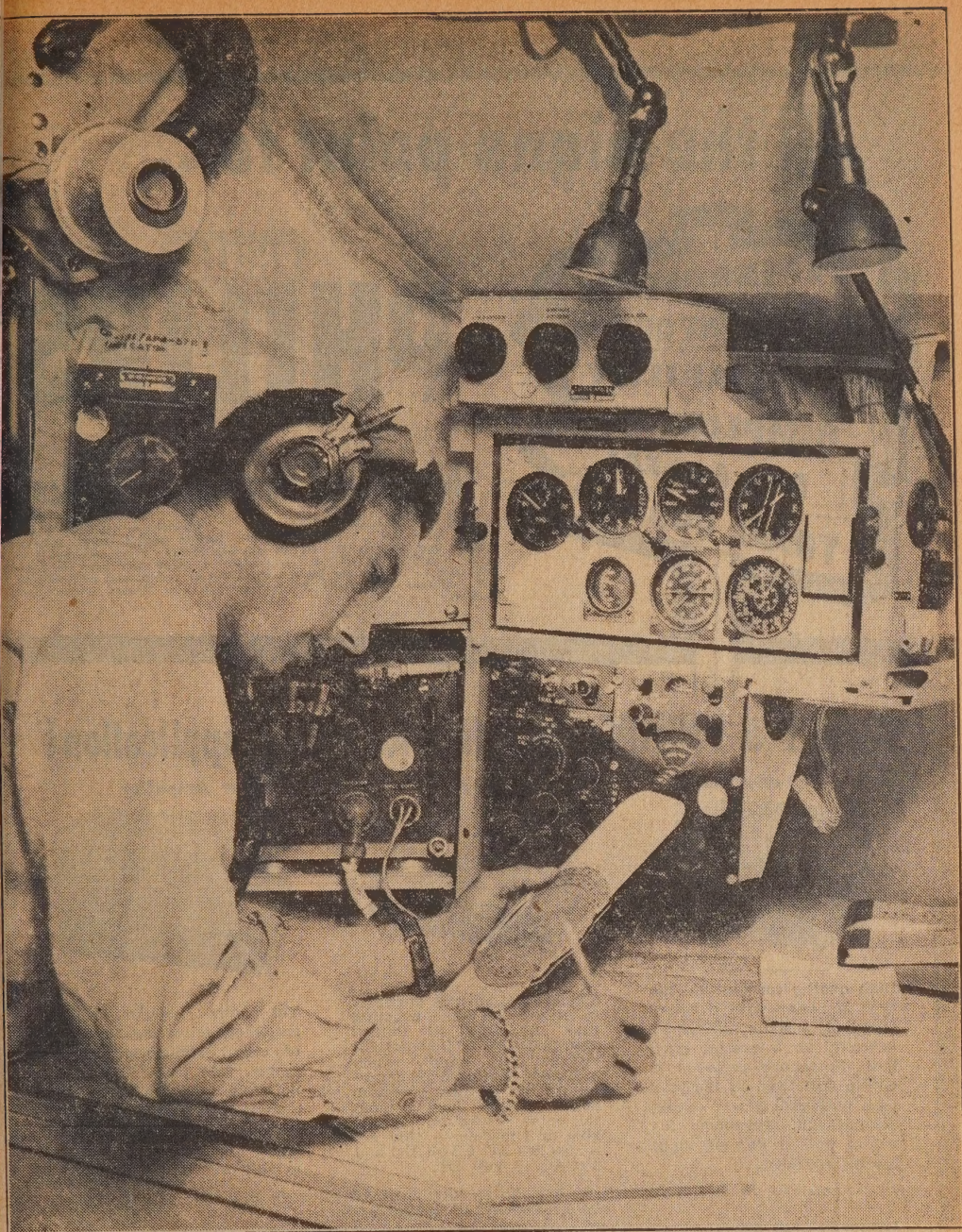
Even at the end of the last war this principle was recognised in the development of radar stations which were virtually a nest of many equipments, each designed to do its own particular job of range-finding, height-finding, speed estimation and so on.

RESULTS COMPUTED

From these equipments, information in the form of electrical signals was fed into a system of computers, which co-ordinated and digested them much more readily than could be done by human means.

One great installation of this type was able to set up an electronic eye which could literally see the movement of any object over a distance of hundreds of miles. Several of them acting in concert were sufficient to give ample warning for defence forces to take appropriate action.

Only last month it was announced that Sydney was being given a radar



HENRY THE NAVIGATOR SKY-STYLE—Where were we at when we saw what we see? This man makes a running plot of radar plane's position throughout the entire flight in order to provide C.I.C. (Combat Information Centre) officers with quick reference points in intelligence reports to command posts and operating units in the area.

centre for defence which would cost £1-million.

But, during the last ten years, the picture has changed, and the greatest change has been in the matter of speed.

Early warning is measured in time,

and time in its turn is important only in terms of the enemy's ability to get from its base to the target.

If since World War II aircraft speeds have increased three times, then the usefulness of the period of warning has been reduced by two-

thirds of its original amount. Other factors have probably decreased the safety margin even further, so that the urge to increase the range and accuracy of the warning system is very great.

The main restriction on radar

All the signs point to...

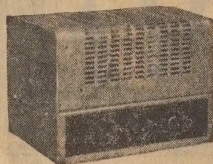


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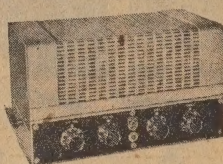
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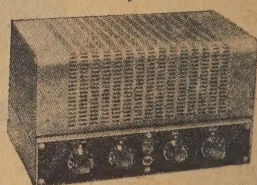
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age is the so-called "line-of-sight" effect, which in general limits the radar beams to little more than the distant horizon.

Siting the early warning stations on high ground, and even on mountain tops near the shore, is a great help. The big problem is to extend the line of electronic vision further than that of the land based stations. One solution which is now being taken into practice in America is to equip large aircraft with an elaborate radar system, which can do virtually the same work as the stations on land.

If these aircraft are sent out at great height, they can extend radar range by a double amount. They can look backward over hundreds of miles to the parent station on shore, and at the same time search ahead for possible targets by an equal distance, reaching to the limits of their own greatly extended horizon.

Technically, the task is not difficult, but the work of designing and installing equipment suitable and light enough to fit into even the large aircraft now being built, is not easy.

The aircraft selected for the project, six Lockheed Super-Constellations, are each required to carry six tons of electronic gear, in addition to an operating crew of 31 trained men.

CONSTANT WATCH

This crew is designed to keep a round-the-clock watch. The aircraft is sent back to base all the information they can gather about possible intruders, weather conditions and so on, and receive co-ordinating instructions from the base and from other stations in the defence network.

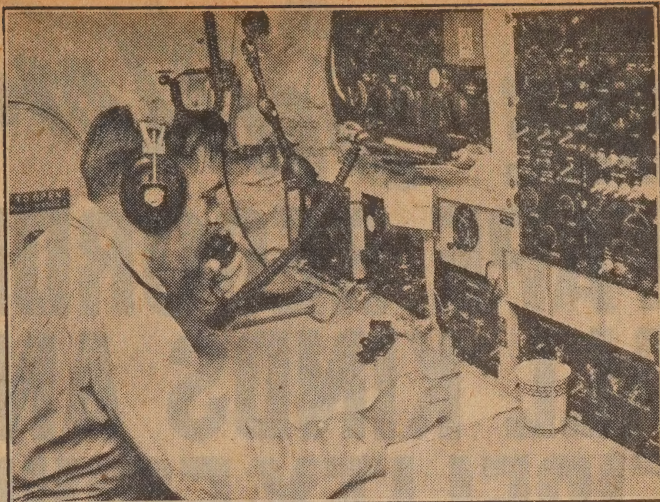
In their sentry work, they are assisted by other units, some of them naval vessels, and some of them other aircraft. They are distinguished by special, range-extending wing-fuel tanks, and strange, streamlined protuberances which carry the microwave directional aerials.

All this can only be done through the highest degree of training and operating skill by the men who man this miracle load of electronic magic, much of which is among the nation's best guarded secrets.

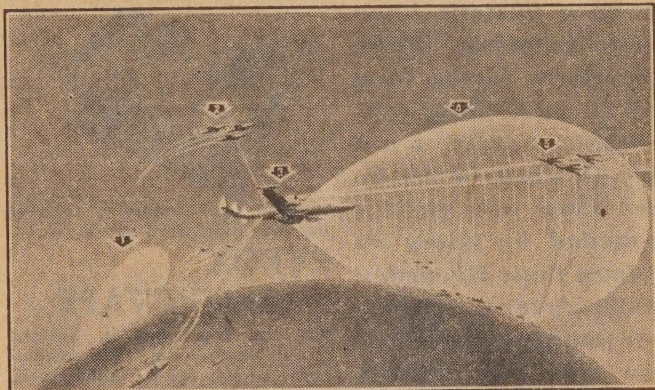
The pictures on these pages give some idea of the magnitude of the project, the complexity of the gear, and the conditions under which the operators and crew must work. They also show graphically how the airborne radar eyes keep their watch, and play their part in guarding the safety of those who sleep at home.

AIR FORCE SENTRY OPERATION —

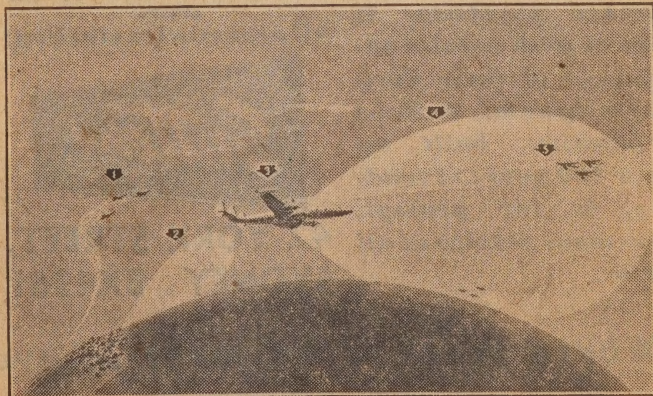
Artist's concept of big radar picket plane in operation shows (1) defending fighters arising to the early-warning call of USAF RC-121; (2) ground radar, limited by horizon, in full operation to pick up any invaders that might penetrate the outer net; (3) radar Super Constellation sentry at altitude which permits peeking over the horizon; (4) huge search area covered by the powerful radar installed beneath the fuselage; (5) height-finder radar operating from the uppermost dome on the airplane.



VITAL LINK — Chief Aviation Electronics Technician T. R. McConnell, USN, tests radio equipment and establishes communication with remote commands in order to flash alert to carriers, bases and fighter airplanes over a wide area. Defensive measures are geared to swing into action within seconds from alert.

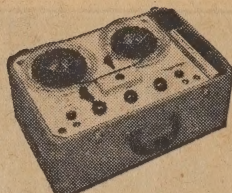


BECAUSE THE WORLD IS ROUND — Artist's conception of radar sentry airplane in operation shows (1) ground radar limited by line-of-sight restrictions; (2) defending fighters moving to intercept invaders; (3) radar-carrying Super Constellation; (4) big sweep area covered by radar located in the saucer-like bulge beneath the airplane, with the aircraft's altitude permitting the radar to peek over the horizon; (5) "invading planes" pinpointed in beam of the radar located in the "shark's fin" on top of the search plane.



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THE FLYING DECKCHAIR STORY

the long, straight stretch of the German Autobahn between Munich and Ingolstadt, 22 world speed records were broken by a new type motor cycle, driven by Gustav Baum. Thirteen days later, April of this year, the machine crashed, killing its designer and writing finishing its designer and writing finishing a thrilling account of determination and success.

THIS is the story of the fantastic "Flying Deckchair", why and how it was designed and built, and the events which led up to its heroic and eventually tragic career.

It is not without reason that all civilized countries have brought down legislation controlling and restricting motor traffic to flow smoothly over the highways. One cannot disregard the life and property of other people, just "to get there fast". Such legislation does not, however, exclude the possibility of arranging speed trials. Record-breaking attempts on certain sections of the road, must be made at certain predetermined times, when they are not likely to interfere with the regular traffic.

MORE THAN COMPARISON

These trials are much more than just a comparison between vehicles of different horsepower, or the skill of the drivers. They are also a rough proving ground for motors, brakes and construction.

Just as there are scientists, who are willing to take the risk of death, testing new preparations and medicines on themselves, there always will be designers and drivers of motor vehicles willing to give their lives to prove the practicability of their designs, or to break records. And nobody can forbid them to do so, provided they do not endanger the lives or safety of others.

Gustav Adolf Baum, a young draftsman, wanted to improve the performance of light motor cycles. So he would do without increasing the motor capacity, by lying the rider flat on his back on his cycle, and providing a streamlined enclosure for both.

NOT NEW

In itself this was not a new or revolutionary idea. As far back as 1939, there was talk about a "racing cigar", designed by one, Koenig-Fachsenfeld, who claimed excellent results from his experiments. Among other things, an air resistance value of only .12 was measured in his models.

Air resistance is one of the most important factors in the design of high speed vehicles.

Resistance values for any particular vehicle depend on the form, surface, and speed of vehicles. As a basis of comparison, an air resistance value, C_w , of approximately .8, is given for old style cars with high superstructure. Modern cars, with streamlined, low bodies, bring



Easily lifted by a man, the Flying Deckchair, as it is popularly known, is shown with its designer-rider, Gustav Adolf Baum. From this picture it is not hard to visualize, that the streamlined form has characteristics similar to modern aeroplane bodies.

this figure down to about .5 to .4.

The Volkswagen, now a familiar sight on Australian roads, has an air resistance value of .25, when fully closed up.

A very low and long, Italian car, in which the driver had to lay flat with his head forward, reached an all time low of .14.

Baum, who joined the NSU motor works in 1951, proved to have constructional ability far above average in designing vehicles of the lowest possible air resistance.

The first tentative experiments

along these lines were carried out about twenty years ago. Without increasing the available power, promising results were obtained in the streamlining of motor cycle bodies.

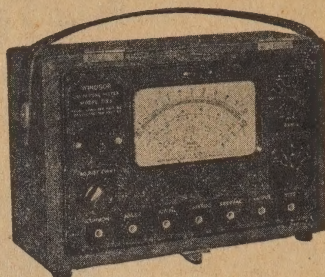
Eighty per cent of the motor power is usually absorbed by air resistance on motor cycles. This power is wasted, and it took many years to recover these losses by streamlining not only the motor cycle itself, but also the driver. He became a built-in part of his cycle.

It goes without saying that air resistance was not the only difficulty



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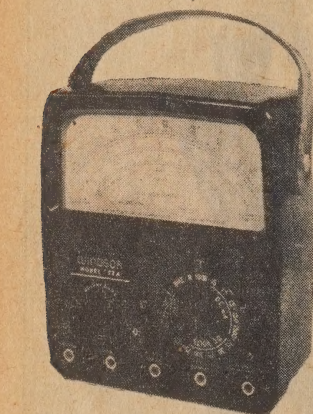
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D.C. Amps: 0—2.5—10.

A.C. Amps: 0—2.5—10.

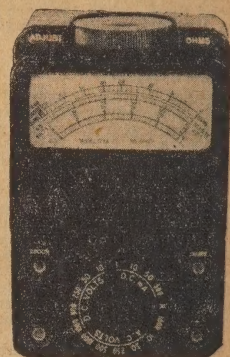
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Ranges:

D.C. volts: 7 ranges from .25—2500 v.

A.C. Volts: 6 ranges from 10—2500 v.

D.C. mA: 4 ranges from 1—500.

Resistance: 0—2000 ohms, 0—200,000 ohms (can be extended to 20 megohms).

Meter: accurate moving coil with 23 scales.

Price: £14/17/6 (Plus tax)

confronted designers. Motors also had to be improved give more power for the same cylinder size.

On the basis of these experiments, Germany broke world records in 1939. Soon afterward, Italy, with fully or wholly streamlined machines, pushed the speed limits still higher. During the last few years, only attempts to break the record have been made with completely enclosing both machine and rider in streamlined capsules.

Motor cycle design has immensely benefited from result of these record-breaking attempts.

When, in April, 1954, NSU succeeded in equalling and breaking several world records, the motor cycle industry began to get interested in this peculiar-looking, but nevertheless sound design of Baumm's.

Its air resistance is less than .1, which comes very close to values achieved in present-day aircraft construction.

NO DIFFERENT MODELS

Two different models were built, one with a 50 cc engine, and the other with a 125 cc engine. Total length was 12ft, with a wheelbase of 7ft. Overall width given as 21 and 23in and height 22 and 24in for the 50 and 125 cc models respectively. Unladen weight for the two models is 160 and 240lb.

Such small weights could, of course, only be achieved by self-supporting aircraft-skin construction.

Baumm had to overcome many difficulties. But, although his first designs were rejected in 1951, he worked

He would not accept the apparent fact that a rider had to sit on his motor cycle, as if it were a horse.

His first experiments were carried out on an ironing board and a rudimentary frame with two wheels, which demonstrated that the idea of laying the rider on his back was definitely practicable. Further experiments followed, and in March, 1953, he built his first record-breaking motor cycle.

The trial runs were much better than expected. In the following year Baumm broke three records in the 50 cc class, and two in the 125 cc class on another machine built subsequently. In several instances he doubled existing record speed.

These records were obtained over short stretches from a flying start. However, they were sufficiently good to arouse interest all over the world.

HOTTED UP"

Needless to say, motors were very much "hotted up" for the trials. Nevertheless, the total power available from the 49 cc motor was only 3.4 hp at 7000 rpm, and 7.2 hp from the 98 cc motor.

For the speed records this year, the available power was increased to 4.7 hp at 7800 rpm on the smallest motor. The special racing 125 cc motor delivered 16.5 hp at 11,500 rpm.

One hundred pc alcohol and 80-octane petrol were used respectively, and this, together with improved motors and streamlined body, enabled a maximum speed of 136 mph to be reached.

On May 23, 1955, the machine crashed while on trial run on the Nurburgring, famous German racing circuit. Baumm, who always rode the "Flying Deck-chair", as it was popularly known, was killed in the crash.

His death was a great loss to research, and the practical application of engineering design in his own field. As with so many other intrepid, fearless men, he paid the price for knowledge which can only be obtained by testing the limits of achievement.—Orion.

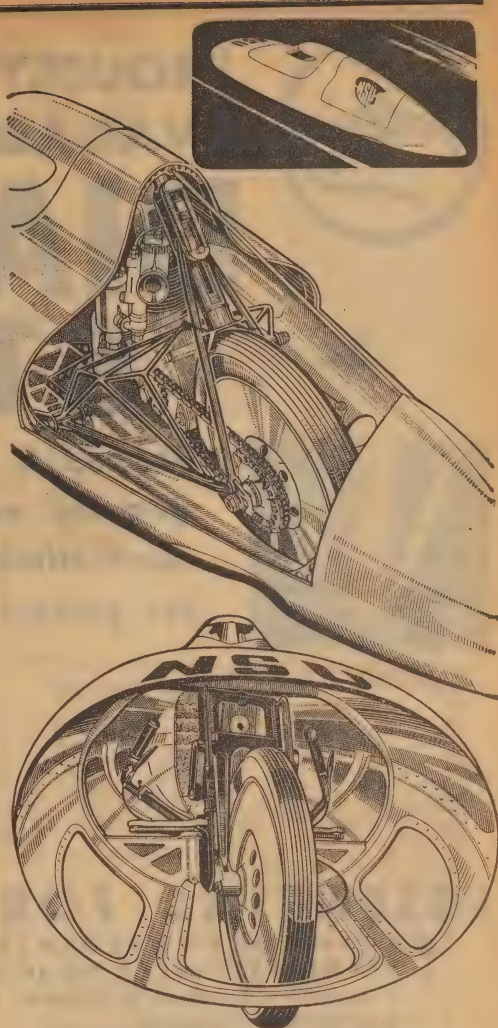
Sunlight into Electricity

SOME time ago it was reported that the Bell Telephone Co. has succeeded in producing sun powered batteries, which are strong enough to supply telephone repeater stations in remote areas, where conventional power supplies are not available or not practicable.

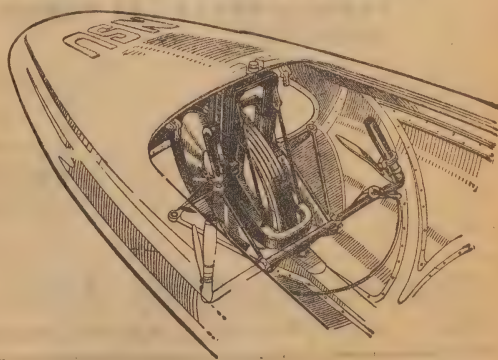
Technical details of their manufacture have now been released by the company.

For single cells, a solid single crystal of silicon is cut and polished with optical precision. Subsequently it is exposed, in high vacuum, to ionic bombardment with ions of 300eKV energy, at a temperature of 390 degrees C.

Subsequently, the polished crystal is coated with a .00025 mm thick layer of boron. So far, cells of 10 x 50 x .1 mm size have been manufactured. One square yard of cell area supplies approximately 50 watts of power, sufficient to run repeater stations or small transmitters.



Detail drawing shows the motor and drive (top), the front fork (centre) and the steering gear (below). The body is a self-supporting tubular "skin", on which are mounted the front and rear forks.





PROUDLY ANNOUNCE AVAILABILITY of THEIR NEW **DIAMOND STYLUS**

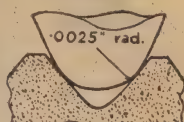


DIAMOND STYLUS
after
1000 PLAYINGS

Micro-photograph shows entire absence of wear and perfect contour after 1000 playings on "78" shellac discs.

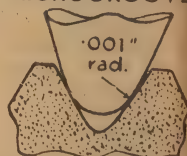
Shaped & polished by hand from genuine natural diamonds to the exact dimensions essential for perfect reproduction!

STANDARD



Goldring Diamond Styli ride correctly on the sides of the groove. Inaccurate needles will either ride on the bottom of the groove, causing undue noise and loss of reproduction quality, or will skate across the record.

MICROGROOVE



ESSENTIAL FOR HIGH FIDELITY

- ★ **CANNOT BE FRACTURED IN USE.**
- ★ **UNCONDITIONALLY GUARANTEED for 6 months against fracture, chipping or accidental damage.**
- ★ **NO RECORD DAMAGE due to worn or deteriorating styli.**
- ★ **NO FREQUENT STYLUS CHANGING.**
- ★ **MORE ECONOMICAL THAN ANY OTHER TYPE of STYLUS IN TERMS of RECORD "MILEAGE".**

Now, with the sensational Goldring Diamond Stylus, you can enjoy better reproduction all the time. No danger of accidental chipping—the genuine diamond point is the hardest substance known. The polished Goldring "Ball Point" glides through the grooves, with perfect compliance and frictionless, non-wearing, noise-free smoothness... an investment in musical enjoyment, an insurance policy for your records!

RETAIL PRICE £6/10/- (Standard or microgroove)

The following diamond styli (standard and microgroove sizes) are now available:

D/7—D/8—D/9—D/16—D/17—D/20—D/24

For special types of cartridges not listed in the Stylus Reference Chart—Connoisseur Decca, Dual, etc.—send the complete cartridge (or armature, stylus holder or stylus—whichever is applicable) to Goldring Engineering for fitting. Fitting and delivery will be effected in 6-8 weeks.

If Goldring Diamond Styli are not obtainable from your usual retailer, contact the Australian Distributors, to whom trade inquiries should also be addressed.

Goldring Engineering (Aust.) Pty. Ltd.

57 H.E. AREA, ST. MARYS, N.S.W. Phone B0701 Ext. 447

HOW THE GOLDRING DIAMOND STYLUS PROTECTS YOUR RECORDS



All other softer types of styli eventually wear to chisel edges which gouge records and distort tone quality.

Polished Goldring Diamond Point protects grooves, extracts the full recorded frequency range.



ORDER THE CORRECT STYLUS

Fill in this coupon, and take to your retailer. If he has not the correct stylus in stock, ask him to obtain it for you.
MAKE of RECORD CHANGER, MOTOR-PICKUP UNIT, or PICKUP

Model or type No. _____
State whether Microgroove or "78" stylus (or both) are required _____
Refer to Goldring Stylus Chart on the following pages for assistance in selecting the correct type of stylus.

X-RAY SHOWS ENGINE IN MOTION

Announcement of a system for "x-ray televising" the internal parts of an operating engine, was among the highlights of an Open House held at the National Bureau of Standards earlier this year. Dr. A. V. Astin, director of the bureau, explained the operation of this new scientific wonder.

DR. ASTIN illustrated NBS work in the x-ray range of the spectrum with demonstrations of the radiation monitor and the system for x-ray televising the interior of an engine.

The radiation monitor is a remote-control system which automatically measures radiation intensities in the vicinity of an atomic explosion and transmits the data by radio to a centrally located headquarters.

The system was developed at the request of the Division of Biology and Medicine of the Atomic Energy Commission for use in nuclear tests.

Its overall design was worked out by L. Costrell and associates of the bureau's nucleonic instrumentation laboratory. As Dr. Astin explained the operation of the monitor, it received and recorded the background radioactivity level at a remote station near Reno, Nevada.

PENETRATING RAY

The x-ray televising demonstration used highly penetrating radiation from the beatron in combination with a technique recently developed at the bureau for converting high-energy x-rays into visual images.

The audience saw clearly the moving piston, piston rod, and other parts in a televised x-ray image of a small one-cylinder engine.

By means of this technique it should be possible to televise the internal operation of a wide range of mechanisms, such as automotive and aircraft engines, pumps, and other devices.

Because of their greater penetrating power and lower scattering, high-energy x-rays from betatrons and synchrotrons produce sharper images than do lower-energy x-rays, allowing the observation of greater detail and the detection of more minute flaws in metallic equipment.

However, until now their use in studying the internal operation of heavy machinery has been confined largely to x-ray photographs. Suitable methods for observing the interior of a mechanism while it operates have been lacking.

The bureau's system, developed by Dr. J. S. Pruitt of the NBS Betatron Laboratory, makes use of an instrument called a pattern amplifier, which acts as an x-ray intensifier, continuously detecting, amplifying and displaying low-intensity x-ray images.

The major component of the pattern amplifier is the converter—a large, cylindrical, thallium-activated sodium iodide crystal, which converts x-ray images into optical images.

When bombarded with an x-ray
(Continued on Page 119)

BATTERY OPERATED RADIOGRAM

The 7-inch 45 rpm records which are now well established have many advantages over their 78 rpm counterparts. Not only do they give more music from a smaller disc, but they are extremely light in weight. Being flexible, they will not fracture as easily as the older types.

Right — The battery operated radiogram which plays only 45 rpm records, using a motor with a power consumption of only 80 milliwatts.

WHEN considering a portable gramophone or radiogram these records would be an immediate choice.

But three-speed spring motors are a rarity and the normal electrically-driven turntables would require far more power than could be supplied from batteries.

If, however, the turntable was to be used only for 45 rpm records its physical dimensions could be reduced and general efficiency greatly improved. Using a miniature motor with a permanent magnetic field the turntable could then be driven economically from dry batteries.

This technique was used in what is claimed to be the first commercially produced portable record player-receiver combination.

Braun, of Germany, now features a four-valve portable with built-in 45 rpm record player.

The set, a conventional receiver with ferrite aerial and bandpass filter, is contained in a plastic cabinet, which also houses the record player and provides storage room for six records in the lid. The cabinet is no



bigger than the average portable receiver.

Besides the usual A and B batteries three baby torch cells are provided for the motor, which, incidentally, has a power consumption of only 80 milliwatts, less than the smallest torch bulb. A life of approximately 500 playings is claimed for these batteries.

AC operation, with a dry rectifier, is provided for at the touch of a button. The function switch consists of five buttons on the front of the receiver.

Special battery-saving features are built into the Braun Combl. Thus the turntable cannot be operated while the receiver is switched on. When the turntable is used the converter and IF filaments are extinguished, reducing the drain on both the A and B batteries.



X-ray image of a single-cylinder compressor as seen on the television screen. Note the piston and piston rod above and the crankcase below.

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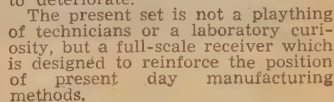
ROLA COMPANY (AUST.) PTY. LTD
THE BOULEVARD, RICHMOND, VIC. JB 3921. 116 CLARENCE STREET, SYDNEY, N.S.W. BX 399

First all-transistor receiver to go into full-scale commercial production is the American "Regency" personal portable, pictured on this page. Details of the set were published recently in the French magazine TSF et TV. We quote:—

It is interesting to note the base connection of the second IF ampli-



A 22½ V battery such as used in flashlights and hearing aids provides the operating power for the Regency receiver. It must be mentioned that although transistors will oper-



by Calvin
Walter



What of the average politician? He is often 100 pc air—but don't let's complicate things any more. Highly intelligent people like those who take the trouble to read what I write are a little more highly organised. I include even the editing in these remarks, even though I do get on my back occasionally for not putting in the commas, or putting them in the wrong place; or I haven't put any in this paragraph so we will see what sort of a job it makes of it himself unless he cuts this paragraph out altogether and make it easier.

As I said, we are a little more highly organised, for our bodies contain—aside from water, fat, protein and so on—many chemical elements. These are as follows:

Calcium, phosphorus, potassium, sulphur, chlorine, sodium, magnesium, iron, manganese, iodine, cobalt, silicon, aluminium, arsenic, boron, copper, fluorine, nickel, zinc.

ESSENTIAL ELEMENTS

Some of these are very important and essential to life while others are more or less superfluous and are only there by accident.

The first ten, from calcium to iodine inclusive, are found in and enter into the contents of the cells and fluids of the body. They exist in the body in comparatively large amounts.

For instance, an adult man contains about $2\frac{1}{2}$ pounds of calcium, $1\frac{1}{2}$ pounds of phosphorus, half

Things are not always what they seem. Both the muscular he-man and the bathing belles in this picture are made of a few shillings worth of chemicals mixed with some gallons of water.

LIFE HANGS ON SMALL THINGS

Among the many substances required to sustain life whether human, animal or vegetable there are minerals which are needed only in minute traces. Without them men would die, plants would wither, and growth would be impossible.

IT has been said that man is about 90 pc water. It has also been said that man is what he eats.

Both these statements have been made by eminent dietitians, but they seem a little contradictory.

Take the first. If this is true then the second cannot be, for how can a man be water if he doesn't drink it. According to the second statement some men should be 90 pc beer and

ten pc water, the latter being what's in his beer.

If the second statement is true, the first cannot be, for if one is observant during the day, one will soon see that the average typist should be cake or lolly, and the average man should be meat pie or tea or chewing gum, and the highly strung executive should be ulcer tablets or sodium bi-carbonate.

pound of potassium, five ounces of sulphur, three ounces of chlorine and sodium, down the list to a fraction of an ounce of iodine.

At this stage we will have to introduce a change of measurement and work in grammes. In round figures a gramme is about one-thirtieth of an ounce. We will also require to use the milligramme which is one-thousandth of an ounce.

amme and the microgramme, which is one-millionth of a gramme. A milligramme is, therefore, one thousandth of one-thirty-second of an ounce and the microgramme is one-millionth of one-thirty-second of an ounce.

Both these weights are extremely small and are given in this rough manner merely to give some idea to readers when reading what is to follow.

The elements from cobalt to zinc inclusive are found in the body only in traces. In addition to these there are elements which are needed in traces for the development of plant life. These include vanadium and molybdenum.

The trace elements as they are called seem to act as catalysts in the development of chemical reactions within the living matter.

In the blood, for instance, the iron stored in the liver cannot be converted into haemoglobin unless traces of copper are present.

COPPER

The copper in the system exists as a copper-protein compound and in the liver the copper content is about five parts per million.

It has been estimated that the normal daily requirement of copper intake for an adult is one to two milligrammes. Deficiency of copper in the diet can be responsible for anaemia.

Copper is derived from milk, butter, cheese, refined sugar, honey, margarine, lard and suet, in quantities up to five parts per million. The most prolific sources are oysters with up to 400 parts per million. Lambs and calves' liver is also good, with up to 100 parts per million, yeast up to 100 parts per million, and cocoa-shell up to 200 ppm.

Copper is available in most fruits and vegetables, table salt, wholemeal flour and oatmeal and a host of other daily foods, so that there is little chance of at least some copper being unavailable for the average eater.

Zinc has a definite function in the human body, particularly in the transport of carbon dioxide by the blood. The average daily zinc requirement is about 8 milligrammes. It is also a necessary element for the formation of hard shells of hen eggs, a deficiency leading to soft shell eggs.

ZINC

Zinc is an important element in the production of insulin. Several investigators have found that the pancreas of a diabetic patient contains about half the zinc of a normal person. In the manufacture of insulin it has been found that the addition of minute traces of zinc prolongs the beneficial action of the insulin.

In agriculture zinc is an important element of the soil where it is present in fertile soils in amounts of only about three p.p.m. (parts per million). A deficiency leads to various diseases such as mottle leaf disease, chlorosis and so on.

Zinc is available in most everyday food, particularly wheat germ, oysters, egg-yolk, peas, beans, coffee, rabbit, beef liver, rice, onions, &c. It is very widely distributed and

YOUR PHONE BILL BY CAMERA



The new "Villette" telephone exchange uses a camera to photograph telephone subscribers meters in banks of 25. Mistakes are avoided and a record kept. The camera is fitted with mercury lamps with a fixed exposure of 1/50th second.

there is little fear of a deficiency. Cobalt has been proved essential to the growth of animals. From this it has been deduced that it is also essential to man, although to date there has been no proof of this.

Certain wasting diseases of cattle and sheep has been proved to be due to deficiency of cobalt in the pasture soils.

If the dry soil content of cobalt falls below five parts per million, wasting of the animals will occur.

The daily cobalt requirement of sheep is only about 0.1 milligramme. An extremely small amount. It has been calculated that on an average cobalt-deficient pasture, the addition of only one ounce of cobalt salt to the acre would be sufficient to keep 1400 sheep healthy for a year.

MANGANESE

Manganese is essential to plant and animal life. In plants it seems to have something to do with the synthesis of chlorophyll. Lack of the element in the soil produces chlorosis in plants, withering of the tips of oats and other troubles. It seems to be essential to enable the plant to assimilate nitrates taken up from the soil.

The minimum requirements for most plants is a concentration of only 0.2 to 1 p.p.m.

In the human body the blood contains about 0.15 p.p.m. of manganese. The liver contains about 1.7 p.p.m.

Although as mentioned above the effect of manganese on human development is unknown, it is thought that it is essential to reproduction, for a deficiency of this element in animals leads to all kinds of faults in this function.

Most foods contain manganese in sufficient quantity for everyday needs.

The element iodine has received a great deal of attention because of its importance in the function of the thyroid gland.

IODINE

A deficiency of iodine leads to enlargement of this gland and in some cases to a stunted growth of the individual.

In natural products the occurrence of iodine is so small that it is measured in microgrammes per kilogramme, or in parts per 1000-million instead of parts per million.

In the soil the iodine content varies from 800 to 8000 microgrammes per kilogramme weight (1000 grammes). Fresh water contains very little iodine. The atmosphere contains only about 1 microgramme per cubic metre but is somewhat higher over the sea.



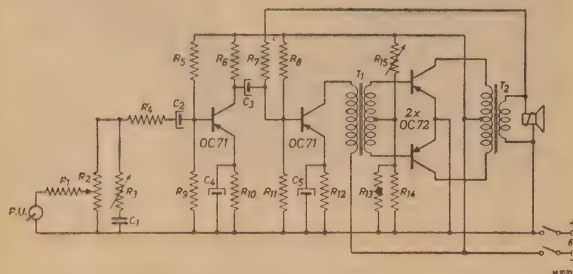
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Iodine is present in all plants, but only in minute quantities or traces from 2 microgrammes to 500. Seaweed contains much more—up to 2 pc.

The average daily requirement of iodine for an adult has been estimated at about 45 one-millionths of a gramme. That is 45-millionths of one thirty-second of an ounce—a very small quantity indeed.

The element boron is essential in small traces to plant life but there is at present no evidence to show that it is essential to animal life.

Several plant diseases are due to a deficiency of boron. It appears to have something to do with the reproductive function.

Three pounds of anhydrous borax per acre seems to be the maximum allowable in some cases. This represents the small amount of one quarter part per million in the top 12 inches of soil.

NITROGEN

Other plants like potatoes and other root crops will stand much more, so that when using borax it is probable that the area can be used only for those crops whose boron requirements fall within specified limits.

The element, molybdenum, has attracted widespread notice because of sensational results obtained in Australia and other parts of the world by the application of minute traces of this element to soils of very poor quality.

There are organisms in the soil which have a lot to do with the fixation of nitrogen in the soil. The most notable of these is called by the formidable name of *Azotobacter chroococcum*.

Soil must contain the correct amount of nitrogen, and this must be fixed in the soil. The above germ acts in helping to do this, but it has been found that it does this much better in the presence of molybdenum.

A concentration of molybdenum as low as one part in fifty-million increases the action of the bacillus one hundredfold.

One-tenth of a part per million stimulates the growth of lettuce. One-hundredth part per million is essential for the growth of tomato seedlings.

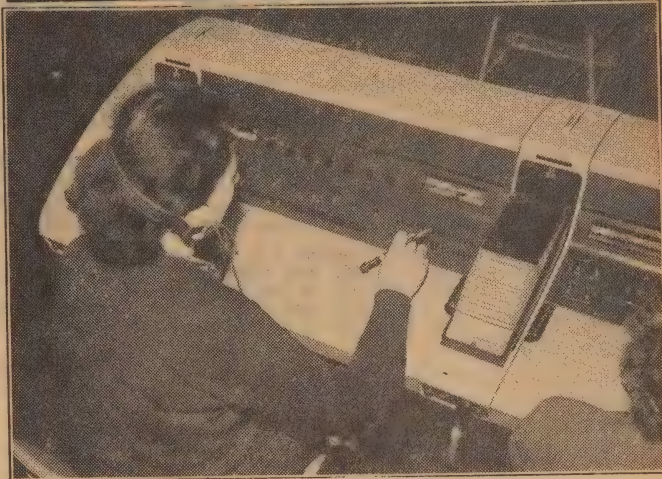
The sensational results in Australia mentioned earlier was in northern New South Wales, where ironstone soil of extremely poor quality was made to double the yield of lucerne by the addition of two pounds of sodium molybdenate to the acre.

A notable feature of all the elements necessary in traces for animal and vegetable nutrition and development, is the narrow margin which exists between the amount necessary for development and the amount which is toxic or poisonous.

BORON

For instance, boron, when added to the soil at the rate of one part per million, is just right for leafy vegetables. More than this will be toxic. A concentration of 1.6 parts per million is just right for root crops, but this will be toxic to grass and leafy vegetables. The difference is only .6 parts per million.

HELLO GIRLS PUSH BUTTONS



A new system is being tried out at the Thanet (Margate) telephone exchange, where operators sit at a board somewhat resembling the console of an organ. These are known as "cordless boards", because, instead of "plugging in" the operators use a "press button" system, which results in better marshalling of calls. No calls can be connected before one which came through earlier and callers "queue" for their turn. In the event of an emergency call coming through, this takes precedence over all others. The new system, dealing with the whole of Thanet, is by way of experiment to study the financial and efficiency side of the installation and to find out the reactions of public and telephone operators.

Iron has not been included in this discussion of trace elements for it is not truly so. It forms over 0.004 pc of the total body weight, so that the body of an adult contains about four grammes of iron. There is about 50 milligrammes of iron in each millilitre of human blood representing a concentration of 500 parts per million.

As stated above, copper is closely associated with iron in the human body, for it is the copper which makes the iron available in the liver.

Before we leave this discussion of trace elements, it is well to mention the vitamins, for they are indeed most necessary for nutrition yet are present in minute quantities in the food we eat, and are needed in very small quantities.

The administration of vitamins is based on the term, International Units.

This term originated when the League of Nations was in existence for this organisation took up the question, and a sub-committee arrived at the basis of measurement which was called the International Unit or IU for short.

It became necessary under this idea to standardise the activity of the vitamins. This is a little complicated to explain, but if I can make myself understood it will give some idea of the smallness of the vitamin unit required by the body.

Let us assume that it is necessary to standardise the activity of butter in preventing eye troubles.

The vitamin in butter which does this is pro vitamin A or carotene.

In order to standardise butter it is necessary to do so against a sample of pure pro vitamin A. One International Unit of pure pro vitamin A is taken to weigh 0.6 microgrammes. This is six-tenths of one-millionth of a gramme (a gramme is about one-thirty-second of an ounce) so that this unit is infinitesimal.

Now if 10 grammes of the butter had the same pro vitamin A activity as six microgrammes of pure pro vitamin A, then the butter is said to contain 10 International Units of pro vitamin A.

The same procedure is adopted for all the vitamins. Nowadays vitamins are not known so much by vitamin A, B, B1, C and so on. They are known by their chemical names. For instance vitamin A is axerophthol. Vitamin B1 is thiamine. Vitamin B2 is riboflavin. Vitamin B2 complex is nicotinic acid. Vitamin C is ascorbic acid and so on.

VITAMIN A

The necessary intake of vitamin A for an adult is about 5000 International Units per day. This is 5000 times 0.6 of a microgramme, which is 3000 microgrammes or 3000 times one-millionth of a gramme, still a minute quantity.

It will thus be seen that for the food we eat and drink we take in very large quantities in order to gain the infinitesimal amounts of minerals and vitamins necessary for life.

Mullard '5-10'

**HIGH QUALITY
LOW COST
AMPLIFIER**

Creates phenomenal interest—the first consignment of handbooks sold out in three days!
(refer page 38 August "Radio & Hobbies")

Already widely acclaimed in Great Britain and America, the Mullard "5-10" has now captured the interest of the Australian amplifier and high quality reproduction enthusiasts. Additional stocks of the "5-10" Handbook (3/9 or 4/3 post paid) have arrived by air and a further quantity is due on the s.s. "Nuddea" this month. The unprecedented interest has even exhausted our stocks of one valve type but by the time this issue is printed two air consignments will have arrived from the U.K.

For the convenience of constructors, here is a list to date of "5-10" kit and special component suppliers. The components are also available from radio part suppliers and wholesalers throughout the Commonwealth. Should you have difficulty in obtaining any item, we will be glad to advise from our offices in Sydney and Melbourne and through our distributors, B. Martin Pty. Ltd., 35 Charlotte St., Brisbane, Q'land, Woollard & Crabbe Ltd., 18 Chesser St. Adelaide, S.A. and Sandovers Ltd., 691 Hay St., Perth, W.A.

KIT SETS

Electronic Products, Box 28, P.O., Punchbowl, N.S.W.
Electronic Parts Pty. Ltd., 206 Broadway, Sydney, N.S.W.
Price's Radio, 5-6 Angel Place, Sydney, N.S.W.
Radio House Pty. Ltd., 296A Pitt Street, Sydney, N.S.W.
United Radio Distributors Pty. Ltd., 175 Phillip Street, Sydney, N.S.W.
Nova Electric & Engineering Company, 311 Sussex Street, Sydney, N.S.W.
Homecrafts Pty. Ltd., 100 Clarence Street, Sydney, N.S.W.
J. H. Magrath Pty. Ltd., 208 Little Lonsdale Street, Melbourne, Vic.
Homecrafts Pty. Ltd., 290 Lonsdale Street, Melbourne, Vic.
Radio Parts Pty. Ltd., 157 Elizabeth Street, Melbourne, Vic.

OUTPUT TRANSFORMERS AND POWER TRANSFORMERS

Electronic Products, Box 28, P.O., Punchbowl, N.S.W.
(output transformer only—Type 5571.)
Electronic Transformers Pty. Ltd., Gardere Avenue, Harbord, N.S.W.
(output transformer—Type A59.)
Nova Electric & Engineering Company, 311 Sussex Street, Sydney, N.S.W.
(output transformer—Type ML10.)
Ferguson Transformers Pty. Ltd., Ferguson Lane, Chatswood, N.S.W.
(output transformer—Type OP308.)
A. & R. Electronic Equipment Company Pty. Ltd., 378 St. Kilda Road, Melbourne, Vic. (output transformer—Type OT949.)

NOTES

1. Output transformer types mentioned here have been approved for the "5-10" by the Mullard Technical Service.
2. A special 300 volt 80 mA power transformer is required.

CHASSIS

Patton Products Pty. Ltd., 433 Princes Highway, Rockdale, N.S.W.
Arcadian Mfg. Company Pty. Ltd., 186 Rochford Street, Erskineville, N.S.W.

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Technical Review

MAGNETIC SOUND RECORDING ON SUB-STANDARD FILM

Magnetic heads and facilities are now available in this country for adding sound tracks to sub-standard movie films. An article in the French magazine, *Revue du Son*, gives a few hints which may be useful to readers contemplating the addition of magnetic sound-track facilities to an existing silent projector.

THE basic idea is an adaption of ordinary tape recording principles and comparable electrical circuits are required for recording and reproduction.

The film must first be submitted to the agents to be run through a special coating machine. This lays a narrow track of magnetic material along one edge of the film and outside the normal picture area. The position and dimensions of the coating vary with the size of film.

One or more magnetic heads have to be installed in the projector so that the film travels past them at even speed on its way into or away from the intermittent action.

To make the initial recording, the magnetic head is fed with a suitable audio signal and a high frequency bias, exactly as in a tape recorder. An erase head, installed immediately before it in the film run, can be used to eliminate any previous recording.

For playback, the head is switched across to the input circuit of the amplifier and signals previously recorded are reproduced in the loudspeaker.

LACK OF SPACE

One of the difficulties facing the amateur is the placement of more than one head in a suitable position on the projector. One method is to employ only a single dual-purpose head for recording and playback, erasing being done separately with a bulk eraser.

Mechanical considerations often do not leave much choice in the placement of even one head. In the interests of good speed regulation, both on recording and playback, the head should be located as far as possible from the intermittently moving part of the film and as close as possible to the speed regulating device. Three solutions appear to be practicable.

Converting a projector already equipped for optical sound track to magnetic sound track is the easiest of the three. Here the mechanism used to steady the film can well be utilised, by placing the head close to the position where the film runs over the flywheel shaft.

This method is often out of the question for amateurs, who only have silent projector. Because of space limitations such projectors cannot be readily modified to incorporate inbuilt mechanical smoothing.

Of two possibilities which remain, one is to place the projector on a pedestal which contains the necessary equipment to equalise the intermittent movement of the film. After the film has left the lower sprocket, it can be threaded through the system of pulleys in the smoothing equipment, before passing on to the take-up spool.

NEAR TOP SPOOL

In this case the record-playback head would be placed just before the film passes the flywheel.

The alternative position for the magnetic sound adaptor is between the feeder spool and the top feeder sprocket. This has the advantage of feeding the film into the mechanism at a constant speed, the continuous sprocket taking up any intermittent movement of the film and assuring, with the aid of a flywheel, a uniform rate of movement.

According to one authority, this method can be adapted to almost any silent projector.

Whatever be the method employed, the mounting of the head must

be carried out with the greatest precision, the gap position being extremely critical.

The trace width is usually less than one millimetre and the part of the gap used is of similar dimensions. To obtain anything like a useful output, adequate precautions have to be taken to prevent lateral movement of the film, which would give rise to serious flutter effects.

In this, the procedure is very similar to the setting up of optical equipment, where the adjustment is very critical owing to the small dimensions of the sound track and the light slit.

AMATEUR, COMMERCIAL FILMS

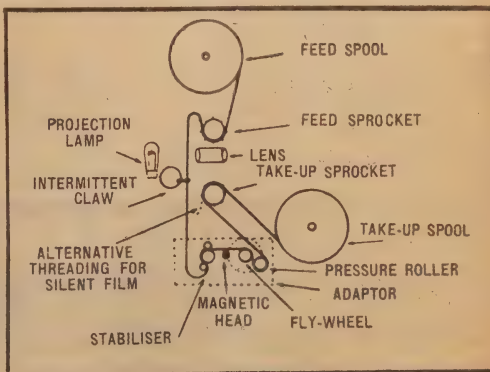
All is well, while the showing of either amateur, or commercial films only is contemplated. Difficulties, however, are likely to arise, if the projector is required to handle both film types.

This is due to the fact that it is preferable to apply the magnetic striping directly to the film base and not to the emulsion side. Although it can be done, better adhesion is achieved on the film base, with the consequent extension of useful life of the magnetic coating.

Amateur films are generally taken on 16 mm reversal film, and they are projected with the emulsion toward the lens. This means that on most commercial machines fitted with speed regulating equipment for the optical sound track, the film would be travelling over the flywheel pulley with the emulsion on the outside. The base would be in direct contact with the pulley, making the placement of the magnetic heads



Figure 1: Illustrating how a magnetic head can be added to an optical sound projector, using the existing provision for speed regulation. The magnetic head rests against the film as it runs around the flywheel shaft.



There's **NOTHING** to equal



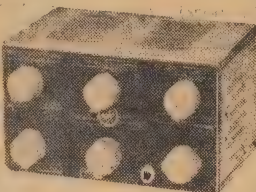
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HOME MUSIC SYSTEMS

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EQUALISER-PRE-AMPLIFIER UNIT

Extremely wide flexibility of control is afforded over the entire musical spectrum, providing innumerable combinations of tonal balance. Six controls are utilised viz., a 5 position record equalising switch for all makes of records, a radio-records switch, a treble rise—treble fall switch, a volume control, a treble control, and a bass boost control (both continuously variable).



POWER SUPPLY UNIT: Comprises a centralised power supply for the Ferris Hi-Fi Home Music System (or any other suitable equipment) and provided with sockets for plug-in cable attachment to the other units. A 6-volt A.C. outlet is also provided for external panel illumination, etc.

PRICES

RADIO TUNER, £30/14/-, **EQUALISER-PRE-AMPLIFIER**, £20/11/-, **POWER AMPLIFIER**, £29/2/6, **LOW PASS FILTER UNIT**, £12/8/6, **POWER SUPPLY**, £28/17/-.

FOR BEST RESULTS high quality associated equipment is recommended for use with the Ferris Hi-Fi Home Music System . . .

Suggested items are:—

Bakers 12in. triple cone loud-speakers . . . £25/16/3
Goodmans Axiom 150 Mark II loudspeakers . . . £22/16/-
Polished Corner vented enclosures for above . . . £33/12/-
Goodmans Axiette 101 8in loud-speakers . . . £12/17/3
Polished vented enclosures for above . . . £21/1/6

Thorens CBA83 automatic 3-speed record player with G.E. variable reluctance pick-up . . . £48/-/-
Thorens CB33 3-speed Manual Record Player . . . £38/10/-
Acos HGP40 Crystal pick-up with 2 heads . . . £9/15/-
Goldring No. 500 variable reluctance pick-up with turn-over head . . . £7/10/-

THIS EQUIPMENT consists of five units—Power Supply, Power Amplifier, Equaliser-Preamplifier, Low Pass Filter and wide range tuner. Each unit is available separately and is self-contained except that the tuner, equaliser and power amplifier draw their required current from the separate power supply.

TECHNICAL SUMMARY

Output frequency response of complete system from input to output 20 cps. —15,000 cps. + or — 1 db.

Harmonic and intermodulation distortion—Negligible. Maximum rated power output—12 watts.

Hum and noise level — 60 db below full output.

Alternative input terminals are provided for magnetic or crystal pickups.

Degree of treble boost at 10KC/S relative to 1KC — 19 db.

Degree of treble cut at 10KC/S relative to 1KC — 19 db.

Degree of bass boost at 50 cps. relative to 1KC — 19 db.

Continuously variable.

HIGH FIDELITY RADIO TUNER

Has frequency coverage of 530 to 1,620 KC/S. Incorporates a 10KC/S whistle filter and special low distortion detector circuit. Large perspex dial calibrated for all Australian States and in metres and kilocycles.



POWER AMPLIFIER UNIT. Incorporates highest quality output transformer with 17 db inverse feedback loop from secondary to amplifier input. Stable, low noise, straight forward amplifier with a completely flat frequency response from 15 to 15,000 cps. Negligible harmonic and intermodulation distortion.

LOW PASS FILTER UNIT

A "top cut" filter for eliminating intermodulation distortion and/or surface hiss from worn or poor quality recordings when played either at home or broadcast on the radio programmes. Designed to provide a sharp cut-off characteristic at 2 cut-off frequencies, viz., 6 KC/S and 3 KC/S plus a third position in which the filter is switched out of circuit to utilise the full range linear frequency response characteristic of the amplifier.



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ther difficult, though not impossible.

On the other hand, commercial 16 mm films are copies made from master negative. These are projected with the base toward the lens, thus, unless provisions are made for an adjustment of the head position in relation to the film, it becomes quite impossible to use the magnetic stripping.

Similar difficulties can be expected in the case of prints made from negative, or an original reversible master, for instance, when a magnetic sound track has to be made in one language, which already has an optical soundtrack in another. These are the basic mechanical problems. Electrically, the results are only as good as the amplifier system, so that due attention must be paid to the basic problems of signal-to-noise ratio, adequate frequency response and low distortion.

Even allowing for good amplifying equipment, results can be seriously compromised by other effects which are not always appreciated by amateurs. It is most important, for

The effect is due to the displacement of the operating point on the hysteresis curve of the head core material.

It is equally important to see that the reels carrying the film are not magnetised, or for that matter, parts of the projector close to or in the film path. The ideal solution is to use non-magnetic metal for reels and other relevant components.

This approach cannot always be

We are not interested in the speed of 24 frames per second, as this speed is not used by amateur photographers. Movement can be depicted with sufficient accuracy at a speed of 16 frames per second and, with modern projectors, no trouble is experienced from flicker at this speed.

The use of 16 frames per second enables the amateur to cut film costs almost in halves.

The coating for the three types

Figure 2: One possible method of adapting a silent projector for magnetic sound. The extra equipment is installed in a base unit, on which the projector rests. The film is threaded through the unit before passing to the final sprocket to take-up spool.

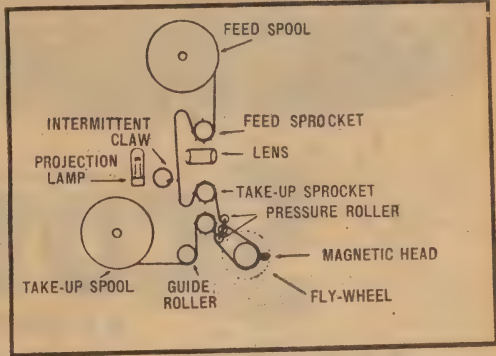
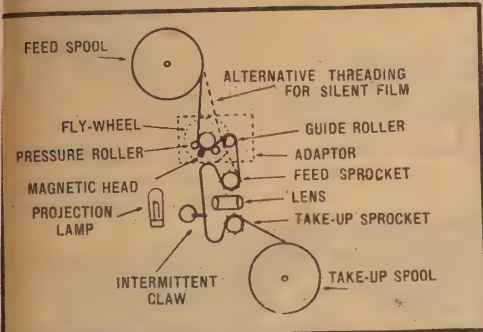


Figure 3 (Left): An alternative method of adding magnetic sound to a silent projector. In this case the head and flywheel mechanism are installed between the feed spool and the top sprocket.



of sub-standard film is the same so that, assuming the same type of head and the same program material, the high frequency limit of the recorded sound varies in proportion with the film speed.

The upper limit of frequency response for 16 mm film at a speed of 12 cm/sec, and using magnetic coating and recording heads generally available in France, is well over 5000 c/s. Values for 16 mm and 9.5 mm are similar because there is only .8 pc difference between the two speeds. The frequency limit is halved for the 8 mm format, as the speed is only half of that of 16 mm film. Actually it is something over 3500 cps.

Results obtained with magnetic sound tracks thus compare more than favorably with those obtained by conventional photographic soundtracks, in the case of 16 and 9.5 mm film.

It is obvious, however, that the results are inferior to those obtained by synchronising a conventional tape with the film, using all facilities offered by modern tape recorders. However, it is likely that significant improvements will be effected, in the future, particularly as far as background noise and frequency response are concerned.

BIAS COMPROMISE

With magnetic recording, a compromise has to be made in the bias level. High bias gives reduced signal level, with low distortion, but with an attendant decrease in signal-to-noise ratio. Lower bias gives high recording level and high signal-to-noise ratio but higher distortion.

Under the most favorable conditions the magnetic recording process is capable of giving signal reproduction with a harmonic distortion of the order of 2 pc.

If we were to reduce the bias level in order to obtain good signal-to-noise ratio, the distortion may increase to about 5 pc. Provided the amplifier used does not introduce a prohibitive amount of distortion of its own, this figure would be acceptable in all except the most critical cases.

example, to avoid magnetising the head.

Such magnetism can occur, for instance, if the recording head is suddenly brought into, or removed from, the stray field of a loudspeaker. Also any discontinuity in the circuit, such as when the head is connected, may result in a short, high intensity pulse of DC and consequent magnetisation. Unless the head is subsequently demagnetised, excessive noise level and distortion may occur.

In particular, one must warn against the practice of checking continuity of the windings with an ordinary DC ohmmeter.

BIAS SWITCHING

Another important point, not generally discussed in articles dealing with magnetic recording, is that the HF bias can cause residual magnetism of the head, if it is interrupted at the peak of the cycle. It is particularly likely to happen when the one head is used for both recording and playback. It is therefore important not to cut the bias current abruptly but to reduce it gradually using, for example, the discharge time of a bypass capacitor on the bias oscillator HT supply.

This precaution, which is not always observed by well-known manufacturers, can give an improvement in signal-to-noise ratio of 10 to 20 db, as against recordings taken without these special precautions.

Distortion is reduced in similar proportions.

applied if an existing equipment is to be adapted for magnetic sound. Too often the sprockets and rollers over which the magnetic coating of the film has to pass are made of ferrous materials. In such a case, the best one can do is to demagnetise these components as frequently as possible.

Having disposed of signal-to-noise ratio, attention can be directed to the frequency response of such recordings.

Although film speed does not affect the bass response of magnetic recordings to any extent, its effect on the treble response is marked.

The manufacturing technique of recording and playback heads has been so nearly perfected that, for practical applications, the frequency range of the head can now be considered unlimited. The real problem has to do with demagnetisation effects in the coating itself.

The magnetic coating on the film should naturally be suitable for the speed at which it is to be used. Oxides suitable for use with standard 35 mm film, the magnetic striping being 6.35 mm wide, at a speed of 77 cm/sec, would give deplorable results if used on 16 mm film with a speed of only 12 cm/sec.

RESPONSE LIMITS

This, of course, leads naturally into the question of what upper frequency response can be attained with present techniques, on the basis of 3db down on zero reference at 1000 cps?

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ELECTRONIC READER FEEDS BUSINESS MACHINES

In a recent article in *Electronics* by D. H. Shepard and C. C. Heasley, jun., details are given of a photoelectric reader which is capable of transforming ordinary printed characters to business machine data at the rate of 3,600 words per minute.

WHILE "processing" machines for business data are by no means new, their use has largely been limited by the slow speed, high cost and low accuracy of keyboard operations.

This is so because the transfer of information from a business document to a machine record medium has always required the services of an operator to read the information and to manipulate a keyboard of some sort or another.

READS AUTOMATICALLY

The analysing reader eliminates this human limitation on the speed of electronic business machines by reading ordinary typed or printed characters and recording the information on machine mediums such as punched cards, perforated tape or magnetic tape. It is also possible to use information suitably sensed to control sorting, editing and table-lookup operations.

The operation of the reading system is shown in figure 1. A feed mechanism passes a single document in front of a photo-electric scanner which scans the characters on the document. Electrical pulses from the scanner are amplified and shaped by the video chassis and then analysed by the interpreter.

The interpreter identifies each character and sends identifying pulses to coding and storage. The storage serves as a buffer to meet the timing requirements of the output device. Information is withdrawn from storage and used to control the output device.

Storage also contains information as to whether or not the document has been successfully read. This decision is sometimes made by the interpreter, which can recognise errors caused by malformation of characters.

PROPERLY SORTED

If a document has been correctly read, it is placed in the accepted pocket; if not, it goes into the reject pocket.

A simplified diagram of the arrangement of the scanner is shown in figure 2. The document is fed at uniform rate past the reading station where it is brightly illuminated. The reflected image of the document is projected through a scanning disc on to a multiplier phototube through a series of lenses and a mirror.

The scanning disc, shown in figure 3, contains a number of radial slits which pass one at a time in front of a fixed slit. At the intersection of these slits, a point of light from the image passes through and is projected on to the phototube. As the disc rotates, the intersection of

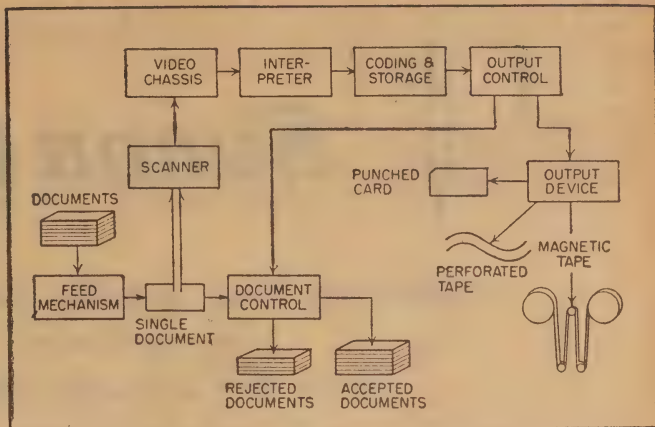


Figure 1. The complete electronic reading system for use with mechanical business machines. The model now under construction will handle over 450 documents per minute, reading printed data on each in turn and transferring it to the desired medium at speeds of over 300 digits per second.

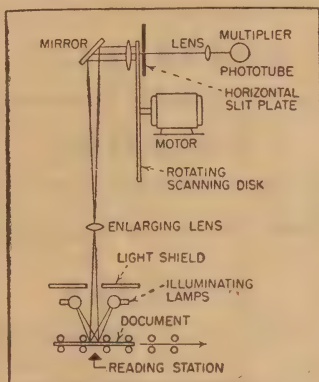


Figure 2. Optical system for scanning one line of text on document as it moves past reading station.

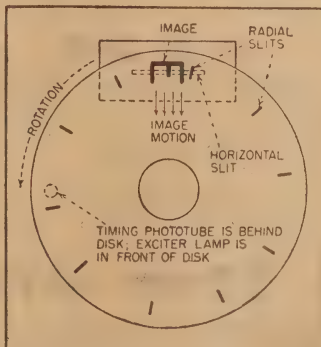


Fig 3. Details of the scanning disc, used to obtain 25 to 30 vertical scans per character.

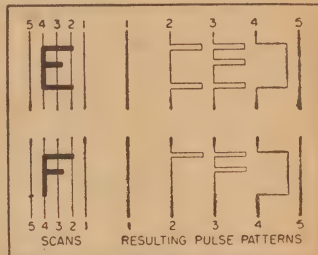


Figure 4. Characteristic pulse patterns resulting from scanning of capital letters E and F.

the slits moves to give horizontal scanning across the image.

Because the document is moving, the image is also in constant motion, so successive scans fall on successive portions of the image.

Since the scan rate is much faster than the document motion, 25 or 30 scans will occur as one character passes the reading station.

As the image of a character is scanned, the output of the phototube will vary. Thus, during a single scan the output will contain positive pulses representing dark portions of the character.

Figure 4 shows the typical pulse patterns produced by two capital letters. With the letter E, the horizontal lines produce three short pulse patterns for many scans. The long vertical line on the left produces one long pulse for at least one scan. Thus the input signals to the circuit would be a long vertical line on the left, three horizontal lines and nothing to the right of the horizontal lines.

Each letter gives its own particular character. If an impossible combination of strokes occurs, the interpreter recognises it as an error and sends out a reject signal.



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MIC 36



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Housed in attractive plastic case, this Microphone is ideal for home recording and public address, etc. Response unexcelled for its size and price. The performance is not affected by vibration, shock or low frequency wind noise. Omni-directional frequency response substantially flat from 30 to 7000 c.p.s. Recommended load resistance not less than 1 megohm dependent on low frequency response. Can be supplied complete with switch and floor stand adaptor as required at a small extra cost.

HIGH QUALITY MICROPHONE

Designed to meet even the most exacting requirements, this Microphone incorporates the world famous floating crystal sound cell construction. Its special characteristics are that its fine performance is not affected by vibration or shock. The fidelity is not impaired by low frequency noise.

MIC 16



SPECIFICATION

Recommended load resistance—not less than 1 megohm.
Output level—65 db ref. 1 volt/dyne/cm².
Frequency response—substantially flat from 30 c.p.s. to 10,000 c.p.s.
Directivity—non-directional.
Size—2 1/8 in spherical diameter.
Connector—Standard international 3-pin.

£24/19/6

GENERAL PURPOSE

MIC 35



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The MIC 35, undoubtedly the best value ever offered, is ideal for amateur transmitters, public address, etc. Housed in an attractive die-cast case, it features a high sensitivity and substantially flat characteristics. Provided with a built-in shunt resistance of 2 megohms, it will, when connected to the grid of the input valve, give a substantially flat response from 50 to 5000 c.p.s.

SPECIFICATION

Output level: -55 db ref. 1 volt/dyne/cm².
Cable—approx. 4ft. of co-axial supplied.
Weight—6ozs. unpacked, 7 ozs. packed.
Dimensions—microphone only 2 1/4 in x 2 1/4 in x 1 1/4 in.

TABLE or STAND MICROPHONE

This omni-directional Microphone is robust in construction, with a pleasing appearance. Vibration, shock or low frequency wind noise will not affect the performance. The low frequency cut-off is dependent on the load resistance. The cut-off is given by the quotation, $F = 80$ divided by R , where F = c.p.s., R = megohms. An adaptor (floor mounting) is available at low extra cost.

MIC 22



SPECIFICATION
Output level = -50 db ref. 1 volt/dyne/cm².
Output impedance—equivalent to approximately 0.002 uF (0.8 megohm at 100 cycles).
Frequency response—substantially flat from 40 to 6000 c.p.s.
Recommended load resistance—not less than 1 megohm, dependent on low frequency response.

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LAPEL MICROPHONE

Designed to give freedom of movement, this Microphone is small and non-directional. Housed in a soft moulded rubber case, which gives protection against shock, it is provided with a pin at the rear of the case for pinning to the lapel.

MIC 28

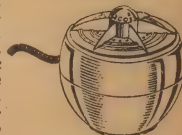


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Output level—approx. -55 db ref. 1 volt/dyne/cm².
Recommended load resistance—5 megohms.
Frequency response—level throughout the whole of the audible spectrum.
Capacity—0.0015 uF. at 1000 c.p.s.
Impedance—100,000 ohms at 1000 c.p.s.
Cord—6ft. shielded cable.
Size—1 9/16 in wide x 2 1/4 in long x 5/8 in thick.

HAND or DESK MICROPHONE

MIC 33



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This Microphone has been designed for the high quality public address and home recording field. High sensitivity and flat characteristics are obtained by a specially designed acoustic filter. Housed in an attractive plastic case with an unexcelled response for its size and price. Unaffected by vibration, shock or low frequency wind noise. Omni-directional frequency response substantially flat from 30 to 7000 c.p.s.

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(MIC 32 illustrated)

CRYSTAL MICROPHONE INSERTS

These inserts are available in varying sizes ranging from as small as 15/16 in square to 1-13/16 in round, with various thicknesses from 7/32 in to 9/16 in. Suitable for every purpose such as hearing aids, public address, tape recording, amateur broadcasting, etc. they have responses from 2250 c.p.s. to 3500 c.p.s. at 5 db to 30 db. Insert can be supplied with or without 10 meg. resistor as required.

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MICROPHONE INSERTS



(MIC 23 illustrated)

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NEWS AND VIEWS OF THE MONTH

Sun drives motor car

NOT long ago we read of experimental model radio sets operated by batteries which drew their power from the sun.

Although there is no present commercial value in such receivers they are of great value to engineers and scientists who believe that some day there will be an application for them.

Now we hear of a model motor car which is driven by sun power. It will be on show in Chicago this month.

The 15in model, built by General Motors, has 12 photo-electric cells which convert light into electric current, which, in turn, drives a tiny electric motor to propel the car.

In the demonstration, light from electric lamps will be used to start the car.

Atom-powered subs

THE US Government is proceeding vigorously with its scheme to build atom-powered submarines.

In doing so, it recognises the value of the sub. in national defence and possible war, and the importance of providing a power source which will be light, compact, and capable of operating over long periods.

Whether all these targets have been met completely is known only to the US Navy.

But in recently letting a contract for the development of a nuclear reactor for a small sub, it is obvious that results are good enough for specialised designs to be considered.

By July the US will have nine atomic submarines with many others to follow.

America's present two atomic submarines, Nautilus and Sea Wolf, have engines already outmoded and the submarines are big and bulky.

The new US submarine will be conventional in size and therefore more manoeuvrable.

Designers of Nautilus and Sea Wolf did not pay much attention to the submarines' specific mission with the fleet.

Future atomic submarines will have to do a specific job.

Travelling in space

THE recent International Astronautical Conference in Denmark produced an unusually detailed and optimistic procession of forecasts about man's future preoccupation with outer space.

Almost every speaker at the conference, which included representatives from 16 nations, made light of the problems involved as being any barrier to ultimate success.

The general opinion seems to be that the first step is to create artificial satellites which will revolve around the earth and the moon, and, from their behavior, check our present knowledge of outer-space conditions.

These satellites are expected to provide new information which is necessary before man can confidently venture farther afield.

Dr. Wernher von Braun, the builder of the V-2 rocket, now a leading missile expert with the US Army, said that the United States plan to launch a satellite within three years marked the beginning

of man's "last great adventure"—the conquest of space.

By 1985 commercial airliners would fly at altitudes of about 12 miles—nearly three times the present height, he said.

They would travel at speeds up to 2000 miles an hour.

Rocket ships would be operating, but not for commercial passengers.

"By 1985 we'll have a manned space station circling our globe in an orbit 1075 miles above the earth," he said.

"I think it is a good bet that within the next 30 years we'll see first an unmanned 'baby' space station—a small instrument-carrying rocket—fired into an orbit, say, 200 miles above the earth."

The president of the Aeronautical Association (Dr. Frederick Durant) predicted that man would set foot on the moon in 45 years.

"Within 25 years man will board satellites circling the moon," he said.

Dr. Durant said a space-craft travelling at 18,000 miles an hour—the speed the planned American satellite would girdle the earth—would take 13 hours to travel the 238,793 miles to the moon.

Professor Knut Lundmark, former head of the Astronomy Department of Lund University, South Sweden, said in Stockholm:

"The news about the first space satellites opens up gloomy perspectives."

If space stations were established they would give great strategic advantages to their owners, he said.

"There is a great risk of a struggle between different groups of powers for the first space station."

POPULAR SCIENCE QUIZ

Q: What new drugs are being investigated for use in the treatment of rheumatoid arthritis patients?

A: These are aldosterone, fluorohydrocortisone, metacortandralone and metacortandracin. Many patients using these new drugs have found increased relief from them and the results are superior to those obtained with cortisone and hydrocortisone. These new drugs also do not have some of the harmful side-effects of the other types. Such side-effects have often limited the use of drugs and, in many cases, the dosage has had to be reduced even at the expense of a return of some of the arthritis symptoms. Another limiting factor in the use of cortisone has been the difficulty of its production in quantity. Of the four new drugs, metacortandralone and metacortandracin appear to have the most beneficial results, although it will be

a year or two before the true value of the new drugs can be assessed.

Q: What is the earliest town discovered by mankind?

A: A University of Chicago expedition headed by Dr. R. J. Braidwood, of the Oriental Institute, has recently discovered at M'lefaat in north-eastern Iraq a town thought to be more than 7000 years old. It was at about this time in history that man changed from nomadic hunting to agriculture. Among the ruins were found excellent flint tools, axes, and heavy stone mortars. The absence of sickles in the ruins suggests that at that time they had not begun to cultivate grain.

Q: What is a twin-rotor conventional plane.

A: This plane, designed and built by the Transcendental Air-

craft Corp., USA, is similar in general appearance to a normal helicopter. However, instead of a single blade rotating in the horizontal plane above the fuselage of the aircraft, two smaller units are mounted on the wing tips. Once the aircraft is airborne these blades may be tilted forward to give forward movement to the aircraft in the same way as conventional propellers. Test flights of the aircraft have been made to a height of 3000 feet and the rotors have been tilted forward about 30 degrees.

Q: How can radioactivity be used to measure machine tool wear.

A: Machine tool bits are first subjected to radiation. Then the chips from the work being processed are collected. The amount of radioactivity transferred to the chips is a measure of the tool wear.

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The Palomar Observatory, California, has completed the first sections of a sky atlas, revealing stars, galaxies, and systems of galaxies stretching far out into space.

The observatory is sending out copies of the first 200 sections of the 1758-section atlas to observatories all over the world.

British A-plant plans

REPORTS say the British Army and Air Force are developing a number of mobile power stations working from atomic power.

They will be mounted in vehicles, which look like big tanks, and will be capable of travelling almost anywhere under their own power.

They would be valuable in providing electricity for landing fields or for troops stationed in areas where fuel was scarce.

These atom-powered "package power plants" are still on the secret list.

In general principles, the power plants will use steam turbines to drive electrical generators. The steam is provided by an atomic furnace, the whole thing being described as "a huge steam kettle".

Color TV unpopular

JUDGING from reports, color TV need not worry Australia for some time to come.

Manufacturers of TV sets in America have almost given up making sets for color.

They predict that sales of color receivers this year will be about 35,000.

This would be less than half of one pc of total sales.

Retailers estimate that total sales of sets this year will beat last year's record of 7,300,000.

The industry believes the present trend is for a second black-and-white set in the home rather than a color receiver.

Retailers estimate that 5 pc of TV owners have two sets.

They predict that booming sales this year will boost that figure to 7 pc.

With no buying rush for color sets, the industry has no incentive to expand color television.

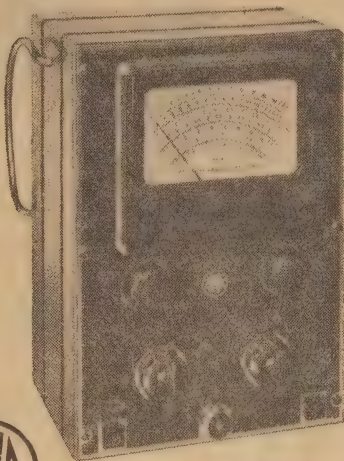
High-power tube

A NEW high-power radio tube called the "Vapotron" is currently being used in France. Cooled by the vaporisation of water, it is being applied to high frequency heating as well as to conventional radio and television transmitters. The tubes are so compact and powerful that they can replace several physically larger types and allow the size, cost and installation problems of the transmitter to be reduced quite significantly.

Maintenance and operating costs are also said to be reduced.

When the tubes are in use, the waste heat can be retained quite conveniently for auxiliary purposes such as heating the building. All this adds greatly to the overall efficiency of the installation, as demonstrated by the high-power broadcasting transmitter at Strasbourg-Selestat, which is equipped with Thomas-Houston Vapotron tubes.

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In addition, direct resistance measurements can be made on all the circuit components—coils, chokes, transformers, and resistors from low ohms to thousands of megohms—plus continuity checks and tests on condensers for leakage. D-C currents can also be measured directly.

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high voltage probe.

Resistance: Up to 1000 Megohms, in 7 self-contained ranges.

Current: 0.02—1500 milliamps D.C., in 7 ranges.

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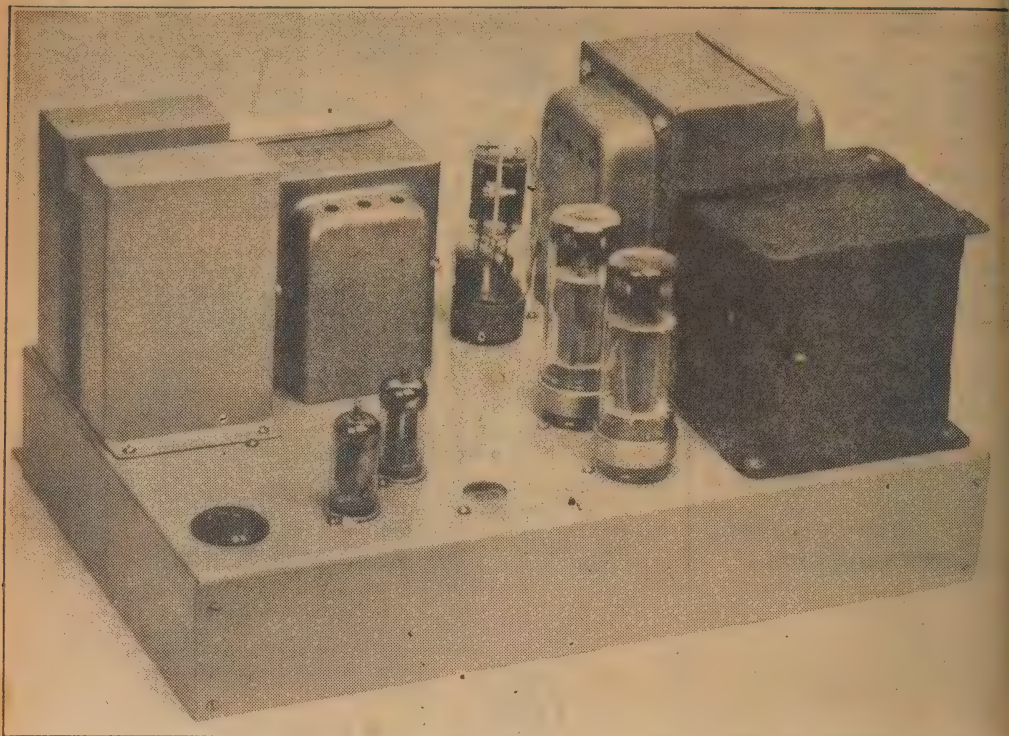
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A front view of the amplifier. Plenty of room has been allowed on the chassis to accommodate any combination of components you are likely to use. Our blue-print will show the first two valves arranged in line. Note the paper filter capacitors, recommended because of the high voltage. Power and output transformers must have their cores at right angles.

A HIGH POWERED PLAYMASTER

Here is a really high-powered amplifier, nominally intended for a maximum output of 20 watts, but capable of up to 30 watts. It is intended for the largest high-fidelity installations, its high-power capabilities being designed to preserve extremely low distortion at useful levels. It operates with any of the Playmaster control units and tuners.

HIGH-POWERED audio amplifiers have always had their following, and there seems to be every indication that they always will.

In the first place there are those who have a genuine use for 20 or 30 watts of output. There are the people who must operate multiple speaker systems, or who can only cover their requirements by brute force. They often include operators of small dance halls and picture theatres, as well as the small army of those interested in PA work.

But there is also a school of thought which says we can't have too much power, even if we never use it. Better to have a 20 watt amplifier and load it lightly, than a

10 watt amplifier stretching out near the limit of its means.

The fact that a big amplifier costs a good deal more money to make isn't a deterrent to such people. They point out that a few more pounds might well have been spent on a fishing rod, or a cricket bat, or a

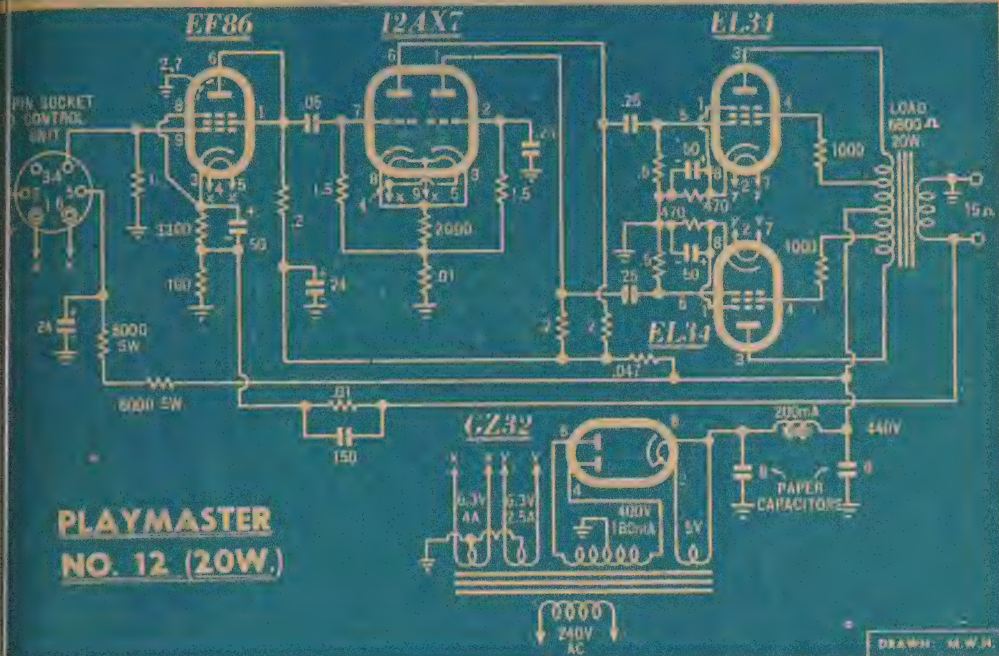
photographic light meter, if other hobbies had attracted them. Why not then go for the very best if they are prepared to spend the money on their amplifiers?

There is ample evidence for this argument, for it is undeniable that amplifier distortion increases as the maximum output is approached, and will rapidly rise to an unacceptable figure just after this point.

We try to make amplifiers which retain an almost constant level of low distortion for as far along the power curve as possible so that the full capabilities can be usefully employed. But there is no doubt that the first 50 pc of available power has much less average distortion on

by John
Moyle

CIRCUIT DIAGRAM OF HIGH POWERED PLAYMASTER



PLAYMASTER NO. 12 (20W.)

The circuit is similar to that of the 17-watt Playmaster which is now probably the most popular of them all. Grid suppressors of 2000 ohms are often fitted to the EL34 valves.

comparative basis than the second.

It is therefore a good thing to use a large amplifier as is practicable with a working power point not eater than 1/10th to 1/20th of the maximum available output to provide ample margin for distortionless

works. This estimate might seem an extravagant one, but we have more an once observed on an oscilloscope the ratio of peak-to-average output voltage from a well-cut LP record, and have been somewhat taken back with its magnitude.

SAFETY MARGIN

It would mean that, for a wide-range system, a 10 watt amplifier could not be operated at more than 10 watts average power to maintain safety margin. In practice, this probably what happens in many cases, as this amount of power fed to a sensitive speaker system makes a very big noise.

For anyone who habitually uses high audio power, therefore, a 20-watt amplifier might not be an absurdity nor an extravagance, particularly if he is one who believes in the value of high power purely on the grounds of lower distortion.

I am not at this stage making any firm recommendations to apply to particular cases. I would be the last to suggest that you owners of 17-watt Playmasters should immediately throw them away and go all out for 30 watts, or even that the 10-watt owners should raid their bank

accounts for the good of the cause.

Rather am I recording that, if you have money to spend, and have a loud speaker system good enough to tell the difference, there is a case for a high powered amplifier, even if it is never pushed to its limit. I am acknowledging, too, that there are plenty of people who think that way, and who ask us how to make such amplifiers.

There are also readers who have in their possession the power supplies which once did duty in a Williamson, or who have in operation the original Playmaster No. 1, with its 807's and 425 volt power transformer, who are looking for something better. They may have no more than a hefty 385 volt transformer left over from the old days, with a choke to match, which looks

very lonely doing nothing at the bottom of the junk cupboard.

But their minds are always turning toward a big job which someday they hope to build.

The recent release in Australia of the EL34 output valve, and the even more recently available data on its use in an Ultra-linear circuit, encouraged us to include in the Playmaster series a large amplifier which would supplant the early version, costing no more to make but giving much better results.

The EL34 is a big valve, and really comes into its own when producing 75 and even 100 watts of audio for special purposes. This it can do under very attractive operating conditions, as a glance through its operating data will show.

Naturally for these outputs very

PARTS LIST

1 chassis 14 1/2 x 9 1/2 x 2 1/2 in

1 power transformer 400v 180 ma, with 6.3v 4a, CT, 6.3v 2.5 ACT and 5v 3a heater windings.

1 12 Hy 200 ma choke.

1 Output transformer, 6600 ohm U/L, to suit speaker, 2 EL34 valves 1 12AX7 valve, 1 EF86 valve, 1 GZ32 valve.

CAPACITORS

2 8 mfd 400v oil filled paper (see text), 2 24 mfd 525v electros, 3 50 mfd 40v electros, 3 .25 mfd 400v paper, 1 .05 mfd paper 1 mica phase correction capacitor (see text).

RESISTORS

2 1.5 meg, 1 1 meg, 2 .47 meg, 3 .22 meg, 1 .01 meg, 1 3300 ohms, 3 2200 ohms, 2 1000 ohms, 1 100 ohms; feed back res. (see text), all 1/2w, 1 .047 meg, 1W, 2 470 ohms, 3W, 1 2 6000 ohms, 5W.

3 Octal sockets, 1 6-pin socket, 2 Noval sockets.

SUNDRIES

Mains flex and plug, nuts, bolts, solder lugs, 4 8 lug strips (ST 28) 1 5 tag strip, (ST 25) 2 3-tag strips, hookup wire, tinned copper wire, spaghetti.

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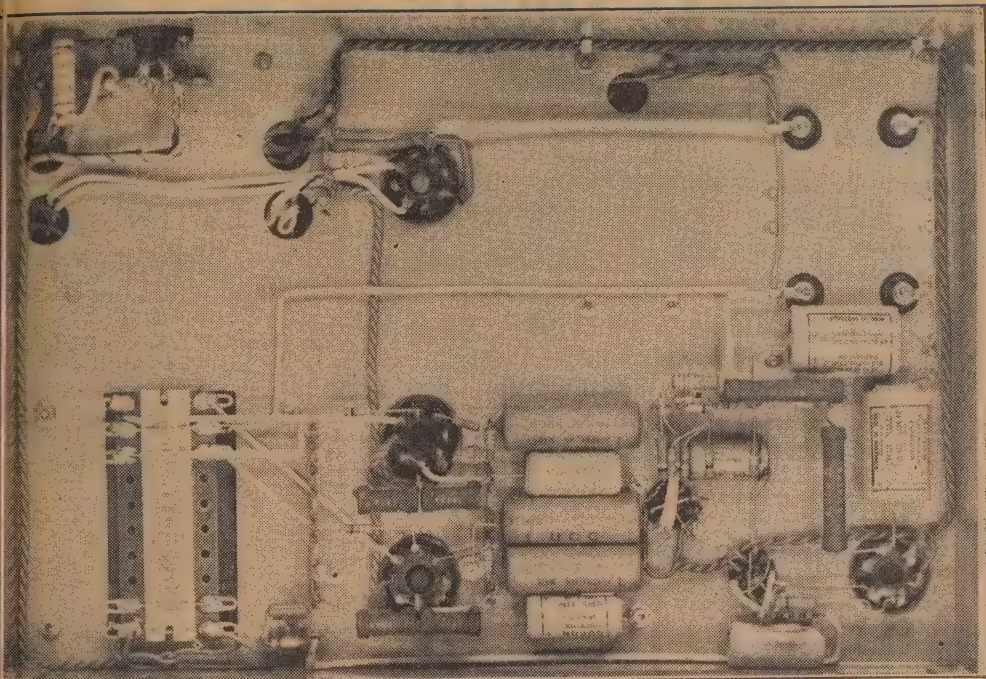
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HIGH POWERED PLAYMASTER—UNDERCHASSIS VIEW



The underchassis view shows how the components are grouped to give a balanced type of construction. Plate cathode and feedback resistors connected to the EF86 should if possible be high-stability types to reduce noise. Phase-changer plate resistors should be 5 per cent types. Two resistors in series will probably be needed to get the right value for EL34 bias.

With voltages are required, and by the time we scale down operating conditions to the 10 and 15 watt level, we find the job can be done more efficiently by its smaller brother, the EL84.

But for 20 or 30 watts, this valve is too small. We could of course use the EL37 with higher voltage, and there is nothing wrong with this excellent valve, which we have already used in the 17-watt Playmaster No. 12.

NEW VALVES

In this design we have used the EL34 because it is a later type, and its merits must be taken into consideration sooner or later.

Just as we were cogitating on its application for ultra-linear work, an amplifier circuit was released by the Mullard company using ultra-linear EL34's, which was, in effect, a vehicle for publishing authorised ratings for this type of service. Its specifications reveal that the valve works very well in ultra-linear connection, and with an effective power supply of 400 volts will deliver nearly 35 watts of output power.

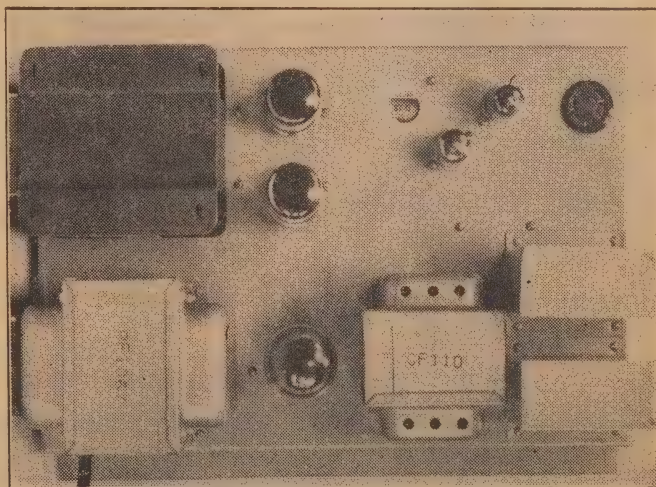
The amplifier is rated as a 20-watt amp, so here again we have this idea of providing a high output maximum, and using only portion of it to restrict distortion.

The circuit uses the same direct-coupled front end as was featured

in the amplifier described in last month's issue, but is otherwise substantially the same as the 17-watt Playmaster circuit described earlier

in the year. Its distortion figures at the 20 watt level, feeding a resistive load, are extremely low.

Although at the time of writing we



This top view illustrates the general amplifier layout. The final design will line up the EF86 with the 12AX7. The odd socket hole was made during some experiments,

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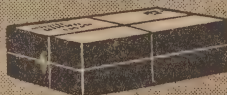
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not measured the distortion of the amplifier described here, we have available some measurements on a similar amplifier. It was built with the same output transformer as shown in the photographs, with 325 volts high tension.

As a matter of interest, the figures show a total distortion at 20 watts approximately .1 pc at 1 Kc, and intermodulation distortion of .5 pc taken at 40 cycles and 1 pc in the ratio of 4-1. Feedback of 20 db and similarly applied.

With our power supply giving 400 volts between plate and cathode, results should be even better.

It will readily be seen that to get hairs over figures of this order is mere waste of time, particularly at our average operating level which will easily exceed about two watts even at really high volume.

FSH MAXIMUM

The extra voltage we used allowed us to measure 33 watts output at 1 Kc, 31.5 watts at 50 cycles and 28 watts at 15 Kc, which, for a transformer rated at 20 watts, isn't a bad performance. Naturally distortion figures at this high level may not be quite as low, but it is an indication of overall performance.

The frequency response we obtained using 22db of feedback, and with the amplifier adjusted to give the best square wave response, is shown in a graph with this article. From an laboratory standpoint it isn't as impressive as some amplifiers we have built, which show little variation up to almost 300 Kc. But from a practical standpoint, any amplifier which is only 1 db down at 60 Kc, which exhibits such a docile attenuation after that is not only in a class, but more than compares with any commercial type you can get.

At the moment this appears to be the only 20-watt transformer available, but there are several 15-watt types, some of which we have tested with almost identical results, except for maximum power output figures. At the time this article appears in print there will probably be several types available from the well-known transformer factories.

The circuit is virtually the same as that used for the 17-watt Playmaster for the good reason that we saw no occasion to change it.

GENERAL CIRCUIT

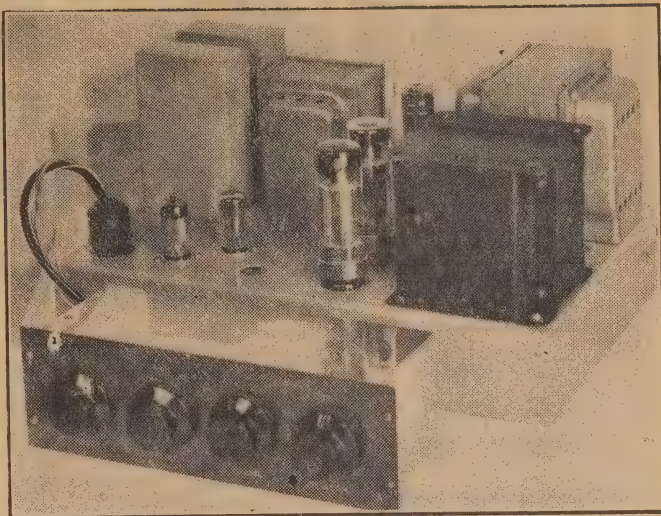
It consists of a triode amplifier, resistance-capacity coupled to a cathode - coupled phase - changer, which is coupled by a similar method to the output stage.

The first valve is an EF86, which is not only non-microphonic, but has a low noise level. The phase-changer is a 12AX7, which gives appreciable gain in this position.

The over-all feedback works out at approximately 22 db. This is a little higher than we advise for general use, but output transformers suitable for this amplifier are not ordinary types, and this one in particular has been designed to operate with this degree of feedback without running into instability.

It will actually stand even more feedback than this, but when tuners and control units are added, with their capacity for extra bass boost, there is always a risk of motor-boat-

AMPLIFIER WITH CONTROL UNIT



Here is the amplifier with the control unit No. 4. The two are connected by a cable and may be separated by several feet.

ing without extreme precautions and circuit complications with very little to be gained.

It is possible that, with the gain wide open, full bass boost, and the selector in a position which has no bass roll-off (the 78 position, for instance), there might be a tendency to motorboat in some cases. It is most unlikely to do so in either the Decca or EMI positions.

But no one in his senses would expect to operate the amplifier under

control with a judicious hand. If your motor car will reach 100 mph, you don't put your foot down without giving the matter some thought!

The sensitivity of the amplifier for full output is just under .3 volts, which is within the design limits we expect of the Playmasters.

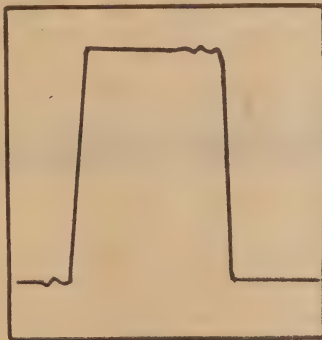
Despite this high sensitivity, the hum and noise level is no higher than with any of the others, remembering the extra available output. You don't build an amplifier like this in order to listen to it from a distance of six feet, but you would have to get closer than this, in all probability, before being conscious that the power was turned on. The total amount of noise is a little higher than with the lower powered jobs, but it is still low enough to be limited by the performance of the valves and perhaps the resistors used in the first stage.

RESISTOR NOISE

For this reason, it is a good idea, as it is with all the Playmasters for that matter, to use high-stability resistors in the EF86 plate and cathode circuits, as well as in the feed-back circuit. These can now be obtained, and we suggest you obtain them if you are very fussy.

Elsewhere in the circuit the gain is low enough for this precaution to be unnecessary.

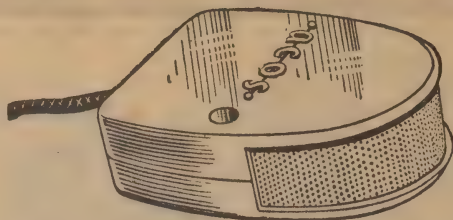
With the high-mu phase-changer, balancing the plate resistors for perfect amplifier balance isn't as important as with lower-mu valves, and with 5 pc resistors, the slight unbalance will only be observed on a full output test, where one sine-wave peak will flatten off a fraction before the other. It is hardly worth bothering about unless you are able to balance the amplifier with an oscillator and an oscilloscope, particularly as the design deliberately avoids using full output.



An oscillograph tracing of a square wave of 5 Kc fed into the input of the amplifier. It shows very little ringing or overshoot, and is appreciably better than that of most commercial amplifiers.

these conditions, which will allow the full 30 odd watts to be obtained with an input of 20 millivolts or less.

In fact, one of the precautions one must expect with a big amplifier like this is to operate the gain



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Approximate capacitance of the microphone is 750pF and cable capacitance will reduce output proportionately.

Frequency response Substantially flat from 50/5,000 cps.

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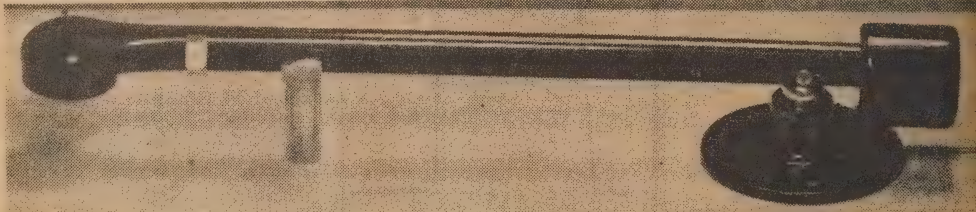
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The M.B.H. Pick-up is the only one on the market whose high frequency resonance is above 20 Kc/s. Thus with an M.B.H. wide frequency range can be enjoyed with a minimum of surface noise. Both private and professional customers have often stated that many discs which had previously been put aside as no longer playable, come back into service when a change was made to an M.B.H. Pick-up.

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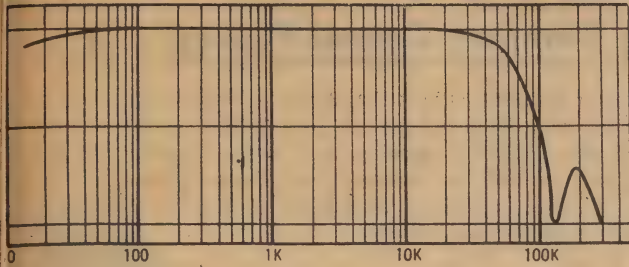
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GRAPH OF FREQUENCY RESPONSE



This graph shows the frequency responses of the amplifier with the transformer illustrated by the photographs. Distortion figures at operating levels are negligible as the amplifier is only 1 db down at 60 Kc. The slight fall at the low end is largely due to the bypass condensers on the output valves, but is in any case insignificant.

The output stage is operated under conditions advised by Mullard the EL34's. You will notice suppressors are used in both pentode and grid circuits. The latter is always a good idea with high-valve valves, but the valve makers at that linearity is improved using the screen resistors in addition to their value as a stability precaution, despite a slightly lowered output.

SEPARATE BIAS

Separate bias resistors are also used for these valves, not so much for the interests of low distortion as to allow each valve to adjust its bias if initial matching is not perfect, or if characteristics should vary with age, as they are almost certain to do.

The load requirement for the valves as pentodes is about 3-4000 ohms, and with high feedback and ultra-linear connection the exact value within reason isn't important. However, the optimum figure is given as 6600 ohms, and there are several 20 watt transformers of suitable type available in this range. As previously mentioned, there will probably be more of them soon, specially designed for this valve. There is, therefore, every reason to use them.

The power supply must provide a final high tension voltage of about 400 volts from the filter, allowing 32 volts of bias for the output valves and approximately 400 volts effective between plates and cathodes. To do this we have used a transformer wound for 400 volts per side at 180 mills which, when used with the GZ32 rectifier, gives almost precisely the required volts.

POWER RATINGS

This transformer has already been made by one manufacturer and will probably be obtainable in several months before long.

There is a type of transformer rated at 425 volts per side at 175 mills, originally designed for the Williamson circuit. This transformer is suitable, although you may have to parallel the filament windings to obtain efficient load distribution. This, again, will depend on whether the amplifier is used with a tuner or not.

In this case, it is advisable to use a pair of dropping resistors in

each high tension lead to the rectifier to reduce the applied voltage to 400, or to whatever voltage gives 440 volts from the filter. This should be considered the maximum permissible voltage, particularly with respect to condenser ratings throughout the equipment.

On this basis it is practicable to use the power supply from the Playmaster No. 1, in which this type of transformer was used.

Because of the high output voltage of 440 volts, it is too risky to use electrolytic condensers directly after the rectifier valve. A breakdown here would almost certainly

take the rectifier with it and might do other damage as well.

Fortunately, there are a number of paper condensers available through disposals sources for less than 10 shillings each which can be used in this amplifier.

The pair we used were rated at 8 mfd, 400-volt working, and there is another type rated at 4mfd, 600-volt working.

These disposals type condensers were almost invariably rated at a temperature of 140F, with a lower rating sometimes given at 160F. It is highly likely that a rating of 500 volts working at 70 or 80F would be quite normal for the 400-volt types, and there seems little reason

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consider them a risk with this
plier.

The 4 mfd types would probably
ply adequate filtering, and 8 mfd
uld be considered the maximum
ue to be used directly after the
filter.

It should be quite satisfactory to
a 600-volt peak electrolytic con-
denser in place of the paper type
connected after the filter choke,
ere there is virtually 440 volts DC
be handled.

As a general rule, these electro-
ics are suitable for DC operation
to 500 volts, so that there would
be a reasonable safety margin.

A capacitance of 16 mfd would be
ample.

There appears to be no direct sub-
stitute for the GZ32 type rectifier.

This is a type rather similar to
the 5V4G, but the makers have been
re generous with their ratings.

RECTIFIERS

The 5V4G would be over-run in
power supply on this basis, al-
though the GZ32 is often supplied
in place of the 5V4G for replace-
ment.

Directly-heated rectifiers such as
the 5U4G can be used in this am-
plifier, but the output voltage will
be less. The difference is only about
10 volts or so, but, being a directly-
heated valve, the supply voltage will
be to something like 550 volts un-
til the remaining valves have heated
up and begin to draw plate current.

This means that all the conden-
sers in the HT circuit in the am-
plifier, control unit and receiver are
likely to receive this voltage during
the warm-up period, and must there-
fore be not less than 600 volts work-

The GZ32, on the other hand, has
a slow warm-up time of 25 seconds,
and this is designed to be a longer
period than any of the other valves.
Consequently by the time the rec-
tifier comes into operation the am-
plifier is already warmed-up, and
the high tension voltage at no time
exceeds its operating value.

The makers do not require the
use of resistors in the transformer
secondary leads to the rectifier except
in a means of controlling voltage.

The amplifier has been built on
a new chassis, as none of the exist-
ing Playmasters will accommodate
the rather large components with-
out a margin to accommodate pos-
sible differences in size between dif-
ferent makes.

AIN FILTERS

The main filter condensers have
been placed away from sources of
heat, and there is enough room on
this part of the chassis to mount any
type you are likely to use.

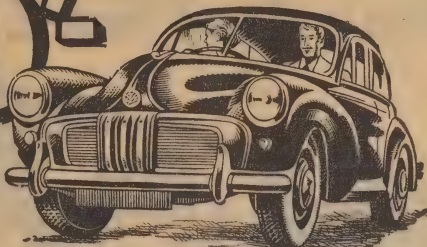
The power and output transform-
ers are mounted quite close to each
other, but their cores are exactly at
right angles to their centres. In
this position there is virtually no
inter-action between them, and neg-
ligible hum fed through to the out-
put.

They are, however, spaced as far
apart as the chassis will allow. No
cut-outs have been specified on the
chassis blueprints, as these would not
be suitable for all the components
which might be used. They should
be mounted with whichever orienta-
tion is most convenient.

The positions of the filter choke
and rectifier are clearly visible. The

(Continued on Page 57)

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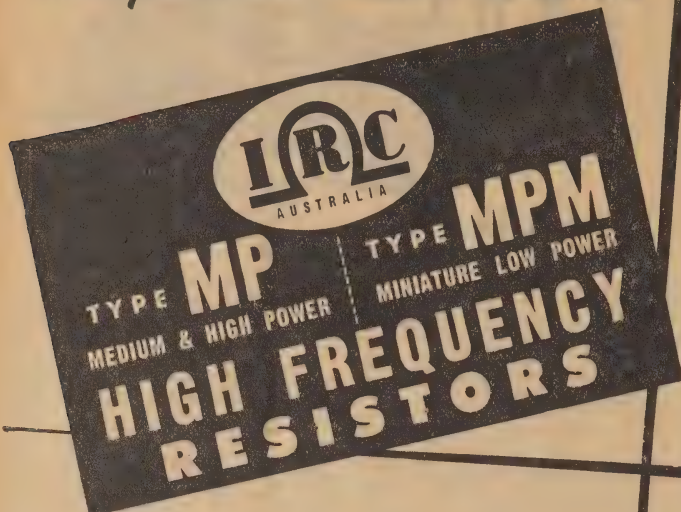
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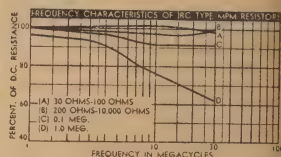
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MPJ	5 watts	1000	35 ohms	3.0 megohms	3"	9/16"
MPP	10 watts	1750	25 ohms	2.5 megohms	4-1/2"	3/4"
MPA	20 watts	2750	35 ohms	4.0 megohms	6-1/2"	1-1/8"
MPO	30 watts	4750	50 ohms	5.0 megohms	10-1/2"	1-1/8"
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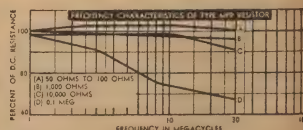


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Continuing his discussion of home-built electronic organs, the author this month passes on to an examination of tone-generating circuits using neon and vacuum tubes. Some typical commercial arrangements are reviewed with the possibility in mind of adapting them for home construction.

PART TWO

The use of neon tubes as general lighting and dividers has received a good share of attention over the years and patents on their application are being registered continuously and in relatively large numbers, going back to the past 30 years, or more. For commercial purposes the gas-filled tube — whether it be neon lamp or thyratron — is not satisfactory: there is too much variation and instability from tube to tube to make their commercial use a good proposition, and only one firm (an English one) makes any use of these tubes, and in this case to a limited extent, only.

However, for the home constructor the most satisfactory organs can be developed around this class of generator, and very pleasing results obtained. One such satisfactory instrument is Dorf's patented Electron 22n.

FREQUENCY DIVISION

A large proportion of commercial instruments, utilising vacuum tube oscillators, resort to frequency dividers as a means of saving on valves. However, a saw tooth wave is, more often than not, required at the output of each divider, and this calls for tuned circuits and special treatment when using vacuum tubes.

ny neon tubes are used, sawtooth wave forms are readily obtainable without involved circuitry. Furthermore, division of the frequency fed to the divider may, at the same time, be had, whether it be by two, three, four or some other integer. This fact is of considerable advantage, and it is well to be borne in mind when deciding upon what sort of a basis an experimental organ will be built.

The reader is asked to note that this is a general article about the subject of building electronic organs, and it is not proposed to give de-

tailed circuits. Such information may be had from Douglas' well known "Electronic Musical Instrument Manual", which also has a fairly good reference list, and forms a satisfactory foundation for the advanced study of this subject, more practical developments being given in his latest book "Simple Electronic Musical Instruments for the Constructor".

Also, providing contact is made through the editor of "Radio, Television and Hobbies", the writer is prepared to advise anyone interested enough to write, on the availability of specific data. In addition, certain firms advertising in this magazine are known to be approachable on the subject, and can probably give a fair amount of information on the availability of circuitry, data and components.

These main two advantages of the gas tube its ability to divide easily, and at the same time to provide a sawtooth output, weigh heavily in its favor for consideration by the home builder.

We now turn to a well-explored field, from which has sprung a bewildering array of devices—oscillators and dividers in all stages of simplicity and complexity — and we find ourselves wondering just where to start.

Since this article is addressed to people who are interested in building an instrument, it may be as well to glance over the various major commercial makes of electronic organs.

In the USA the most publicised are the Allen, Baldwin, Connsonata, Lowery and Minshall organs and in Great Britain the Constant Martin, Jennings, Lincoln and Maestrovox.

ONE TUBE PER NOTE

Of these Allen, Constant Martin, and Consonata use individual tubes per note of the instrument, the remaining makers resorting to frequency division in one way or another. It is interesting to note that the organs having one tube per note all use inductances for determining the various frequencies. Inductances represent a lot of work (or a lot of money) to have wound, and for this reason do not appeal to the amateur, although construction of such instruments is well within the capabilities of the hobbyist, and give, in general, a better return for the financial outlay involved.

Of the others, the Baldwin, Lowery and Minshall instruments represent a fair average representation of frequency division in practice.

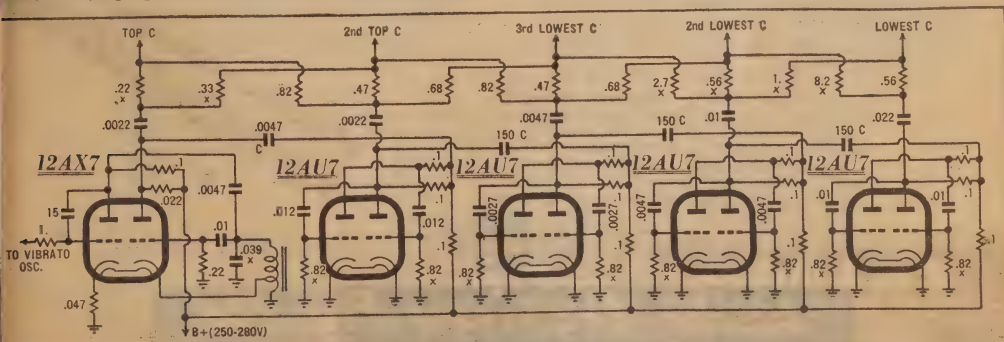
In the writer's opinion the Baldwin organ is the pick of the lot, being truly organesque in attack and tone.

It, however, presents two major obstacles to the would-be constructor: one of these is the method of keying which will be explained later, the other is the generator divider system which is demonstrated schematically.

In the Baldwin instruments all the notes of the one sign are generated on the one chassis, so that we have 12 chassis in all—one containing all the C's for the organ, another all the D's and so on.

Except for variations in the tuning elements of the master oscillator

by R. A. B.
Tarrant



Generator circuit for the notes "C" in the Lowery organ. Values marked "X" change for different notes. The 12AX7 is the master oscillator, the 12AU7's serving as multivibrators for octaves below. The circuit is foolproof and relatively simple even if 60 tubes are used!



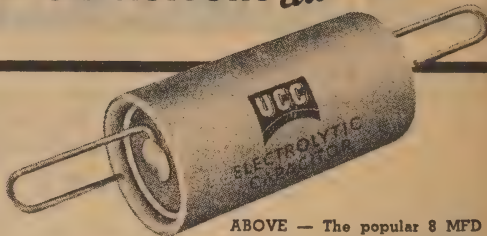
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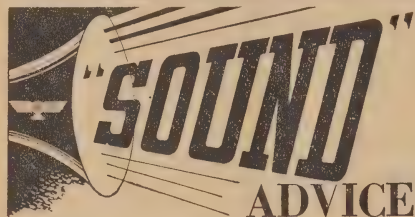
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each chassis, all 12 of the units identical. To give the reader an idea of the work involved in the construction of these units, reference is made to the circuit of one generator chassis—the C

the Baldwin Model 5, 6SN7GT valve used, 36 only being required for generation of all the notes. Both manuals and the 32 pedals, which are quite a considerable saving in tubes when comparing the possibility of construction of this type of instrument with, say, a Connata, of the same specification.

PRECISION REQUIRED

The master oscillator transformer the C notes has a turns ratio of 1:1. The turns ratios in this organ are critical, and very little error can be countenanced, particularly with divider transformers, which are critical for all the generators.

The windings for the multiple pulse transformer are on a common core, as follows. DT1 primary 3000, secondary 3000 (ratio 1:1), DT2 3600, 3600 (ratio 1:0.97), DT3 3750, 4000 (ratio 1:1.1), DT4 4000, 4000 (ratio 1:1), DT5 4000, 4250 (ratio 1:1.0625).

The frequency dividers are, in themselves, blocking oscillators—grid type—and it is in the employment of this system that the Baldwin organ is unique, the master oscillator serving as a synchronising pulse to keep the dividers in step.

This detail is given for the sole purpose of showing the reader what is up against since, 99 times out of 100, the instrument he finally decides to build will soundly based on some successful commercial organ.

However, while commercial manufacturers are always delighted to give general details of their products known—with the consequent ringing around of the name—they will not disclose the technological details, such as sizes of inductances and values of other components. This is where the experimenter starts his chain of headaches, unless he is fortunate enough to have access to certain manufacturers' information not normally available to the public.

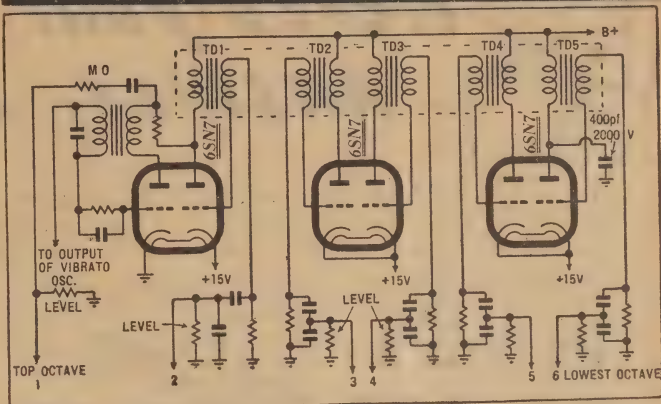
PATENT POSITION

Remember, too, that all these instruments are patented and that every facet of their generating and final system is legally protected. Therefore, to commercialise an instrument, the manufacturer has to ensure that he is not trespassing on someone else's domains and, as has been done in the Baldwin organ, he is at times resort to some most unusual electronic applications and twists in order to circumvent other established practices.

The key switching in this particular instrument, and now illustrated, is the unique system of obviating key clicks which was mentioned earlier in this article. Key clicks in the Baldwin instrument are practically negligible, and it is interesting to note that the registration tablets, stops are also switched in and out by similar resistance switches.

The effect is that, at the moment of making contact, there is a resistance of about $\frac{1}{2}$ megohm suddenly placed between the tone source and amplifier. Because of the compara-

GENERATOR—BALDWIN ORGAN



Generators for one note sign in the Baldwin organ. Transformers TD1 to TD5 are wound on a common core; design is critical and cost about £16 for each of the twelve units required. Resistors level the outputs 1-6, the signal being very rich in both odd and even harmonics.

tively large value of this resistance there is only a minor voltage surge with negligible current flow: the resulting "click" is inaudible, or virtually so. As the playing key is depressed, the contacting member is flattened down, gradually, along the resistive element, thus decreasing the resistance between its two ends in a regular manner. The result is that there is a gradual decrease in resistance, thus allowing the "volume" to build up.

PLEASING INSTRUMENT

The Baldwin is a particularly pleasing instrument and, if you can make-up the divider transformers and resistance switches or have them made for you, the major obstacle in copying it is overcome.

Of a quite different circuit configuration is the Lowery organ. This organ, a postwar development, also a fully polyphonic device (that is, chords can be played), is housed in the domestic piano, without, in any way, affecting the playing technique of that instrument.

In fact, the only indication that the piano is unusual is the fact that the Organo's controls are mounted just below the front edge of the keys, these controls being six pairs of tilt-type switches which allow the performer to have the right-hand end, the left-hand end or the full compass sounding. Another pair select the depth of vibrato and others the three main types of voice—horn (strident), string (rich in higher harmonics) and the stop which the makers label "principal", but which, in the writer's opinion, has no relation to this four-foot pipe organ stop of the same name.

It is, at best, a flute-like tone with a tendency to richness in the upper harmonics. Each of these voices may be sounded either loud or soft, such choice being put into effect by depression of a "piano" or "forte" tablet.

The reason that mention is made of the Organo is that it is an instrument unknown in Australia and New Zea-

land, and, having no unusual circuit features, it may be assembled by the home builder with not too much trouble. However, it uses one valve per note—48 12AU7's and 12 AX7's in the model known to the writer—in the generators alone (later models use 12AU7's only).

As an indication of how simple, or otherwise, an organ design can be (and please note that the author has NOT built-up the circuit, which was obtained from the manufacturers—Central Commercial Industries Inc., 332 South Michigan Av., Chicago 4, Illinois, USA), a circuit of one frequency dividing network is shown, this being for the note C, the highest in the chain being labelled No. 1, the lowest No. 5.

SWITCH OPERATION

In common with the Minshall organ all outputs are grounded in the "off" position. If a note is to sound, then depression of the playing key removes the earth connection, thus allowing the signal from that output to go on its way to the tonecolor filter circuit, which, for simplicity, takes some beating.

A number of other commercial instruments—both British and American—follow this general pattern of master oscillator followed by frequency dividers, the resulting outputs being boosted, attenuated and filtered through degrees of R, C and L stages either singly or in combination.

The only exception is the Minshall Organ which, too, follows the above plan. However, in the Minshall, the tone-forming circuits are unique in that no resistances, capacitances or inductances are used as such in forming the tones. Without going into a detail of the theory of operation, it can be seen that here we have an organ which may be built up by the amateur with very good prospects of success—due in no small measure to the relatively cheap construction costs involved.

The cost of all tubes involved is in the vicinity of £40.

To be continued.



Here's your answer, Tom!

Many a problem has been raised and dealt with in these columns but we doubt if Tom's initial question has come up before. They say there is always a first time but we were taken somewhat aback, when Tom brought up a question, which clearly belongs to the realm of Romance.

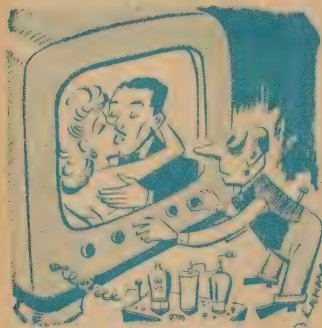
OR is it merely a spelling error, we wonder? Anyway, here it is.

Could you explain the difference between an Oscilloscope and an Osculograph? And what is an Osculogram?

Of course, Tom, it may only be a spelling error. But the trouble is that there is such a thing as an "oscilloscope" in the field of electronic science.

We refer to the television set, a piece of apparatus which will soon be familiar to our readers.

You see, Tom, "osculoscope" is



An osculoscope . . . !

actually a hybrid word, coming partly from Latin and partly from Greek. "Osculare" means . . . to kiss in Latin; "scopein" means to see, or in many cases, to make visible, in Greek. In other words, we have a machine which makes kissing visible!

From what we have heard of American TV programs, such an occurrence is by no means a rarity on the TV screens of that country.

Similarly the words "graphein" and "gram" mean to draw, or the drawing itself. Hence an osculograph would be a machine which draws a picture of that well known expression of affection, while an osculogram would be a permanent record made by such apparatus.

However, just in case you did get your spelling mixed up a little, Tom, we add at this juncture that there is a very similar word in Latin, "oscillare", which means to move to and fro.

Although the TV receiver is not generally known as an osculoscope,

a very similar instrument is familiar to many, who have something to do with electronics. This instrument is the oscilloscope, which, as its name implies, is used to present a visual pattern of oscillations or variations in electric potentials.

After what we said previously, Tom, it should not be too difficult for you to discover that an oscillograph would be a machine which makes a permanent record of such oscillations, while the oscillogram would be the record or picture made by just such a machine.

But let us leave the realm of romance and turn our attention to questions more appropriate to the pages of this magazine. Tom's next question concerns Absorption Wave-meters and Grid-dip Oscillators, no doubt prompted by a recent article on the subject.

Could you tell me what is the essential difference between an absorption wavemeter and a grid-dip oscillator and how do they work?

Well, Tom, both instruments are actually used for the same purpose. This is to determine the resonant frequency of tuned circuits, frequently those used in transmitters. The degree of accuracy obtained will, of course, depend on how accurately the instrument is calibrated, although in most cases an approximate indication is all that is required.

We can describe the essential difference between an absorption wavemeter and a grid-dip oscillator in very simple terms: the first is actually a simple receiver with a calibrated scale, whilst the second is a simple transmitter. Let us explain a little further.

ABSORPTION WAVEMETER

The absorption wavemeter consists of a variable capacitor, a coil, and a small torch lamp, all connected in series. If the coil is brought near say the tank coil of a transmitter, current will be induced in it. Tuned to the frequency of the transmitter, the current in the circuit will be sufficiently strong to make the torch lamp glow.

When this occurs, the frequency can be read off the dial.

You will notice, Tom, that the power required to light the lamp is derived or absorbed from the transmitter. The instrument therefore acts as a receiver.

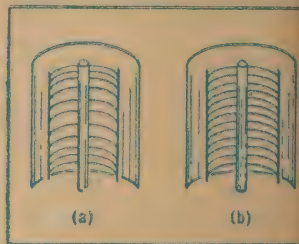
On the other hand, the grid-dip

oscillator supplies the power itself. Its main components are an oscillator valve, a meter, and a tuned circuit consisting of a coil and a variable capacitor. The tuned circuit, of course, is used to vary the frequency of the oscillator.

The meter is connected in the grid circuit of the oscillator, measuring grid current, and thereby giving indication of the strength of oscillation. Now, the amount of power available from the instrument is very small, and if some of it is absorbed by an outside circuit, the meter will be an obvious drop in the strength of oscillation, indicated by the meter.

The coil on a grid dip oscillator is mounted outside the instrument case, to enable it to be coupled to another coil by bringing it close to it. When both are tuned to the same frequency (this is done by varying the frequency of the oscillator) there is a pronounced dip shown on the meter, as power is absorbed by the outside coil. The frequency is then again read from the dial.

Sometimes, as in the recent "R,"



Grid construction for (a) a variable-mu and (b) a sharp cut-off control grid.

& H Grid-dip Oscillator", a meter is used instead of a meter to indicate the dip.

So much for that. And now the next question.

How does the valve engineer achieve the different characteristics and cutoffs for the different valve types? Does he just sit down and work out everything on paper, or does he determine them experimentally?

To put it bluntly, Tom, he does a bit of both. Or rather he does lots of both! Designing of valves is an extremely tricky business, and

of work has to be put into prototype, before the valve can into production.

Needless to say, today's valve engineer has all the experience gathered in the production of many thousand valve types, at his disposal. He therefore knows what general type of valve will give him the required characteristics, and relies himself the tremendous amount of basic research that would otherwise have to be done.

Now valve characteristics mainly depend on the physical placement, in relation to each other, of the valve electrodes. If a request comes through for a valve of certain characteristics, the valve engineer selects a valve of the same general characteristics and proceeds to modify its electrode structure. The general effect of certain modifications is known, so that he can predict that the new prototype will have different characteristics in these respects.

ST PROTOTYPES

A small number of the prototype made up and tested, to see if the modifications did change the characteristics to the desired extent. After perhaps several changes and tests the desired characteristics are achieved and a pilot batch of valves produced to see if production methods are suitable for the new type.

Naturally, the valve designer has to take into account whether the proposed new type can be produced within suitable tolerances with existing facilities.

Let us say, for instance, that a designer wants to produce a valve which, besides other characteristics, is required to have a gradual cutoff, or, as it is generally known, a remote cutoff. The starting point might be a valve which has characteristics very close to those desired, but is a sharp-cutoff type.

These types have a control grid of uniform pitch. In other words, the spacing between the grid wires is equal throughout the length of the grid. Remote cutoff valves have grids which have widely spaced wires near the centre, the spacing becoming gradually less toward the ends.

FURTHER TESTS

Accordingly, the valve engineer makes up several valves, each with a different grid spacing, and subjects them to tests. The one giving the most favorable characteristics is repeated and improved further, until it has the required cutoff slope. Pilot production runs then prove if the valve can be mass produced, and there the designer's job largely ends.

There is no doubt, Tom is keeping up with the times. He has even discovered that there are transistors! What more, he wants to know—anyway, here is his question:

What would be the correct value of negative grid bias for transistors?

You must still suffer from the illusion, Tom, that transistors are identical in every respect to ordinary vacuum tubes. Nothing could be further from the truth!

We could not state any grid bias values for transistors, Tom, even if we wanted to. You see, transistors just haven't any grids. Nor have they any other electrodes identical to valve electrodes.

At the best, one could say that certain elements in the transistor carry out functions similar to valve electrodes in a triode. As a rough comparison it could be stated that the emitter corresponds to the cathode, the base to the grid, and the collector to the anode. There, however, the similarity ends.

Unlike valves, the transistor does not depend on electron passage through vacuum for its operation, but on the movement of electrons in solid matter. It is therefore understandable that their mode of operation and their behavior is vastly different from that of valves.

CORRECT VOLTAGES

However, as with valves, the voltages applied to a transistor have to be in certain relation to each other for correct operation. Hence, it would be quite futile to quote one voltage as being universally correct, whatever the other voltages may be. It would have to be calculated for any particular operating condition, with the aid of data published for any particular transistor.

We suggest you re-read some of the articles we have published recently about the use of transistors.

And lastly, here is a problem which no doubt has mystified many a budding radio enthusiast.

What do trimmers in a receiver do and how do they do it?

Trimmers, Tom, are small variable capacitors with a maximum value of somewhere between 30 and 50 pf. They are used in applications where it is necessary to have several circuits tuned accurately to certain frequencies, such as for instance the tuning circuits of a receiver.

These circuits are usually tuned over a band of frequencies by means of ganged tuning capacitors, which are actually two or more variable capacitors mounted on a common shaft. Ideally these sections should all have the same capacitance.

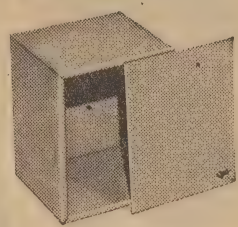
MASS TOLERANCES

In mass manufacturing processes, however, such close tolerances cannot be achieved, and it is quite likely that you will find a difference in capacity of 2 or 3 pf between individual gang sections. Furthermore it would be quite impossible to make all connections to the gang identical, while shunt and stray capacitances across the coils may also cause considerable differences in the total capacitance of the tuned circuits.

Unless the capacitances are equal, the circuits will not be tuned to exactly the same frequency and some form of compensation must be applied to them.

This is usually done by connecting a small variable capacitor, a trimmer, in parallel with the gang sections and adjusting them until each circuit tunes to exactly the right frequency.

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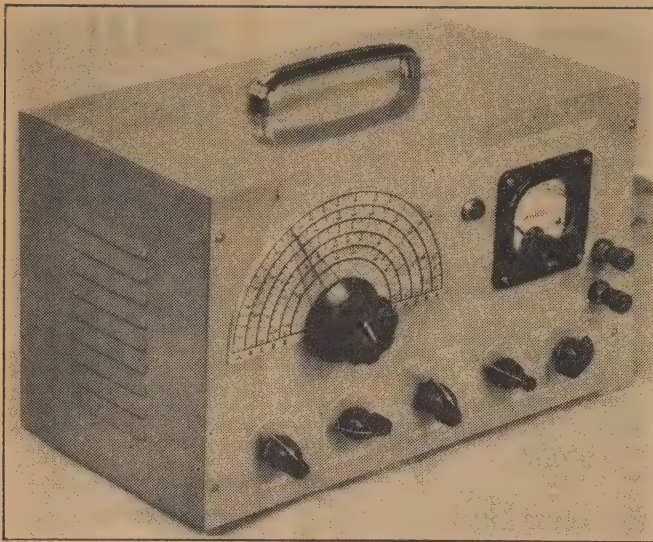
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A photograph of the completed instrument. Our scale was in etched metal, but a celluloid-covered cardboard scale would look good.

AN AUDIO SIGNAL GENERATOR

In last month's issue we published details of a new audio generator and the considerations upon which the final design were based. This month we publish full details of the construction of the generator and the calibration procedure.

PERHAPS the easiest way to tackle the actual building of the oscillator is to construct it in sections in the same order as was described in last month's issue.

The general layout of the Wien Bridge oscillator section can be seen from the photograph of the top of the unit (figure 3) and from the coded under-chassis photograph, (figure 4).

The two-gang condenser, which is a Philips miniature type, needs to be insulated from the chassis since the frame is connected to the first valve grid.

MOUNTING RODS

Our method of doing this was to obtain some 3-8in diameter polystyrene rod and to drill and tap a 1-8in Whitworth hole through it, to take mounting screws in each end. Three such pieces will be required, each 5-8in long. These are affixed to the three mounting lugs on the condenser frame.

Two large holes were punched in the chassis immediately under the condenser to take the connections through the chassis. By maintaining adequate clearance between these leads and the chassis any possi-

bility of leakage currents through poor insulating materials is avoided. Stray capacitance is also minimised.

The lead from the gang frame was soldered to the gang mounting bracket and not the actual frame, which is of a cast metal and will not take solder.

Because the gang frame is 'hot', an insulated coupling is required for connection to the control spindle. Here again, some care should be taken in the choice of the component. A ceramic type is to be preferred if available, although the moulded plastic type appear to be quite satisfactory.

The coupling should be of the flexible type to prevent strain being placed on the gang shaft. Care taken in the alignment of the two

shafts will be repaid in long life and stability of calibration.

The dial shaft must be bushed where it passes through the front panel and the bearing from 80 types of potentiometer can be pressed into service.

As the whole of the gang has to be shielded to prevent hum pickup, an aluminium screening box was constructed to cover the gang (see figure 2). This screen needs to be spaced well away from the gang to minimise stray capacitance.

CAPACITANCE BALANCE

This capacitance appears across only one side of the bridge network, and, to maintain balance of the network, additional capacitance must be added to the opposite side. In so doing the ratio of the minimum to maximum capacitance is reduced.

This, in turn, reduces the range of frequencies which can be covered in one range and so must be kept to the minimum possible. The balancing capacitor is the air trimmer shown in the underside photograph near the rear of the oscillator compartment (figure 4).

Other types of two-gang capacitors could be used but most of them are generally available do not use ceramic insulation and are larger physical dimensions. The larger dimensions make it more difficult

to keep the stray capacitances to a minimum.

The range switch used was of the ceramic type to minimise leakage resistance. If a normal type was used, switch has to be used several precautions are well worth taking.

The leakage path from the metal side screws to the switch contacts is normally very short, the retaining nuts often being in close contact with the surface of the wa-

LEAKAGE PATH

This length of leakage path can be increased by fitting longer screws and using short lengths of polystyrene tubing on them to stand the nuts well off the surface of the wafer. The surface of the switch should be clean and free of any flux deposits.

As the resistors used on all ranges other than the lowest were single resistors, it was convenient to wire these directly to the switch at one end. The lowest range, up to two 10 megohm resistors in each section of the Wien Bridge network and for the anchor points of the resistors, miniature ceramic star-off insulators were used.

The preferred type of resistor for these frequency-determining

by Reg.
Rawlings

Depending on which of the restorers is the higher or the lower, the circuit will tend to oscillate more or less fiercely than on other ranges. While the automatic amplitude control may take care of this, it does not limit the range of control left to the operator to take care of other variables.

Not only should this value be kept small, but held constant. For this reason a change was made in the wiring after the photograph (figures 4 and 5) were taken. Instead of using flexible 10/010in plastic covered wire for these leads, solid 20 SWG tinned copper covered with sleeving was used. This was spaced well off the chassis to keep the capacitance low.

The screen under the oscillator compartment was secured in position by means of three screws. These screws were tapped into three pieces of brass rod, mounted on the chassis. These can conveniently be made from lengths of $\frac{1}{4}$ in brass rod. Each

Fig. 1. The complete circuit diagram of the Audio Generator. The various sections were discussed in last month's issue and in the above circuit they are combined to give a complete instrument.

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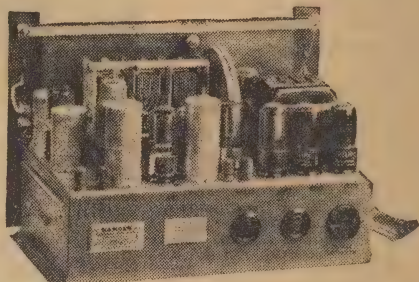
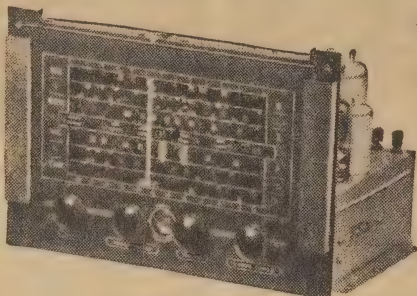
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TOP VIEW COMPLETE OSCILLATOR

ce needs to be about 1-15/16 in. and is drilled at either end and typed 1/8 in. Whitworth.

The rest of the oscillator section is quite straight forward and, provided small components are used and the valve sockets are mounted in the same direction, no trouble could be experienced.

All the valve sockets in the equipment are mounted in the same direction, that is with the space between the pins one and nine toward the oscillator end of the chassis. The valve sockets used were the mica lead ones now available.

The centre portion of the chassis contains the square wave shaper and the valve voltmeter. The shaper is the nearer to the front panel to keep the lead lengths from it to the one/square switch short.

SMALL RESISTORS

Grid and cathode resistors are wired directly from the valve socket pins to earth lugs secured under one of the valve socket mounting screws. By using the BTS type of 1-watt resistors very little room is taken up by these components.

The plate loads for the squarer are wired from the valve socket pins to the tag strip and on the tag strip itself. This tag strip can be seen between the squarer and oscillator sections.

The valve voltmeter is toward the rear of the chassis and its associated germanium diode is wired directly across the tag strip between the squarer and cathode follower sockets. The grid return resistors are also taken to this tag strip.

The input grid of the valve voltmeter is switched to earth through a 1 megohm resistor in the extreme anti-clockwise position of the coarse attenuator to permit the meter to be set to zero. This resistor is bypassed by a .005 mica condenser to prevent it pick up of stray voltages on the two highest frequency ranges.

VOLTMETER SWITCHING

If the voltmeter is switched directly to earth without the resistor, the .5 input condenser is suddenly discharged and the meter receives a large surge current. By discharging the condenser through the 1 megohm resistor this surge is limited without unduly increasing the time the meter takes to settle down to zero.

As was mentioned in last month's article the output of the sine and square waves from the oscillator are made to have equal peak value. If the valve voltmeter was truly peak reading, the meter would read the same for the sine or square waves output.

However some energy does leak away from the .5 input condenser through the diode load and back to earth. The result is that the voltmeter does read some 10 or 15 per cent higher on square waves.

No components are mounted under the filter chokes at the rear of the chassis and in fact all components in the instrument are readily available if service is required at any time.

The cathode follower stage is the next valve along the chassis and is the type 6BW6. The effective cathode bias resistor in this valve is the 1000 ohm resistor. This value was chosen

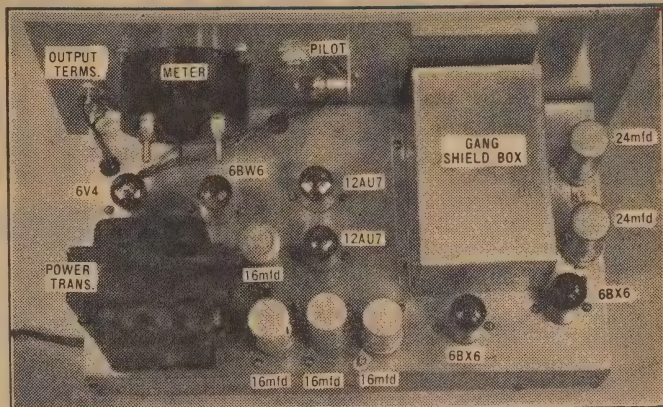


Fig. 3. A top view of the instrument showing the placement of the main components.

to keep the B-plus drain to a reasonable figure and also to make the attenuator values easy.

The fine output level control immediately in front of the 6BW6 and the coarse output attenuator is the last control along the front panel in front of the rectifier socket.

The resistors, for the coarse attenuator are wired either directly to the switch or are in close proximity to it. The output electrolytic condenser is immediately behind these resistors, and a further ceramic in-

feeding the cathode follower, as this will cause hum voltages to be fed back into the oscillator section.

As was mentioned in the first section of this article last month the whole construction of the instrument, with the exception of the case was in aluminium to avoid hum troubles. Subsequent to taking photographs of the instrument, a bracket was fitted to the rear of the chassis projecting downwards. When the instrument is in its case this bracket supports the weight of the power supply without placing strain on the front panel.

At this point, a word about valve types would be appropriate. As we were starting from scratch, we used those types that appeared from the data sheets to be the most suitable for the job. However there are other types which, if they are already on hand, may be suitable.

VALVE TYPES

The first limitation on valve types is their size, and it is doubtful if other than miniature types could be used in the oscillator section without changing the size and layout of the chassis. In the other positions it might just be possible to accommodate some "GT" sizes.

The valves in the oscillator section must be high-gm type television pentodes. Those used were 6BX6/EF80 which types the valve companies assure us will be standard for TV applications. Other currently available miniature types which may be satisfactory are the Z77, 6AC5 and the 6AM6/EF91.

Some of the earlier high-gm types such as the 6AC7 and EF50 might also be satisfactory if the layout is altered to accommodate them.

The requirements of the squarer stage are less stringent and the valve used is the low- μ double triode type 12AU7. A suitable substitute for this would be the 6SN7. Much the same remarks hold good for the valve voltmeter section which, in our instrument, is a 12AU7.

The cathode follower stage which,

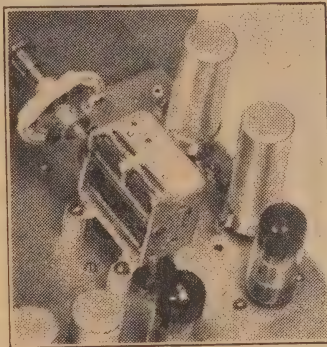


Fig. 2. Details of the gang mountings and the insulated shaft coupling are clearly shown in this photograph taken before the gang shield had been fitted.

ulating post supports one end of the condenser.

The power supply section is quite standard. Providing the upright type of transformer is used and the pair of 25 ohm resistors placed across the filament supply, no difficulties should be experienced with hum voltages and locking in of the oscillator at mains frequency or multiples of it.

No attempt should be made to eliminate the separate filter section

MAGNETIC SOUND INDUSTRIES

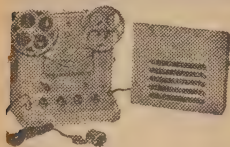
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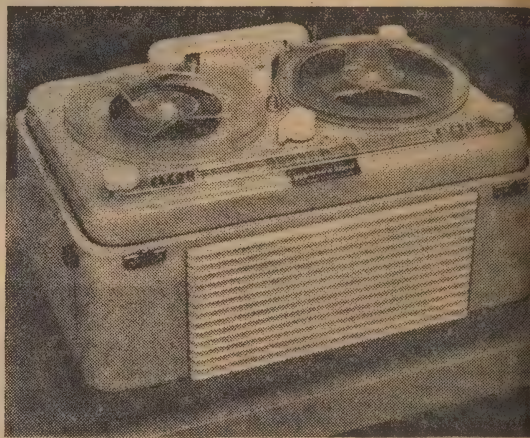
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our case is a 6BW6, can be any input pentode of similar characteristics. The 6AQ5 miniature type or the 6V6-GT could thus be used. One of the types mentioned above is of the high-gm type. In general, we have had much better results with low gm output valves in cathode-follower stages.

The rectifier valve, which is the most critical of all, is a 6V4. However, types 6X4, 6X5, 5Y3, &c., would be satisfactory.

So much for the building of the oscillator itself and the possible variations. Now for the calibration procedure.

CALIBRATION

Calibration of the oscillator consists of comparing its output frequency with that of a known standard. This standard may be any suitable oscillator covering the required ranges.

Because of the wide range of our oscillator, in all probability two other oscillators will be needed, for example an audio oscillator to cover the lower ranges and a RF or modulated oscillator to cover the higher ranges. Further, at the extreme low frequencies, the mains frequency can be used as a standard and at the extreme high frequencies a radio receiver can be used.

Before the final calibration is attempted the small oscillator trimmer capacitor must be adjusted to give the desired frequency at the top end of the ranges. This is best done in the range for which the most reliable standard is available as the setting is common to all ranges and only needs to be set on the one range.

If care has been taken in the construction to keep down the stray capacitances in the oscillator section this trimmer should require to be set at about half full capacitance. In this position a frequency ratio from the low end of a range to the high end should be in excess of 10 to one on all but the highest range. Once this trimmer has been correctly set it should be sealed.

LISSAJOU FIGURES

The most convenient means of comparing two low frequency oscillators is to feed one signal to the X plates of an oscilloscope and the other signal to the Y plates. In this way Lissajou figures can be obtained and, from their pattern, the frequency ratio between the two signals can be determined.

If the pattern is a circle or ellipse the frequency ratio is 1:1. If the pattern is a figure 8, the ratio is 2:1; a three loop figure is a ratio of 3:1. After this it is much easier to note the points at which a stationary pattern is obtained rather than count the loops. A copy of the scale obtained with our oscillator is reprinted in Fig. 7 and will give the reader an idea as to where the various calibrations should occur. While individual instruments will vary, the general scale shape will be the same.

If the calibration of the higher frequencies is being carried out using a signal generator the small mixer and demodulator shown in Fig. 7 will be of considerable help.

When the two frequencies fed to this unit are nearly identical, a beat note will be heard in the output of the audio amplifier. This will also occur when the harmonics of one of the signals is nearly identical to that of the other signal.

WIRING OF OSCILLATOR SECTION

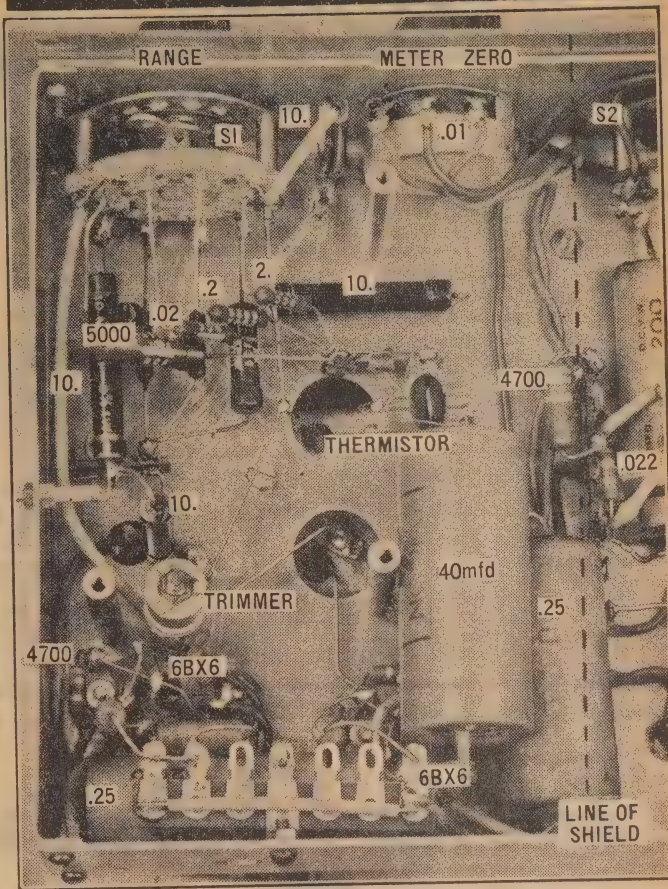


Fig. 4. A detailed photograph of the underside of the oscillator section with the shield cover removed. The large holes for the leads from the gang condenser can be seen to the left of the 40 mfd feedback condenser.

By switching the audio oscillator to the square wave output position a harmonically rich output is obtained. Even though the shape of the output square wave deteriorates above 10 or 15 Kcs., the squarer stage is sufficiently overdriven to produce a wave having a high harmonic content at all frequencies.

If the RF oscillator being used has a modulation switch, this should be turned off to enable the audio beat note between the two RF signals to be heard more clearly.

In the absence of a suitably calibrated RF signal source, a radio receiver can be used to tune in the output frequency of the oscillator directly or to tune in the harmonics of the oscillator output.

The coupling for the oscillator to the receiver is made by a very small capacitance. This can conveniently be done by twisting a lead from the oscillator around the aerial lead of the receiver without making actual metallic contact.

A receiver having a frequency coverage down to 150 Kcs. is particularly useful for this calibration

work and in our case we put into service a wartime AR8 which was ideal for the purpose.

At this point a few remarks are in order as to the method of making the dial for the instrument.

For marking the calibrations a single sided prespex cursor is required in preference to the one which will finally be used with the instrument. This allows the points to be more accurately marked on the white card which is fixed temporarily to the instrument.

SCALE MARKING

Once the calibrations have been made on this card it can be removed and marked in Indian ink. However the following method gives very much improved results.

The calibrations and their frequencies are marked lightly in pencil on the card. The card is then removed and photographed and a print made twice full size.

On this print the points are marked in with Indian ink and letters and figures from magazines cut out and stuck on to the print. This is

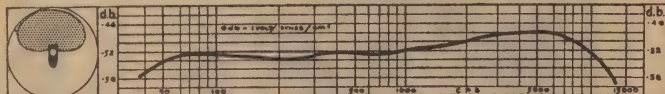
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en photographed and a print made of original size. Because of the photographic reduction and the use of printed letters the final result is very good.

We went one stage further than this and had made from the vice full-scale printing block reading the correct way. The figures and letters (which are recessed) were then filled with black wax and the surface polished and lacquered. The final result was a very professional looking scale.

It remains now only to calibrate the valve voltmeter to complete the instrument.

On test, the use of a germanium diode was found to give very good nearity in the voltmeter, even though the full-scale deflection corresponds to only some ten volts.

Its small physical size makes it easy to fit into the chassis, and it requires no heater supply. Its maximum reverse voltage is only 50 volts compared with much higher value for thermionic types. However, in a fixed circuit position, as in this oscillator, this limiting condition is not reached.

If a germanium diode is used on the probe of a valve voltmeter, care must be taken to see that it is protected against accidentally applied voltages in excess of the maximum permitted.

VOLTAGE CALIBRATION

For those of our readers who do not have accurate voltage calibration facilities, fairly good accuracy can be obtained by using a meter already fitted with a 0-10 scale. The valve voltmeter full scale deflection is then merely set to a known 10 volts. The lower points on the scale can then be taken as near correct. This avoids the need to calibrate each individual point and then draw up a special scale.

The resistor which sets the full scale sensitivity of the valve voltmeter is the resistor in series with the meter. In practice, the value of this is about 8-9,000 ohms, and could be made up of a fixed value of 5,000 ohms in series with a wirewound potentiometer of the same value.

If it is desired to put in the preset control a small bakelite panel can be made and mounted across the rear of the meter. Once the control has been set to the desired position, it should be fixed with sealing wax or other sealing compound.

GENERAL UNDERCHASSIS WIRING

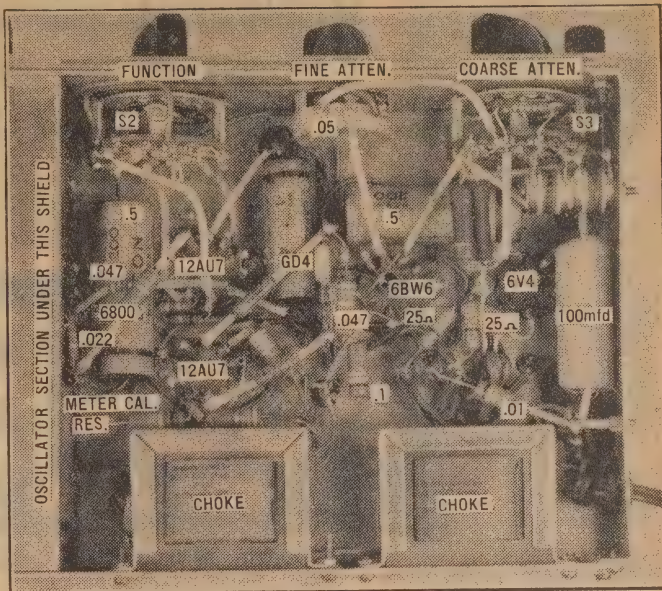


Fig. 5. A photograph of the underchassis wiring of the other circuits in the oscillator. The coarse attenuator is in the top right hand corner of the chassis with its associated resistors mounted behind it.

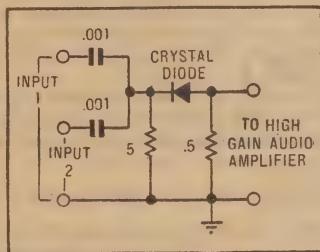


Fig. 6. The circuit diagram of the mixer/demodulator used for the calibrating of the oscillator higher frequencies.

Whilst a 0-10 scale can be used, it is preferable to be able to read voltages slightly above 10 and also to have a db scale.

This db scale is particularly useful when adjusting the feedback on audio amplifiers. The output of the amplifier can be set to a constant reference output and the amount of feedback in the circuit determined from the db's difference in input required to the amplifier with and without feedback connected.

This is read directly off the meter scale in conjunction with the coarse attenuator. Each "times ten" position on this attenuator correspond to an increase in the output voltage of 20 db.

In this regard it would be well worth the trouble to calibrate the coarse attenuator in db steps also. We have taken the db zero reference points as 1 millivolt so that the times one position should be labelled 0db, the times 10 position plus 20 db times 100 position plus 40 db and the times 1000 position plus 60 db.

METER RESISTOR

We arranged the meter to read 11 volts full scale with the coarse attenuator switch in the maximum position. As this position of the attenuator is marked X1000, the scale of the meter was marked as 11 millivolts full scale. Thus at any setting of the attenuators, the output voltage of the oscillator will be the meter reading in millivolts multiplied by the coarse attenuator setting.

Once the value of meter series resistance for the required full scale deflection had been determined, this was measured and replaced with a fixed resistor of the same value, and wired in position under the chassis.

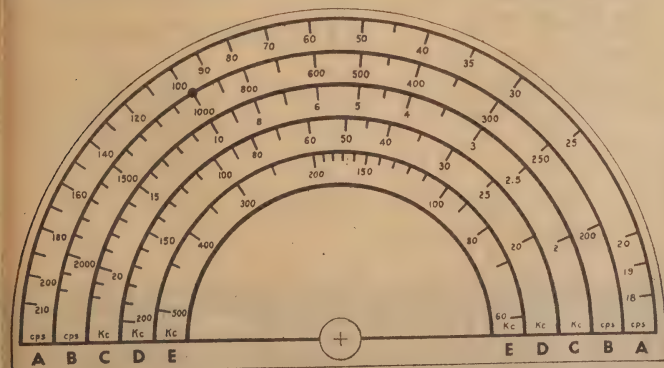


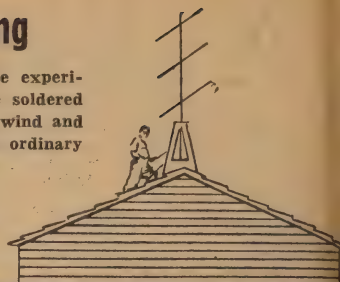
Fig. 7. This is a reprint of the scale that was obtained with our oscillator and will serve as a guide to readers when calibrating their instruments.



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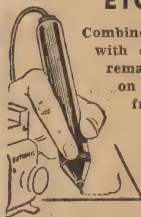
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A HIGH POWERED PLAYMASTER

(Continued from Page 41)

ke need not have more than 10
series inductance, with a current
ing of 180 mills. Its orientation
is not appear to be important.

ncidentally, this 180 mill rating
plies only if a tuner is used which
y draw up to 30 mills. The overall
uin of the amplifier and control
it is about 150 mills.

The amplifier itself is so arranged
to proceed in a fairly balanced
out from the input at the left to
output at the right.

When this version was built we
had some indecision about the posi-
tioning of the first two sockets, but
the final blueprint will show them
situated on a line which runs between
the two output valves.

COUPLERS

The two electrolytics near the input
sockets are decouplers for the control
unit and for the plate circuits of the
first two valves. The two 5-watt
resistors in series make up the series
resistor of 10,000 ohms.

If no tuner is used this value must
be increased to limit the voltage
applied to the control unit to 250
volts.

The tag strip on which these resis-
tors are mounted also terminates
the plate and grid resistors.

Between the 12AX7 and the EL34s
will be seen the grid coupling con-
densers, the .1 condenser earthing
the 12AX7 grid and the two cathode
bypasses for the EL34 bias resistors.

The resistors themselves are car-
ried forward to another tag strip so
that their heat will not warm up the
electrolytics. The screen suppressors
are also connected to this tag strip.

The grid resistors and suppressors
for the output stage are supported on
a tag strip on the input side of the
sockets, the cathode resistors also
being mounted here at the cathode
end.

The voice coil output connection
for this transformer is toward the
rear of the chassis and the feedback
resistor with its bypass is mounted
on a small strip near it.

An even better mounting for the
output and power transformers would
have been to orientate their cores by
90 degrees, which would have given
shorter plate and screen connections
for the EL34s.

FILTERS

The filter condensers we used were
fitted with flange mountings so that
their connections came through holes
in the chassis. This made connections
to them easy.

It would be permissible to reduce
the size of the chassis if your own
components will allow, although you
will find it hard to cut much off any
measurement if you are to avoid
magnetic or heat interference be-
tween the components.

When wiring the input stage see
that the input lead and the cathode
earth connection are made to the
same point on the chassis, to avoid a
possible earth loop which might in-
troduce hum. It is quite a good
scheme to use a heavy length of
copper wire for common earthing.



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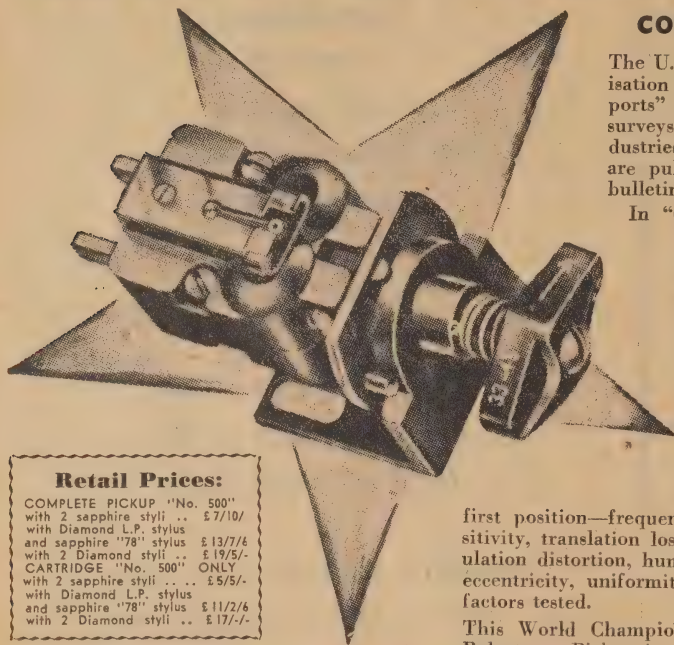
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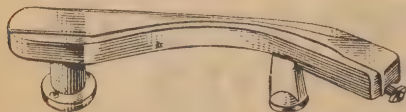
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Vol. 20, No. 6, there is a special report on "HI-FI PICKUPS" in which the 26 leading magnetic and crystal pickups are investigated. Only magnetic types were found to have the frequency range necessary for High-Fidelity.

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FROM THE SERVICEMAN WHO TELLS

At the risk of seeming monotonous I am detailing another good deed story this month. Fortunately it is a little different from my previous emergency calls. From my more regular case histories I have an unusual case of intermittent hum and set failure.

BUT before delving into these technical stories I want to comment on the recent discussion in these columns on the merits and demerits of various receivers from a servicing angle. Since most readers appear to have had their say I think I can only "sum up" and perhaps add my own opinion. What started as a straight out criticism against a design from a servicing angle (which was quite natural) into criticism from both the customer's and the serviceman's angle, even though the customer's case was put by the serviceman.

ALL TO BLAME

One point appears to be quite beyond doubt. Whatever criticism there is, it may be levelled equally against the better known brands and the obscure manufacturer. With this opinion I am forced to agree. In fact, I sometimes feel that the obscure manufacturer, by sticking to standard practice and avoiding "smart" designs, produces a more reliable set than some of the branded types.

This is particularly so in the case of dial mechanisms. As already indicated by readers, many of these leave much to be desired, both in reliability and in their actual functioning. This is mainly because manufacturers have tried to produce fancy dials which look very nice from the front, but call for an unnecessarily complicated mechanism.

The simple dial scores "hands down" every time.

I also agree that pigtailed twisted wires are a "pain in the neck" in anybody's language and appear to serve no useful purpose. On the contrary they can effectively hide a faulty joint which would otherwise be obvious.

CORE TROUBLE

Likewise, I have had trouble with coils using threaded iron cores in a threaded former. This idea was used many years ago when iron cores were first introduced, but was dropped smartly when similar troubles were encountered.

However, I don't feel that the manufacturers are to blame for such things as sale of sets without an RF stage in districts which are obviously unsuitable. This is a matter for the salesman and, ultimately, the customer to decide.

In the matter of form wiring versus point to point, I imagine there may have been some confusion. Just because F.J.C. expresses a preference for point-to-point wiring I don't think it automatically follows that he condemns form wiring.

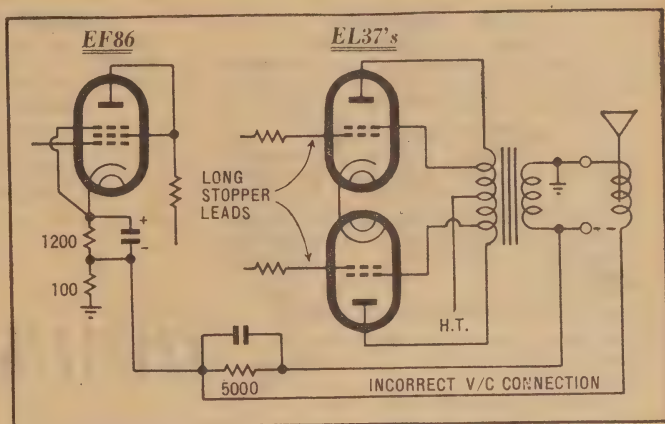
Rather, I imagine, he is condemning the sloppy type of wiring job that cannot really be classified at all, at least not in print.

Also, there does seem to be a very real need for some manufacturers to study the problems of tropical operation, particularly as most sets are designed and built elsewhere than in the tropics. The experience of those men who service them in the tropics should be of considerable benefit.

Which brings me to my final

pleted. By all accounts it was doing just about everything an amplifier should not and the builder, who was not a very experienced experimenter, was completely baffled.

I tried to get some idea of the trouble over the phone, but we didn't seem to be speaking the same language and were rapidly getting nowhere. Finally I suggested he bring it over to the family mansion that evening, reasoning that he probably had a few obvious wrong connections that could be put



Speaker connections like the above make it tough going for the amplifier. Although not apparent when presented in circuit form, the two terminals involved were close together on the chassis and thus easily confused. Note also the long stopper leads.

point. I still think that most benefit will result from complaints to the maker, listing the faults which are apparent in any set. As one who has worked in such factories in years gone by, I have vivid recollections of the upheavals which such letters sometimes caused.

You may think you are a voice crying in the wilderness, but you may take my word for it that it doesn't take many complaints about a specific design feature to ensure that something will be done about that feature before very long.

Summed up, my advice is: Complain where it will do most good. Do that and you will be making your contribution toward better radio.

GOOD DEED

My next good deed story concerns an amplifier. It all started when an acquaintance, to whom I felt I owed a good turn anyway, rang me up with a tale of woe about an amplifier he had just com-

pleted without much bother. (One characteristic of servicemen is that they seem to remain confirmed optimists—in spite of experience which should teach them otherwise.)

And so it was that my friend duly arrived, complete with amplifier, which we set up on the bench and proceeded to examine. It was one of the Playmaster series (actually the No. 8 ultra-linear job), plus a No. 6 control unit. He had also brought a copy of the circuits with him.

LOW OUTPUT

My friend's main complaint was that the output from the amplifier was very low and a quick check supported his statement—it was horribly low. A few seconds inspection around the speaker circuit was sufficient to reveal the cause. While one side of the speaker voice coil returned (correctly) to the chassis side of the transformer secondary, the other side connected to the remote side of the 5000 ohm feedback resistor.

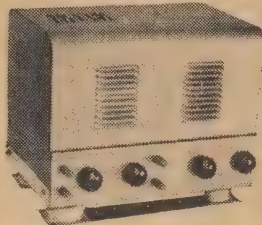


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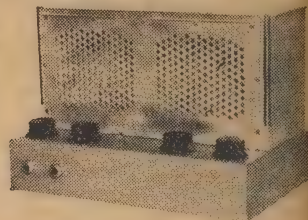
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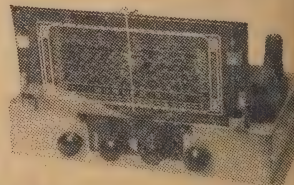
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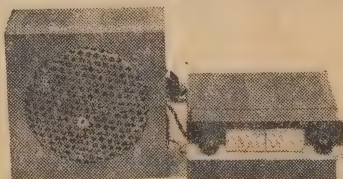
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As a result, the speaker was, in fact, connected across the 100 ohm resistor forming part of the EF86 cathode circuit. Small wonder that he was battling to make itself heard. The cause of the mistake was fairly obvious; the layout was such that the wrong end of the feedback resistor was closer to the speaker voice coil socket. Hence it had been selected almost automatically. With this point corrected, the amplifier "came good" and appeared to be doing all that might be expected of it. However, I was far from happy with the general appearance of the job. My friend had purchased the correct chassis and seemed to have followed the recommended layout quite carefully—at least as far as the major components were concerned. Where we had gone astray, like many beginners, was in the wiring. Most of the longer connections were made in gentle sweeping arcs rather than straight from point to point. Apart from its appearance such liberties are out of place even at audio frequencies.

WIRING TROUBLE

Another point was the filament wiring. This used about the thinnest hook-up wire available, and I had some doubts as to its suitability. After all, the total current drain was considerable, assuming a tuner as well as a control unit, would be quite high, and it would be quite easy to finish up with a substantial voltage loss at the remote filaments.

I was also staggered somewhat by the mounting and wiring of the grid stopper resistors for the EL37's. From what I could see in the original reproduced photograph (later confirmed) the stoppers were mounted between the resistor strip and their respective grid pins, putting them hard against the pins in accordance with standard practice.

But not so in this amplifier. For one thing the resistor strip appeared to have been moved bodily toward the input end of the chassis and for another the stoppers were mounted on the strip itself. As a result they were some three to four inches away from the grid pins.

When I drew attention to this, my friend replied that he didn't think it mattered. Oh yes, he quite understood that it was not the usual practice, but this case was different. Radio and Hobbies had interfered, even if they didn't say it outright, that it was a naturally stable amplifier. This being so, why worry about the finer points of stopper lead length?

Presumably it had not occurred to our friend that the amplifier could only be claimed as stable because of various precautions—including the use and careful placing of stoppers—which the designer had the foresight to employ.

STOPPER ACCURACY

In contrast with this casual approach to the placing of the stoppers the selection of the actual resistors had been undertaken with considerable care. This was revealed when I commented that one was one of the new, very small, half-watt types, and the other an old, very much larger 1-watt variety. Not that it mattered, of course, but I was intrigued.

"The reason I did that," my

friend replied, with a touch of pride, "was because it was the only way I could get them matched to within one pc."

I'm afraid I didn't have the heart to say very much, merely commenting that it wasn't really very critical. In fact the entire value of the stopper is only equal to one five-hundredth part of the total grid resistance, or about .2 of 1 pc. On this basis the stoppers could differ in value by 100 pc without having the slightest effect on performance.

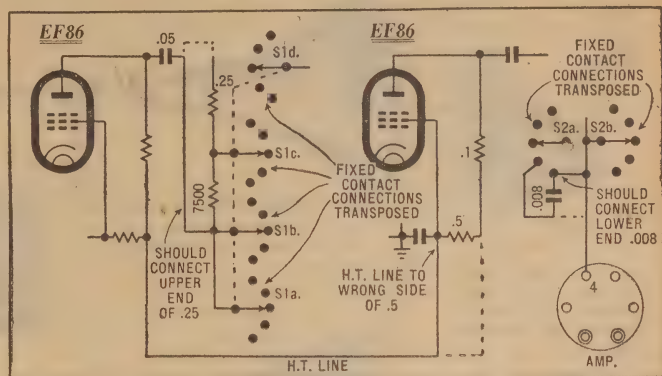
Truly a case of misguided zeal.

Another point which seemed to be worrying my friend was the apparent lack of balance between the two screen taps on the output transformer. He had established

up a little and the stoppers mounted more logically. This my friend agreed to do, probably experiencing a much greater incentive now that the amplifier was working correctly.

Next we tackled the control unit. This was working in a sort of a way but lacked gain, was distorting somewhat, and did not appear to do all the things it was supposed to do. Checking against the circuit quickly revealed two obvious faults. Both were in the plate circuits of the EF86's.

The first one I found was in the second EF86. In this case the screen dropping resistor was .5 meg, and the plate load .1 meg, the junction of the two resistors running to the HT line—or so it



The control unit was really in a mess. Any one of the faults would be bad enough; collectively they rendered it completely useless. Apart from the transposed switch connections the correct connections are shown dotted.

that they were lacking in balance by measuring the DC resistance with an ohmmeter, discovering that there was a difference of 20 ohms between the two.

He didn't volunteer in what total value this discrepancy occurred and I didn't press the point. It wasn't really important because, as I explained to him, this DC resistance had little bearing on the impedance values presented by the transformer. In the first place the impedance of the winding is so many times higher than the resistance, that any unbalance caused by lack of balance in the latter would be quite negligible.

RESISTANCE AND IMPEDANCE

Secondly, it must not be inferred that a difference in resistance automatically means a difference in the number of turns and, therefore, a difference in impedance. There may be a different length of wire in each half due, for example, to one half of the secondary being wound over the other half, but this is not the same as a difference in impedance. Not all transformers are wound as suggested above, but there are plenty of other reasons why they may not be exactly symmetrical in the physical—and resistive—sense.

Which just about disposed of the main amplifier. Although it appeared quite stable, I tactfully suggested that the wiring might be tidied

should have been. Instead the screen end of the screen resistor connected to HT, meaning that full HT voltage was applied to the screen and the plate load was increased to .6 meg. The result was a set of operating conditions never dreamed of by the valve manufacturers.

COUPLING CIRCUIT

The fault in the first EF86 involved the .05 mfd coupling condenser from the plate to the frequency compensating network. Instead of connecting to the .25 meg. resistor it connected to the lower end of the 7500 ohm resistor, that is, straight into the moving arm of one of the switch sections (S1b). The upper end of the .25 meg. resistor was floating in mid-air.

With these faults corrected performance was better, but the various compensating networks appeared to be tangled up in some manner and not functioning anything like correctly. I commenced a careful check of the switch connections against the circuit, starting with the bass boost and cut switch (S2a and b).

I found a small error here, the lead from pin 4 of the six pin socket running to pin 5 of the bass switch instead of pin 4, and done in such a manner as to completely short circuit the .008 mfd condenser. This was easily fixed.

Then I found the really big fault,

**SWITCH
TO**



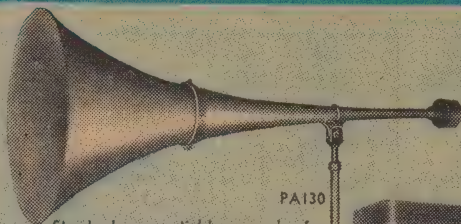
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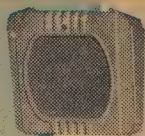
PA138

Standard reflex horn speaker for medium distance projection of speech and incidental music.



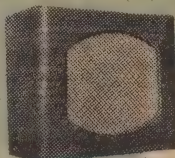
PA130

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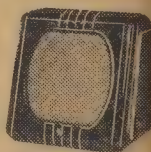
PA150/I

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PA77/12PS

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PA150/W

Moulded walnut speaker, similar to above. These models are also available with 600 ohm stepped faders.



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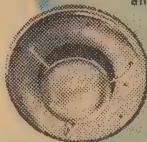
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confused by the multiplicity of contacts on the switches my friend had assumed that the moving contact belonged to the wrong bank of contacts and had thus transposed the connections relative to the moving arms. The first one I found was the bass control switch S2a & b). The treble control switch, involving only a single section, was correct.

With a horrible premonition I turned to the record characteristic switch (S1). Yes, you've guessed it, it was wrong, too, every section of it. Fortunately it was not quite so bad as it seemed. Two of the sections (S1c & S1b) were joined together with a 7500 ohm resistor, and so had worked out correctly in spite of the error. But that still left the other two sections, making four in all, which had to be re-wired.

WOULD I?

I didn't particularly fancy the job of practically re-wiring the entire switch assembly, but there seemed little help for it. Although my friend appreciated what he had done and would have been quite willing to tackle the job himself, I had a lingering doubt about his ability to get it all straight.

My doubts, added to his own, settled the question. We tackled the job on the spot. For the most part I found it easier to change the connections to the various fixed contacts rather than the moving ones, although this involved more joints, it was a more logical approach, the moving contacts having been wired in such a way that a far more logical placement of components was possible when the switch was correctly wired. In most cases I had to shorten pigtailed rather than lengthen them.

One idea I did not like was the earthing system adopted. Most of the components involved had been earthed to the front of the switch slider plate (presumably before it was mounted). Once mounted it was virtually impossible to get an iron near the joint. It so happened that one of these had to be changed, but if they had it would have been a sticky situation.

Finally it was all done and I don't mind confessing that I had really had it. We gave it a rough check and everything seemed to be working as it should. Then I turned my attention to a somewhat different problem, that of the pickup.

WHY No. 6?

It was a crystal and I still have not been able to discover why my friend chose the No. 6 Control Unit for use with it. This particular unit was designed, primarily for very low output pickups, such as the variable reluctance types. It is far more elaborate than need be for a crystal, with its initially high output.

(Checking with R & H staff I find that this is a common error among enthusiasts, in spite of the publicity given to the use for which the unit was designed.)

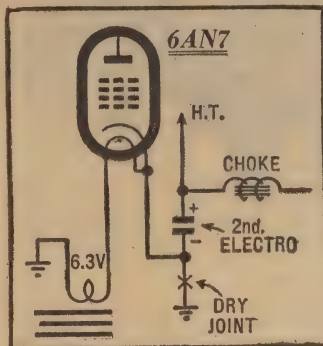
The difficulty in using a crystal pickup is that it is so very easy to overload an early stage which has been designed on the basis of a much lower input. Where a crystal must be used, it is desirable to provide a voltage divider to reduce the

pickup voltage to something more like that for which the unit was intended.

Then, of course, the valves in the control unit provide the necessary amplification to restore this lost voltage by the time the signals reach the main amplifier.

It is also desirable to remove the natural bass boost of these pickups in order that the bass boost built in to the control unit may be allowed to operate. This makes the whole scheme a lot more scientific, even if it sounds just like a crystal pickup after you've finished!

The usual arrangement is to provide a load for the pickup which is much lower than normal, thus



No wonder it hummed! A faulty chassis connection caused the filament voltage to be superimposed on the HT line. It also opened the cathode circuit and effectively killed the converter stage.

eliminating its natural bass boost and to tap this load to provide the aforementioned voltage division.

I had in mind to do just this but my friend was most emphatic that nothing be done to spoil the "beautiful bass response of the crystal pickup". As a result I left the pickup working into its normal .5 meg. load and tapped this load at about one-tenth its resistance from the earthed end. As an additional precaution I added some feedback around the first EF86 (as recommended in the original article) thus reducing the gain appreciably.

The final result was entirely satisfactory, at least from the owner's point of view, even if it sounded like nothing any musician ever produced.

"Ah lovely, just listen to that beautiful bass" my friend sighed blissfully, as the speaker cone rocked back and forth.

NOT FOR ME

Personally, I like my reproduction a little more like the original but it's surprising the number of raised eyebrows one encounters when one diffidently suggests that the original might be used as a basis for comparison.

Along more conventional lines is the following story concerning an unusual hum trouble. The set was a four valve mantle type, of recent design (and by a well known manufacturer), and the complaint

was intermittent operation accompanied by severe hum.

For once the fault was in evidence immediately I switched on. There was no sign of any signals, only a very severe hum. It was the low pitched, relatively pure hum attributable to a 50 cps source. This was important, since most hum in receivers is 100 cycle due to faulty filtering. This has a higher pitched, harsher characteristic and is not difficult to recognise with a little experience.

HANDY TIP

An ability to tell the difference between the two can often help a great deal in service work, since there is obviously no point in replacing filter components in an effort to cure 50 cycle hum, or in searching for faulty audio shielding and the like when the hum is 100 cycle.

In this case I had a second symptom to consider; the complete lack of signal. I decided to attack this first. A quick check showed approximately normal sensitivity in the IF channel and as far as the converter plate. From the converter grid there was nothing.

I pulled out the converter (a 6AN7) with the idea of testing it. The hum ceased immediately. With visions of internal shorts to the heater I didn't bother to test it, but simply plugged in a new one. The hum was just as bad as ever and there were still no signals.

At this point I commenced a more detailed examination of the stage, and after one or two routine checks I suddenly realised that the 6AN7 filament was not alight. (It is quite surprising the number of times one can be caught in this way. While going to considerable pains to check plate, screen and other similar voltages the filament circuit is invariably taken for granted. The result can be a lot of wasted time.)

Since I knew that the filament of the replacement 6AN7 was intact the fault could only be in the filament wiring. As is frequently the case in commercial sets there was only one active lead, the return circuit being through the chassis. I soon established that there was voltage on the active valve pin, thereby suggesting that the chassis connection was at fault.

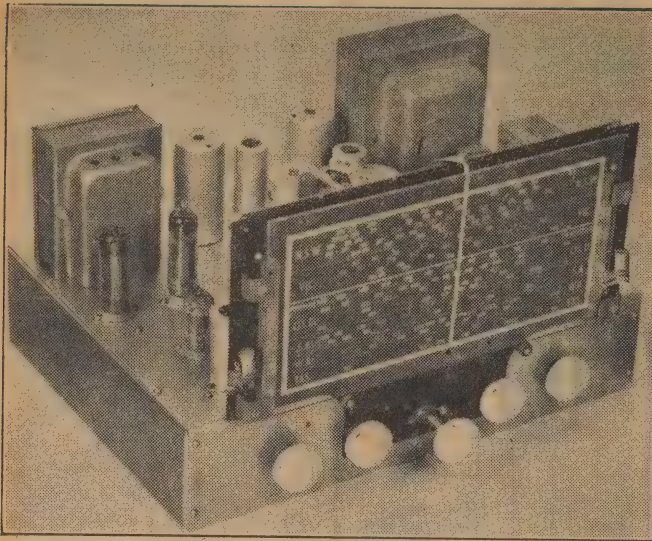
INTERESTING FAULT

Sure enough this was where I found the trouble, but its exact nature is quite intriguing. Mounted alongside the 6AN7 was the second filter condenser, a chassis mounting 16 mfd electrolytic. This was a type usually sold with a bakelite mounting plate attached and intended for use in back bias circuits, &c., where the negative side needs to be insulated from the chassis.

The mounting plate is normally held by two small lugs—both negative terminals—which pass through slots in the plate and are given a 90 degree twist. Many manufacturers, including the one who made this set, punch similar slots in the chassis, discard the insulating plate, and mount the second filter condenser directly on the chassis by the same means.

In this case both lugs had been given the aforementioned twist and

(Continued on Page 119)



A front view of the completed set. The complete audio section is on the left of the chassis, with the EF86 just behind the dial. The power supply is on the right, and the tuner in the centre. The two IF transformers and IF amplifier are at the rear. Controls, left to right are. Volume, bass, tuning, treble, and function.

AN EIGHT VALVE RADIOGRAM

It is some time since we described a large radiogram, so here is one to bring us right up to date. Featuring an ultra-linear output stage, flexible compensation controls, and a sensitive tuner, it gives an impressive performance on both records and radio.

THE inspiration for this set was the Ultra Linear Crystal Pickup Amplifier described in last month's issue. It seemed to us that this amplifier would make an ideal audio section for one of the larger radiograms; the type that has never lost its popularity with a large section of our readers.

PERFORMANCE

For those who want better than average results at a moderate cost, the combination of this amplifier with a high performance "front end" would be hard to beat. It is ideally suited to the crystal pickup which, with all its academic limitations, is still one of the most popular types. Used in conjunction with one of the commercial record players now available, it makes up into a set of much larger proportions than you could get for equivalent outlay on the commercial market.

There is also the advantage that all the facilities are mounted on a single chassis. This makes it a better proposition for readers who may have an existing cabinet—prob-

ably an expensive one—which they wish to retain. Again, there is quite a tendency these days to incorporate sets in built-in cupboards, room dividers, and so forth, and a single chassis will often lend itself more readily to such an arrangement than will the several chassis of the more complex gear.

For the man who has been holding off conversion to microgroove because of expense and indecision about equipment, this may well be the answer.

As a radio, the set retains the advantage of the continuously variable bass and treble compensation which, used intelligently, can overcome

by Philip
Watson

many of the limitations of the conventional receiver. Treble boost may be used to offset to some extent the loss of top response due to side band cutting in the tuner, thereby giving some semblance of wide-range reproduction.

On the other hand the tuner is selective enough to work in all "difficult" locations, while the cut is always useful when conditions are bad and noise level is high.

Bass boost can be very useful in restoring the balance of some recorded radio programs which apparently escape the attention of the station engineers. Bass cut is not so likely to be required for radio programs but is there, if required.

All in all then, this set should be able to cope with almost any form of signal, whether it originates from any of the popular crystal pickups or a broadcast station, be it near or far away.

OLDER EQUIPMENT

In designing the set we took an other factor into account. There are many readers who already possess radiograms made before the present era of wide range recordings, &c, and who are faced with the problem of bringing their equipment up to date.

Most of them naturally feel disinclined to scrap their present equipment completely and any new design will naturally be viewed in the light of the question, "What can salvage from my present set-up?"

With this thought in mind, we deliberately designed the chassis along fairly generous lines, leaving room for the older style valves if these should be available. The space allowed for the power transformer and other heavy gear is also rather liberal so that it should not be difficult to accommodate many of the older style units, which may happen to be suitable electrically.

SAME AMPLIFIER

As can be seen from the circuit the audio section is virtually identical with the amplifier described last month. The only major change is the substitution of a 5Y3 for the original 5V4 rectifier. This has the effect of reducing the HT voltage to approximately 250 and bringing the total current drain, including the tuner, into the range of a 100 mA power transformer and choke.

This size-reduction represents quite a worthwhile saving in cost as well as widening the scope of existing gear which may be salvaged. Naturally, the power output will be lower but it should still be about

Doubtless, the question will arise regarding the possibility of using valves other than the EL84 (or 6BQ5) in the output stage. While these are undoubtedly the preferred types for this position, you could probably get away with other high-slope valves in the same circuit arrangement. Valves like the KT61, 6M5 and 6BV7 suggest themselves. Check the datasheet, however, which can be the recommended valve for push-pull pentode operation, in the absence of further information.

ENTODES

If you want to try 6V6's, they had best be used as pentodes, with the appropriate bias resistor and, possibly, some reduction in the feedback resistor. We are not advising such a substitution but merely foretelling the inevitable queries about whether it would be possible.

The EF86-12AX7 section is best left all alone. Like all direct-coupled circuits, it is rather more critical than resistance-coupled circuits and does not lend itself so readily to other valve types, without careful adjustment of the circuit.

The speaker transformer is another component regarding which it is not advisable to take too many liberties. One is thinking of salvaging existing rig equipment. Of course, if it is of one of equivalent quality, well and good, but it would be unwise to expect much from the cheaper types supplied with speakers, if the existing feedback network is to be retained.

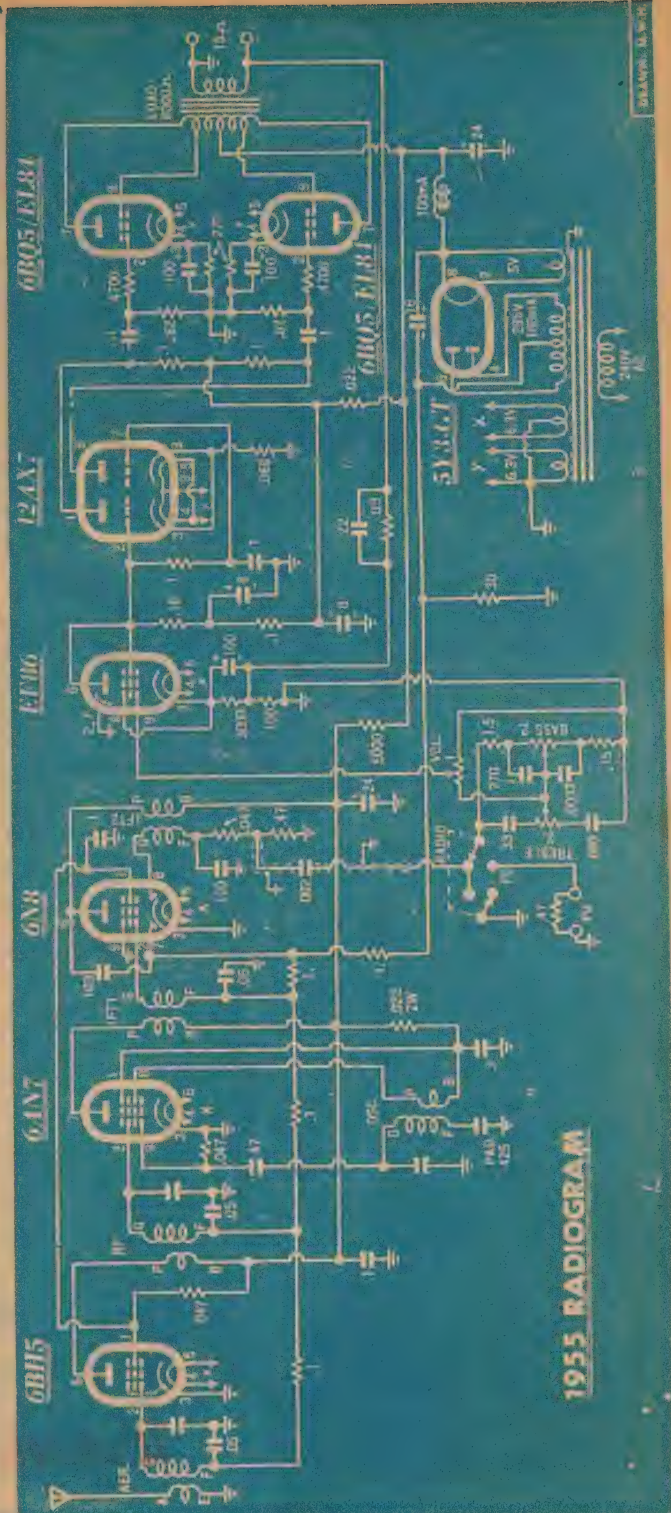
In some cases such an arrangement might work, particularly if the feed-back was reduced, but each case would have to be treated on its merits and purely as an experiment which may or may not be satisfactory.

THE TUNER

For the tuner we decided that something more than the bare minimum was desirable in order that the set would be suitable for country as well as city use, and have the widest possible appeal. Accordingly we included an RF stage and the extra gain and selectivity should make available any signal which is strong enough to get through the natural noise level.

As an RF amplifier we used the 6BH5, a moderately high-gain valve which gives good performance without too much risk of instability. The

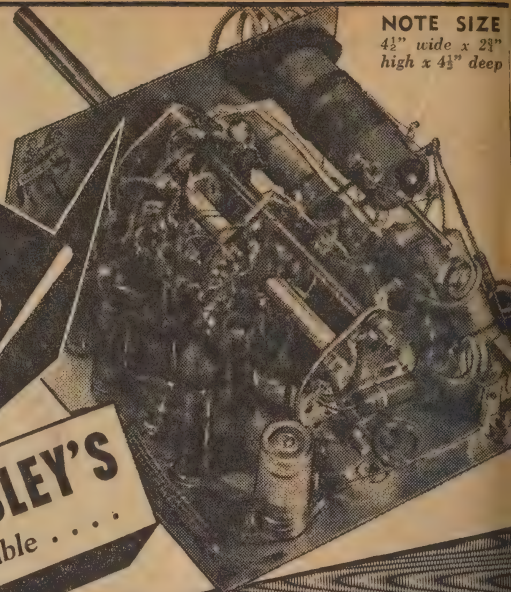
This circuit shows how last month's amplifier is combined with a sensitive tuner to produce a first class radiogram. Note the changes to the power supply which include the substitution of a 5Y3 rectifier, smaller power transformer and choke, and back bias for the tuner.



NOTE SIZE
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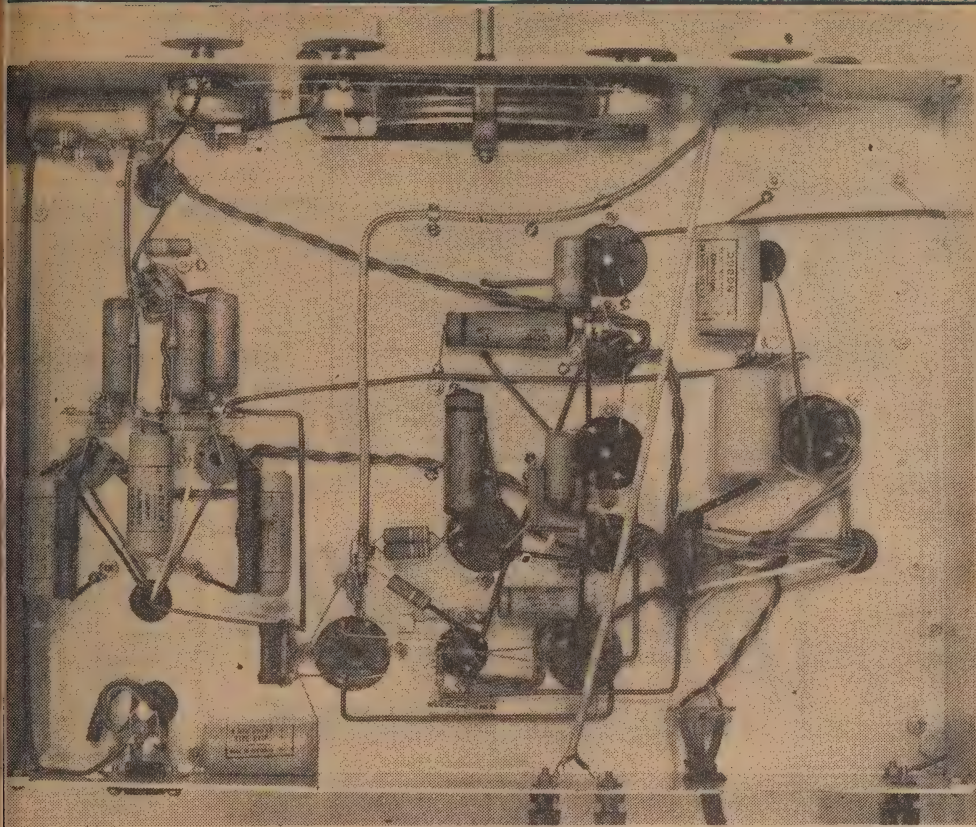
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KINGSLEY

RADIO

UNDER CHASSIS VIEW OF EIGHT-VALVE RADIOGRAM



There is plenty of room under the chassis and no need to crowd the parts. The audio section is on the left with the EF86 at the top. Above it is the volume control, then the bass control, tuning, treble, and function switch in that order. In the finished chassis these controls are enclosed by a shield panel to minimise hum.

AN7 is one of several possible choices for the converter stage, while 6N8 is an almost automatic choice for the IF amplifier, which must also provide AVC and detection.

Older type valves could be used here, such as the 6SK7, X61M and AR7, or the 6U7, 6J8 and 6G8, or combinations of these. The only changes, apart from the physical ones, will be to the grid and screen voltages in certain cases.

Assuming that such valves are being salvaged from older gear, it is likely that the appropriate oscillator coil will also be available. These valve suggestions are by no means the only types that could be used, though they are the most likely.

Back-bias is used throughout the front end, providing bias for all three stages from a single resistor. The alternative would be a separate bias resistor and by-pass capacitor for each stage, making for higher cost and greater circuit complexity without adding anything to the performance.

As it is, it is only necessary to add a 30-ohm resistor to the transformer centre tap and return the first electrolytic negative lead to the

PARTS LIST

1 chassis 14 x 10½ x 3in.
1 dial USL46 or similar. Suit gang.
1 power transformer 285v. 100mA.
5v 2A. 6.3v 2A. 6.3v 2A. CT.
1 filter choke, 10H 100mA.
1 output transformer 8000 ohms P-P.
Tapped for ultra linear operation.

VALVES

1 6BH5, 1 6AN7, 1 6N8, 1 EF86,
1 12AX7, 2 EL84's 1 5Y3.

VALVE SOCKETS

3 miniature 9-pin plain.
1 miniature 9-pin with short shield.
3 miniature 9-pin with long shield.
1 Octal.
1 4-pin miniature speaker socket.

COILS

1 BC aerial. 1 BC RF. 1 BC Oscillator.
2 455 kc IF transformers. All standard size cans.

RESISTORS

2 2 meg. potentiometers. 1 1 meg. potentiometer. 1 1.5 meg. 3 1 meg. 2 .82 meg. 2 .47 meg. 1 .2 meg. 1 .15 meg. 2 .1 meg. (5%) 3 .1 meg.

1 .068 meg. 2 .047 meg. 1 .03 meg. 2 4700 ohms. 1 3300 ohms 1 1000 ohm. (All ½W) 1 .047 meg. 1W. 3 .022 meg. 1W. 1 5000 ohm 3W. 2 270 ohm 3W. 1 30 ohm 1W.

CAPACITORS

2 100 mfd 40VP Electro. 1 100 mfd 12 VP Electro. 2 24 mfd 525V Electro. 1 16 mfd 525 Electro. 2 8 mfd 525V Electro. 6 .1 mfd 400V paper 3 .05 mfd 200V paper. 1 .002 400V paper. 1 .0033 mfd mica. 1 680 pf ceramic. 1 425 pf 5% mica. 1 270 pf ceramic. 2 100 pf ceramic. 1 47 pf ceramic. 1 33 pf ceramic. 1 22 pf ceramic. 1 3 gang tuning capacitor, midget or standard.

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2 8 term. 1 7 term. 2 5 term. 4 3 term.

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nearthed side of this resistor. This in no way effects the bias of the radio amplifier stages, which operate as before.

We spent some time working out chassis and layout which would be reasonable in size and yet versatile enough to accommodate older-style components. The result is a chassis measuring 14in x 10in x 3in, which is not over-large for a set of this type. We used standard size coils and left enough room for the larger valves, if they are preferred.

The lay-out may be considered in three sections. On the left is the amplifier, in the centre the tuner, and on the right the power supply. The layout of the amplifier is virtually identical with that used for the original version last month (excluding the power supply), and the four control knobs are distributed along the front of the chassis in the same order.

TUNING CONTROL

The only difference here is that the controls are spaced to make way for the tuning control, which is located between the bass and treble controls. As with the original amplifier, the controls, their associated wiring, and the EF86 stage are all arranged so that they may be enclosed by a right-angle shield running the length of the chassis. This, with the top and front of the chassis, forms a box which completely encloses this section.

To keep the tuner components clear of this section it was necessary to move them back a couple of inches from the front of the chassis. This includes the gang and this is coupled to the dial drum by means of a 2-8in to 3-8in extension shaft. If a larger type gang is contemplated, there should be plenty of room to accommodate it by allowing the front to approach closer to the dial. An extension shaft may or not be required, according to the particular type.

In order to locate the controls suitably and also space them equally, it is not possible to use the holes originally provided in the dial plate. Instead we had to modify the plate slightly and cut two new holes in the mounting slots near each end. This allows all controls to be spaced equally 2 1/8-in apart.

ORDER OF CONTROLS

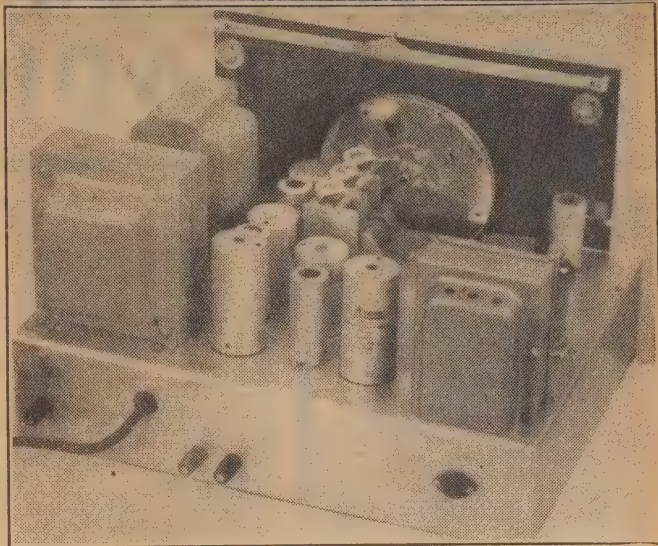
The volume control is on the left, closest to the EF86, then the bass control, tuning, treble control, and the radio/pickup change-over switch.

The aerial coil, the 6BH5, and the RF gang are mounted alongside the RF coil, with the oscillator coil at the rear. The sections of the gang are used in the same order. The 6AN7 is directly behind the RF coil and the IF transformers and the IF amplifier run parallel with the rear of the chassis.

Orientation of the valve sockets is important and they should be mounted as follows, using the gap between pins as the reference. All the amplifier valves toward the nearby end of the chassis, the exact position being indicated by the chassis, the 6AN7 and 6N8 toward the oscillator coil, and the 6BH5 toward the gang. The rectifier is not critical.

With the sockets laid out as above the coils may be quite easily mounted to provide minimum length for the critical grid and plate leads. The

RADIOGRAM—VIEW FROM REAR



On the right is the output transformer, on the left the power transformer and choke. Left of the gang is the aerial coil, RF valve, RF coil, and converter in that order from the front of the chassis. Oscillator coil is behind the gang.

HT and AVC leads are less critical, being "cold" by reason of their respective bypass capacitors.

Two leads which can be quite critical are those from the AVC diode (pin 7) to the two one megohm resistors of the AVC circuit. The diode ends of these two resistors are "hot" at RF, while the opposite ends are "cold", being bypassed. It is important, therefore, that these two resistors are mounted as close as possible to the diode pin.

RESISTOR PLACING

In our case the load resistor (running to the back bias resistor) is mounted between the diode pin and a terminal on a three tag terminal strip mounted under the 6N8 rear socket bolt. The decoupling resistor runs direct to the AVC pin of the first IF.

There are a number of terminal strips used in the set and they help to support the smaller components in a logical manner. As in the original amplifier, an eight terminal variety is used to accommodate the grid stoppers for the EL84's, one end of the coupling capacitors, one end of the plate load resistors for the 12AX7, the .022 meg. decoupling resistor, and the positive end of the 8mfd decoupling capacitor.

In the grid circuit of the EF86 two terminal strips support a number of the compensation circuit components. A seven terminal type is used for the .1 meg. decoupling resistor, the EF86 plate load resistor, and the 8 mfd decoupling capacitor.

A five-terminal strip accommodates the EF86 3300 ohm cathode resistor, the 100 mfd by-pass, the 100 ohm cathode resistor and the 680 pf capacitor in the compensation circuit. The earthed terminal also serves as the single earth point for

this section, as indicated in the circuit. As explained last month this procedure is advisable to minimise hum problems.

A three terminal strip is secured under the second IF transformer mounting nut and supports the 5000 decoupling resistor. Also near the second IF transformer is an eight-tag strip which supports the .047 diode decoupler, the .47 diode load, one end of the 100 pf bypass, and the .002 mfd diode coupling capacitor. It also provides a HT terminal from which the .047 meg. screen resistor and the .011 meg. oscillator plate resistor are taken.

Note that we have omitted the 100 pf capacitor which normally bypasses the "hot" end of the diode load. Using ordinary good quality shielded hook-up wire, there should be enough capacitance to simulate this capacitor, but it may be fitted if there is any suggestion of RF instability in the audio system.

TRANSFORMER LEADS

A three-terminal strip is used to terminate the power transformer primary leads and the power cable. A five terminal strip terminates the filament leads and the secondary centre tap as well as supporting the 30 ohm back bias resistor. A three-terminal strip near the rectifier socket terminates the choke leads and the positive leads from the main electrolytics.

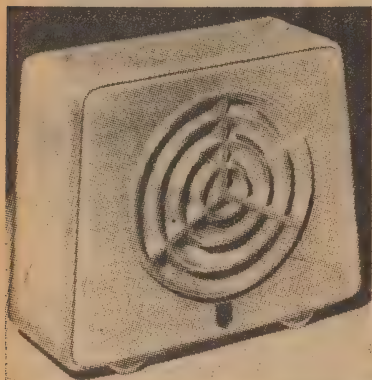
The remaining minor components may be supported between terminal points of larger ones, using their own pigtail.

Before commencing the wiring proper it is a good idea to carry out some preliminary wiring on the valve sockets. This consists of determining those pins which will have to be earthed, such as the

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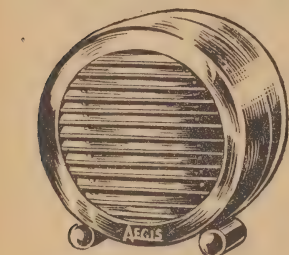
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M9



SP6



M18

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athode, suppressor, &c., plus the central shield, linking them together with 20g tinned copper wire and earthing them to a solder lug under one of the socket mounting nuts. Where a steel chassis is used, it is a good idea to link all these earth lugs together and not rely on the chassis.

There are two filament runs, one for the EL84's and 12AX7 and the other for the EF86 and the tuner valves. Both are made with twisted hookup wire and the one for the EF86 circuit should use the centre-tapped winding. The other winding is simply earthed at one side.

WIRING

For the shorter connections, as between coil and socket pins, 20g tinned copper wire is most satisfactory and will not need insulating sleeving except in odd cases. Other wiring, HT runs, and so forth, may be made in plastic hookup wire.

The aerial lead is best kept clear of the RF and IF stages and should be taken straight across the chassis to the right-hand side, through a small hole in the side and along the outside of the chassis to the rear. Here it enters the chassis again for an inch or so to connect to the aerial terminal on the rear.

Two other terminals on the rear of the chassis provide for pickup connection and a shielded cable runs from them to the function switch. As mentioned in the article on the amplifier it is necessary to provide a suitable load for the pickup, a common value being .5 meg., but varying with different types and individual requirements. The optimum value is best determined by experiment and may be mounted on the function switch.

The final testing and adjustment of the set does not present any particular problems. As with all amplifiers employing voice coil feedback it is necessary to determine the correct polarity of the voice coil circuit before a permanent connection is made. Connection to one side will cause the amplifier to oscillate and obviously the wrong one. Connection to the other side will cause a noticeable drop in gain, indicating negative feedback.

For this reason this connection is best left until the amplifier is functioning and the correct polarity determined, experimentally. The wiring may then be made permanent.

TRIAL RUN

Unless there is some major defect either in the wiring or a component the tuner should produce some kind of signals immediately it is switched on. Ideally one should be in a position at this stage to connect it to a service oscillator and complete the alignment in the approved manner.

Even if this cannot be done immediately it should be the ultimate aim, since best results are not likely to be achieved otherwise. However, as a temporary measure, it is possible to improve performance using the simple "alignment by ear" technique.

The IF transformers as received from the makers should be adjusted fairly close to the correct frequency. They should only require slight adjustment, mainly to offset the stray capacitance of the associated wiring, probably amounting to one turn at the most.

(Continued on Page 103)

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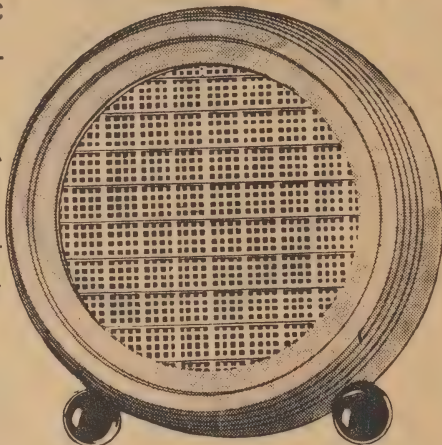
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WHY ELECTROSTATIC SPEAKERS?

Great interest is being shown at the moment in the development of electrostatic loudspeakers both for high frequency and full-range use. This article has been contributed by a world-famous designer of audio equipment.

WHERE appears little doubt to the author that the 30 years' supremacy of the moving-coil loudspeaker as a high-frequency reproducer is ending, and that it will be replaced by a particular form of electrostatic loudspeaker.

This opinion is based on engineering experience of the inherent limitations of moving-coil systems during these 30 years, and on intensive study and development of electrostatic loudspeakers.

It also appears that the moving-coil loudspeaker will stay with us as a bass reproducer, for which purpose it seems better fitted (when properly designed) than any foreseeable practical alternative.

Let us first consider the inherent faults of conventional moving-coil loudspeakers as high-frequency reproducers. These faults are eradicable because they arise primarily from the physical properties (which are limitations) of the materials available for use in the vibrating parts (paper, copper, aluminium, &c.), and secondarily from the mode of operation and the relative disposition of these parts (speech coil, diaphragm, surround).

MOVING COIL SPEAKER

Consider the structure of a typical small moving-coil cone loudspeaker. We know that modern feedback amplifiers can deliver an almost undistorted electrical signal to the speech coil, and our wish is to obtain a correspondingly undistorted acoustical signal as the result of the mechanical movement of the coil and diaphragm.

For this to be possible we can state with certainty that the moving parts must:

- (1) move as a rigid whole, i.e. without flexing;
- (2) move instantaneously with the changing electrical signal;
- (3) move proportionately to the magnitude of the electrical signal, irrespective of frequency.

Now 1, 2 and 3 above imply that such a loudspeaker will be a linear device and will not produce harmonic or other spurious frequencies, that it will have perfect "transient response" and freedom from "hangover", and that it will have a "flat" response, on and off the axis, up to a frequency whose wavelength is related to the cone dimensions.

Unfortunately, 1, 2 and 3 also imply that the moving parts will be mass-less and also infinitely rigid (i.e. of infinite internal stiffness). Alas, weightless and infinitely stiff materials have not yet been invented! Small cone loudspeakers are, therefore, somewhat short of perfection; how short may be gauged from Figs. 1 and 2, which are frequency response curves taken under

by

H. J. Leak

M. BRIT, I.R.E.

conditions laid down by the British Standards Institution.[1]

The 5in loudspeaker is more expensive than the elliptical; both have aluminium voice coils, and both are representative of present-day performance. The irregularities in the response curves are due to:

- (1) the mass of the voice coil resonating with its own compliance (the reciprocal of the stiffness); and
- (2) the cone breaking up and vibrating in unpredictable modes.

The only way to improve (1) is to make the voice coil as light and stiff as possible so that resonance will occur as high in the frequency scale as possible. The only thing that can be done about (2) is to make the cone stiffer, and to do this (using

the same material and without reducing its size) we must increase its thickness and therefore weight, when the loudspeaker's sensitivity and range will be restricted.

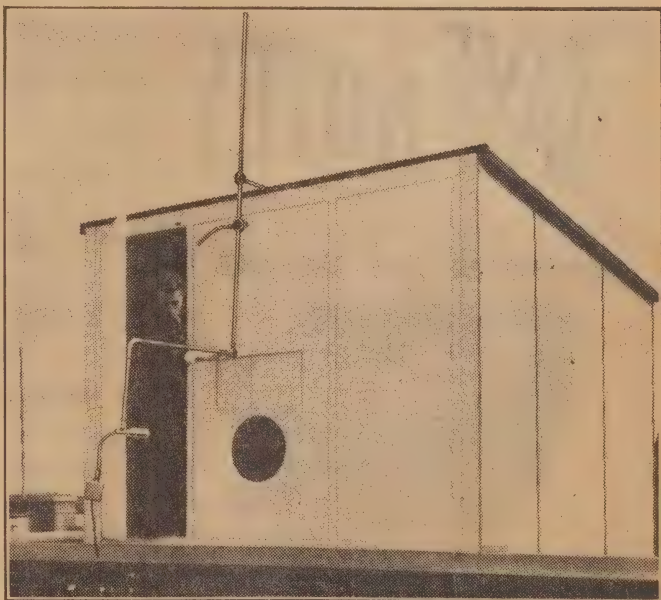
If we reduce the size of the diaphragm in order to make it stiffer it will then not move enough air to be an efficient radiator unless it is coupled to a horn. These are exactly the reasons why horn tweeters are made, and why they have a flatter frequency response (when well designed) than direct-radiator cone loudspeakers. Unfortunately, horns introduce distortions.

It is important to know that the sharp hills and valleys in the response curves are provenly indicative of a poor response to transient signals and of a slow decay time (hangover).[2]

NOT REALLY GOOD

To sum up, moving-coil cone loudspeakers have an irregular and restricted high frequency response and a poor transient response because the moving parts are too large, too heavy, and not stiff enough.

The aspect of "not stiff enough" which is important is that the mechanical driving force originating at the speech coil is mechanically re-

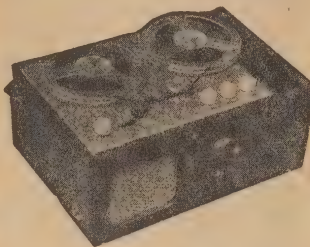


The loudspeaker curves shown here were taken out-of-doors. Note the microphones, one on the axis and one 30 degrees removed.



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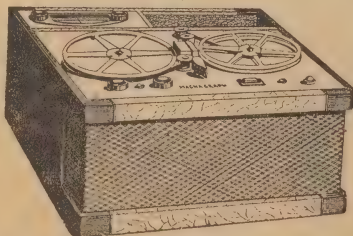
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and mechanically decoupled in the main area of the radiating diaphragm. The movement of the radiating diaphragm is, therefore, completely controlled by the electrical signals delivered to the diaphragm; hence the distortions in the sound output.

Now let us consider the only type of moving-coil loudspeaker which does not possess the above inherent faults to anything like the same degree.

The ribbon loudspeaker has a mode of operation essentially different from the cone loudspeakers previously discussed because the mechanical driving force is applied only over the whole area of the diaphragm.

It will be observed (see Fig. 3) that this diaphragm is extremely thin, being made of foil approximately 2in long by 3-8in wide and of a fraction of one-thousandth of an inch thick.

Notice that the diaphragm is actually the "moving-coil", and that it will obviously not be infinitely stiff. Now, this is a very important point indeed: the diaphragm does not need to be infinitely stiff because it is forced to move by the electrical signal as if it were infinitely stiff.

REBON SPEAKER

Fig. 4 shows the frequency response of the developed ribbon loudspeaker illustrated in Fig. 3. In the author's opinion the ribbon speaker has been the most faithful speaker transducer until the advent of the new electrostatic loudspeakers which we are soon to discuss.

The ribbon loudspeaker must, of course, employ a horn, in order to give an appreciable amount of air to the magnet will be expensive if the loudspeaker is to have an efficiency comparable with its associated woofer. A ribbon loudspeaker such as that illustrated is rather fragile as regards the moving parts and would cost around £45. These are the two main reasons why the ribbon has not been put into production.

It would appear from the above that what we really want is a system similar to the ribbon system, in its essential of a light diaphragm forced to move as a rigid whole, but having a diaphragm many times the area that it can radiate directly without a horn.

This would be quite impracticable at stepping up all the dimensions of the above ribbon tweeter, for the

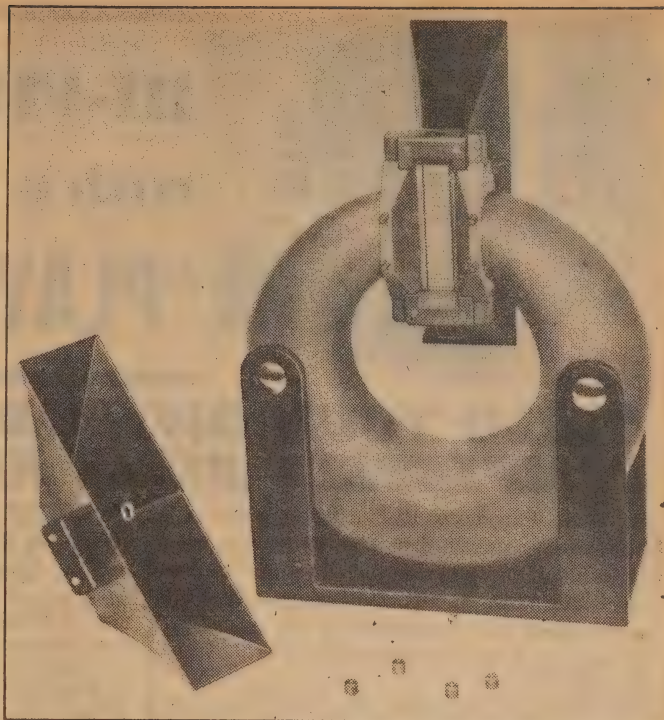


Fig. 3: A ribbon type tweeter made by Leak with the horn removed.

magnet would be of great size, weight and cost (certainly some hundreds of pounds).

But there is another way of electrically forcing a very light flexible diaphragm to move as a whole and to follow very accurately in its mechanical movements the electrical signals supplied from the amplifier. Furthermore, the diaphragm can be large; and this is where we come to electrostatic loudspeakers.

PERFORMANCE LIMITATIONS

Electrostatic loudspeakers have been under development for some 30 years, but have not been generally acceptable because of their performance limitations. Comparatively recently these limitations have been largely removed by the development of new materials and techniques, coupled with the conception

of ideas. It will greatly help us to grasp the significance of these new developments if we consider the basic form of the earlier electrostatic loudspeakers, pictured typically in Fig. 5.

The isolating capacitor merely serves to prevent the transformer short-circuiting the polarising potential applied across the rigid plate and the moving foil which comprise the actual electrostatic transducer.

The high resistance may be several megohms in value because no current is drawn from the polarising source by the loudspeaker, which can be seen to be a capacitor ("condenser"). This resistor also prevents the transformer being loaded by the source of the polarising voltage. This voltage will be several hundred volts or more, and in practice will be derived from the supply

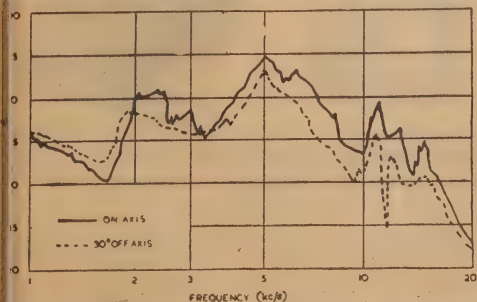


Fig. 1: Frequency curve of 5 inch cone tweeter with aluminium voice coil.

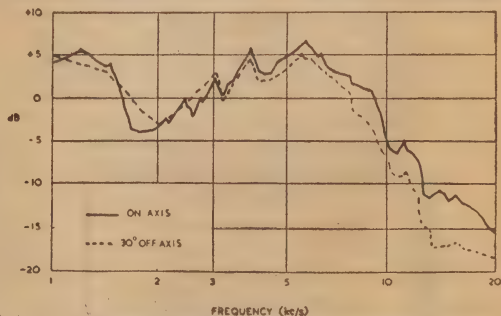


Fig. 2: Frequency response curve of 6 x 4 inches elliptical tweeter with aluminium voice coil.



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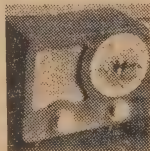
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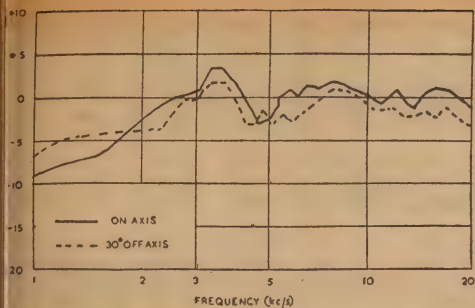


Fig. 4: Frequency response curves of ribbon tweeter illustrated at Fig. 3.

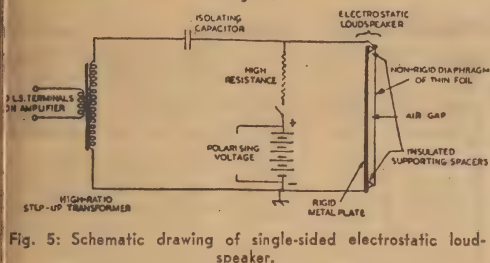


Fig. 5: Schematic drawing of single-sided electrostatic loudspeaker.

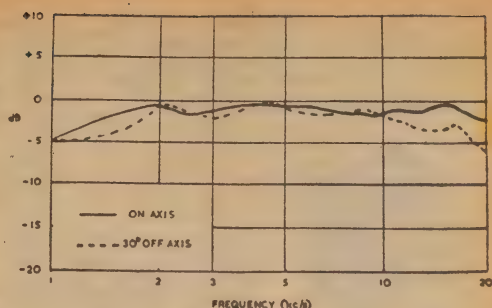


Fig. 8: Frequency response curves of the balanced push-pull electrostatic speaker illustrated at Fig. 7.

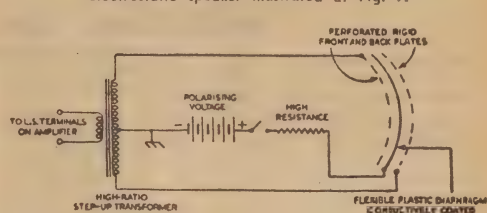


Fig. 6: Schematic drawing of balanced push-pull electrostatic loudspeaker.

gains, but for simplicity a battery is shown in Fig. 5.

The air-gap between the rigid plate and the diaphragm will be of the order of a few hundredths of an inch.

The area of each plate will be related to the lowest frequency which the loudspeaker is expected to reproduce efficiently; a few square inches will suffice to cover the range from, say, 8 kcs upwards, but to extend the range downwards to, say, 100 cs will require something more than a square foot.

Whatever may be the dimensions and spacing of the plates, we can calculate or measure the capacitance between them, and in practice it will range between a few hundredths and a few thousands of p.f. This value will give us the impedance range of the loudspeaker, which behaves as a capacitive reactance. We can now design our step-up transformer to give optimum matching between amplifier and loudspeaker.

We should now have a fair idea of the circuitry, construction and dimensions of what is called a single-sided electrostatic loudspeaker, and we can proceed to examine its modes of behavior, referring again to Fig. 5.

STEP-UP TRANSFORMER

Assume that the high-ratio step-up transformer is temporarily disconnected from the amplifier. If the polarising voltage is now switched to circuit a potential will build up across the rigid plate and the resulting electrostatic force of attraction will cause the thin diaphragm to move toward the rigid plate.

If this flexible diaphragm is not restrained, as by stretching, it will obviously move into contact with the rigid plate. If the diaphragm is tensioned sufficiently to prevent this collapse, then it will take up a position of equilibrium whose location

with respect to the rigid plate will be determined by the ratio of the forces contributed by the polarising potential (toward collapse) and the diaphragm tension (against collapse).

It can be shown, experimentally and mathematically, that to ensure stability the diaphragm must not be pulled toward the fixed plate more than one quarter of the distance which separated them before the application of the polarising voltage.^[3]

If we now connect the high-ratio step-up transformer to the amplifier the electrical signals from the latter will cause the diaphragm to move back and forth about the equilibrium position, so producing a sound output. Our immediate interest is the degree of faithfulness of this sound output, which depends on how accurately these backward and forward movements duplicate, mechanically, the positive and negative half-cycles of the electrical signals which cause them.

SMALL DIAPHRAGM

It must suffice to say that it can be shown, experimentally and theoretically, that the degree of duplication is poor (i.e. the distortion in the sound output is high) unless the amplitude of movement of the diaphragm is kept very small.^[3] This means that the sound output is small, and the loudspeaker is therefore effectively too inefficient to be of practical interest.

There are also other disadvantages arising from our stipulated construction:

- The layer of air trapped between the diaphragm and the rigid plate adds to the non-linearity of the system.
- The foil diaphragm will be too heavy to follow quickly the electrical signals if it is made thick enough to obviate extreme fragility, and

- temperature changes will affect the tensioning of the thin foil diaphragm; a drop in temperature will stiffen it, and a rise may expand it sufficiently to cause the polarising potential to arc across the reduced air-gap.

Therefore, our basic single-sided electrostatic loudspeaker does not appear practical as a high-fidelity reproducer, and this conclusion is confirmed by every engineer who has labored on this project.

But engineers are apt to think deeply and work hard on those problems which are theoretically attractive, and as the result of many years' development there has been evolved a form of modern electrostatic loudspeaker whose performance is markedly superior to that of other types.

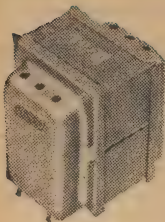
BALANCED SYSTEM

We will jump the slow progressive stages of its evolution and proceed to examine the basic form of the balanced-push-pull electrostatic loudspeakers which have recently been developed.

It will be seen that Fig. 6 bears some resemblances to Fig. 5. We still have the high-ratio step-up transformer, the high polarising voltage and the high resistance, but the actual loudspeaker elements are quite different, and we can state their basic features as under:

- The thin, flexible diaphragm is a sheet of extremely tough plastic material, having a negligible co-efficient of expansion as regards temperature, and coated with a conducting material which is so thin that it does not materially add to the weight of the diaphragm. The thickness of the diaphragm is a fraction of one-thousandth of an inch.
- The thin diaphragm is held by a system of insulating spacers

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From Australia's largest range of Transformers we have pleasure in introducing to you a streamlined preferential listing of power, output transformers and chokes.

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CODE NO.	PRIMARY VOLTS	HTV Aside	HT MA	FILAMENTS
PF 130	230-240	285	100	6.3VCT/2A 6.3V/2A 5V/2A
PF 130F	230-240	285	100	6.3VCT/2A 6.3V/2A 5V/2A
PF 151	230-240	285	60	6.3V/2A 5V/2A
PF 151F	230-240	285	60	6.3V/2A 5V/2A
PF 152	230-240	285	125	6.3VCT/2A 6.3V/2A 5V/2A
PF 165	230-240	385	60	6.3V/2A 5V/2A
PF 170	230-240	285	80	6.3V/2A 6.3V/2A 5V/2A
PF 185	240	150	30	6.3V/2A
PF 201	240	225	50	6.3V/2A
PF 265	230-240	Secondary Volts		17 TAP 11.5, 10, 8.5/4.2A
PF 299	240	285	40	6.3V/2A 5V/2A

POWER TRANSFORMERS SECOND PREFERENCE

CODE NO.	PRIMARY VOLTS	HTV ASIDE	H.T. MA	FILAMENTS
PF 160	230-240	385	100	6.3V/2.5A 6.3V/2.5A 5V/2A
PF 164	230-240	325	100	6.3VCT/2A 6.3V/2A 5V/2A
PF 166	230-240	325	60	6.3V/2A 5V/2A
PF 168	230-240	385	80	6.3V/2A 6.3V/2A 5V/2A
PF 169	230-240	325	80	6.3V/2A 6.3V/2A 5V/2A
PF 173	230-240	425	175	6.3VCT/3A 6.3V/2A 5V/2A
PF 174	230-240	285	150	6.3VCT/2A 6.3V/2A 5V/2A
PF 175	230-240	385	150	6.3VCT/2A 6.3V/2A 5V/2A
PF 545	240	Ext. 1000	2	6.3V/3A 6.3V/6A
PF 439	240	350	20	4V TAP 2.5/2A
		32V,	60	240-32 STEPDOWN

POWER CHOKES FIRST PREFERENCE

CODE NO.	HY IND.	D.C. RES.	D.C. MA
CF 102	15	300	60
CF 103	30	420	60
CF 105	15	250	80
CF 109	20	225	150
CF 196	20	130	125

POWER CHOKES SECOND PREFERENCE

CODE No.	HY IND.	D.C. RES.	DC MA
CF 106	12	200	100
CF 111	16	165	200
CF 112	10	70	250

If you have difficulty obtaining regular supplies, contact us immediately.

OUTPUT TRANSFORMERS FIRST PREFERENCE

CODE NO.	WATTS	PRIM Z	SEC. Z.	RESPONSE
OP 9	15	10,000, 6600, 5000 PP	500, 250, 125	50-8000 C/S
OP 13	25	10,000, 6600, 5000 PP	500, 250, 125	50-8000 C/S
OP 24	5	5000 SE	8.4 OR 2.1	30-15,000 C/S
OP 25	15	10,000 PP	15-3.7 OR 8.4-2.1	20-30,000 C/S
OP 44	10	5000-2500 SE	500, 250, 125	50-8000 C/S
OP 54	10	5000-2500 SE	15, 12.5, 8.4, 6.5, 4, 3, 2.7, 2.3, 2.	50-8000 C/S
OP 58	15	10,000, 6600, 5000 PP	15, 12.5, 8.4, 6.5, 4, 3, 2.7, 2.3, 2.	50-8000 C/S
OP 63	15	10,000 PP	15, 3.75	30-15,000 C/S
OP 112	6	10,000 PP	2, 8	40-12,000 C/S
OP 113	6	5000 SE	2, 8	SUIT 12 OL
OP 118	6	8000 PP	2, 8	40-12,000 C/S

OUTPUT TRANSFORMERS SECOND PREFERENCE

CODE NO.	WATTS	PRIM Z	SEC. Z	RESPONSE
OP8M	15	10,000 PP	500, 250, 160, 125, 100, 83.5, 7.5, 62.5, 55, 50	50-8000 C/S
OP 17	32	10,000, 6600, 5000 PP	500, 250, 125	50-8000 C/S
OP 19A	15	5000 PP	12.5, 8, 2.3	30-15,000 C/S
OP 65	15	10,000 PP	8.4, 2.1	30-15,000 C/S
OP 67	15	5000 PP	15, 6.5	20-30,000 C/S
OP117	6	5000 PP	8, 2	40-12,000 C/S
OP119	6	6600 PP	2, 8	40-12,000 C/S
OP 60	32	10,000, 6600, 5000 PP	15, 12.5, 8.4, 6.5, 4, 3, 2.7, 2.3, 2.	50-8000 C/S

VIBRATOR TRANSFORMERS FIRST PREFERENCE

CODE NO.	PRIM VOLTS	D.C. VOLTS	O'PUT MA	BUFFER FULL SEC.
VT 104	6	250	60	.004
VT 210	12	250	60	.006

VIBRATOR TRANSFORMERS SECOND PREFERENCE

CODE NO.	PRIM VOLTS	D.C. VOLTS	O'PUT MA	BUFFER FULL SEC.
VT 116	24	250	60	.005
VT 208	6	250	60	.01
VT 209	12	250	60	.08
VT 211	32	250	60	.005 ea. half

equidistant between two rigid plates, these being acoustically transparent (i.e. they allow sound waves to pass through them unimpeded).

- 3) The whole assembly is formed into an arc in the horizontal plane. (See Fig. 7.)

We will now examine the behavior of this push-pull loudspeaker. If we change from a single-sided amplifier to a push-pull amplifier there are appreciable improvements in distortion and power output, but even one change from a single-sided electrostatic loudspeaker to a balanced-push-pull type it would be an understatement to say that the improvements are appreciable: they are indeed spectacular, as can be shown mathematically and experimentally.[3]

WILL NOT MOVE

If, in the absence of a signal from the amplifier we switch the polarising voltage into circuit, the diaphragm will not move toward either plate, because it is subjected to equal and opposite electrostatic forces from each plate.

This means that the diaphragm need not be stretched to resist the static forces, thus removing one cause of the non-linearities inherent in the single-sided loudspeaker previously discussed.

Another important feature of the push-pull assembly is this: if the diaphragm is moved toward one plate it does not upset the condition of equal and opposite forces acting on it, provided that the charge is maintained, and this can easily be ensured by making the resistance in series with the diaphragm of sufficient magnitude to give a long time-constant.

Under the above conditions the loudspeaker is an almost linear device, and harmonic distortion is extremely low. An unusual feature of this push-pull device is that the second harmonic will always be greater than any other; furthermore, it can be shown that if the second harmonic is reduced all the higher harmonics are reduced simultaneously!

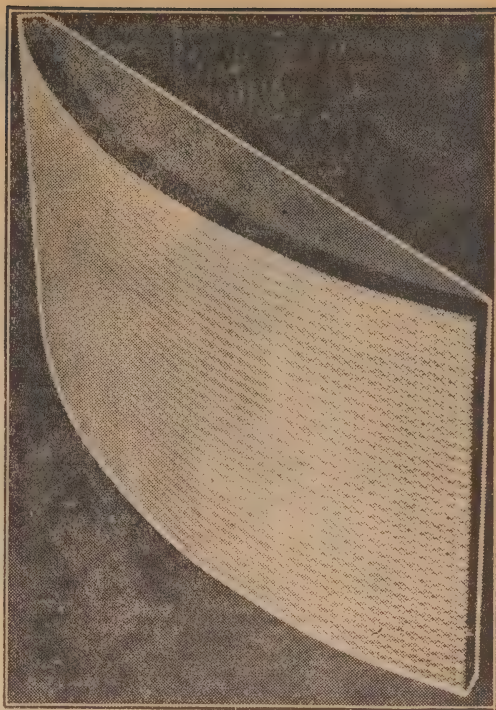
PER CENT!

At volume levels sufficient for a small hall, the particular type of loudspeaker illustrated in Fig. 7 has measured distortion content over its working range of approximately 1% per cent! This result may be considered incredible, and it is therefore worth recalling that incredulity is also expressed when the author produced the very low-distortion amplifier (the original "Point One") in 1945.[4] Strangely enough, there is often resistance to progressive developments, both in the arts and sciences.

Fig. 8 shows that the frequency response of the loudspeaker in the horizontal plane is excellent, and its high frequency response is maintained off the axis because of the curved construction. However, in the vertical plane the response will be more directional if the total area of the diaphragm is used as the radiator for high frequencies.[5]

Broader directivity can be obtained by sub-dividing the diaphragm and/or fixed plates, and dividing these separate areas through electrical dividing networks connected to tappings on the trans-

Fig. 7: A developed balanced push-pull electrostatic loudspeaker.



former. A further advantage can be obtained from this expedient because it tends to minimise the variation of load impedance with frequency. [6] A neat solution of these directivity/impedance problems is offered by Janszen, who uses a diaphragm coated with resistive material.[7]

The absence of rapid changes in the frequency characteristic is indicative of a transient response superior to any other form of loudspeaker (excepting the Ionophone).[8] A gaseous device previously investigated by the author). Corrington confirms that a similar type of balanced-push-pull electrostatic loudspeaker gives transient decay measurements greatly superior to those of any other loudspeaker tested in the RCA acoustics laboratories.[2]

The acoustic output from this type of balanced-push-pull electrostatic loudspeaker is of the same order as from conventional cone loudspeakers. Its sensitivity is therefore satisfactory, in direct contrast with the single-sided system.

From the above performance details the reader may deduce that in this particular case it is possible to disagree for the first time with the dictum that "the loudspeaker is the weakest link in the chain". Any record-pickup combination and any transmitter/receiver combination (FM included), will have greater distortions than this particular loudspeaker.

REVOLUTIONARY

This is, of course, a revolutionary engineering situation, but the reader may ask, "Does this loudspeaker sound revolutionary?" The short answer is, "It most certainly can do so, but much depends on the goodness of the bass woofer which must of necessity be heard simultaneously."

Now, there is little to choose between the better few of available conventional 15in woofers, and when the balanced-push-pull electrostatic tweeter of Fig. 7 is properly married to such a woofer the overall quality of reproduction is voted a notable advance by the majority of listeners.

A further noticeable improvement in sound quality can be effected by using novel constructions and materials for the woofer, and it has thereby been found possible to eradicate or ameliorate three significant distortions common to all the contemporary woofers investigated by the author. However, these developments make another story, and it must suffice to say here that a greatly improved tweeter needs and deserves a greatly improved woofer.

To sum up: the author believes that the development of balanced-push-pull electrostatic loudspeakers will rank in importance, as an advance in listening quality, with the advent of the Rice-Kellogg moving-coil loudspeaker in 1925 and with the introduction of very low-distortion amplifiers in 1945.

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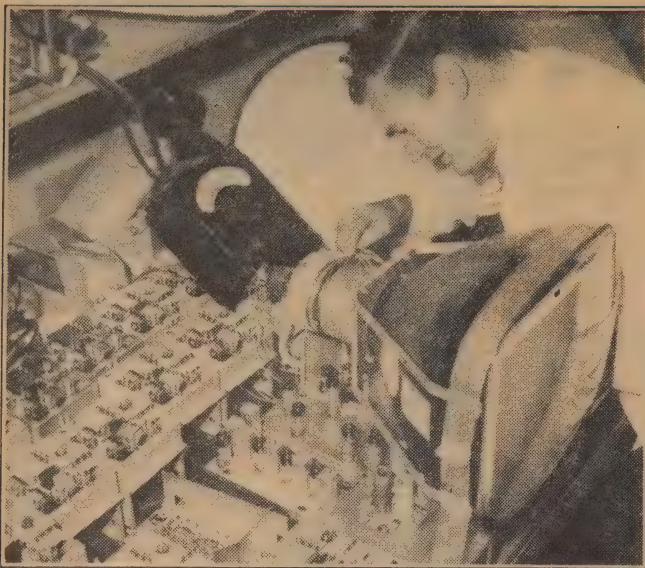


Figure 1: For some years engineers in the major Australian radio factories have been working quietly on prototype television receivers. Pilot runs have been put through to discover assembly problems and manufacturing costs. Very soon the rush will be on to produce, buy, instal—and service—the nation's TV receivers.

We can only suggest that you find each issue, or, if you feel inclined, cut out the relevant pages and paste them in a large scrap book. This way you will have your television course in one piece for handy reference.

Our course will start in the television studio, with a glance at the picture to be televised and the means whereby its light and shade are translated into electrical signals capable of being amplified and broadcast by a radio transmitter.

We shall follow the picture signal and its accompanying sound to the receiving aerial, thence through the various stages of the receiver to the point where the signals divide, one to operate the picture tube and the other the loudspeaker.

We shall examine the timing signals which are necessary to keep transmitter and receivers in step, that viewers see a steady image, not one that flickers and jumps like the picture from a broken-down movie projector!

We shall examine the special features of a television receiver: its tuning system, its IF channel and valve complement, its picture control circuits, its power supply arrangements, its sound channel and so on. But let's not make it sound too complicated; these subjects are some months away.

Let's start in right at the beginning.

A COURSE IN TELEVISION

Within the next twelve months, television will have become a "hot" topic of conversation in Australia. By all present indications, receivers will be on sale and preliminary programs on the air. Servicemen will be wondering about the problems to come and readers speculating on the chances of building their own receiver. Our new course in television is designed to bring you up to date in this most important subject.

IN framing the course, we have tried to anticipate the needs and the approach of the average reader of *Radio, Television and Hobbies*.

We visualise this "average" reader as someone who is reasonably familiar with ordinary radio terms, components and circuitry. At the very least he has built a few receivers and amplifiers but he probably isn't too happy with maths, graphs and formulas beyond secondary school standard.

HOW IT WORKS

Right now, he wants to know how a television set works and, better still, how to make it work again when something goes wrong.

In other words, our average reader is likely to be a radio serviceman, a dealer or technician, a "Ham" or someone for whom radio has been a long-standing hobby.

This being so, we are not going to concern ourselves with the basic elements of radio theory, nor are we going to the other extreme, to get bogged down in a mass of design

PART ONE

data which really concerns a components engineer.

Our job is to explain the principles of television, insofar as they concern the "average" reader, to discuss and illustrate typical components and the kind of circuits in which they are used. If we can do this without the articles becoming too involved, we will have accomplished our aim.

Approached on this basis, the reader's main problem will not be to understand individual articles but to remember what has gone before.

Have a look at the picture on the foot of the next page. In its original form, it was an ordinary Press release photograph, with plenty of detail and contrast.

As it appears on the printed page it might still be accepted as the picture of an attractive model, not unlike dozens of other pictures which appear every day in the newspapers.

If you look closely into it, however, you will find that it isn't homogenous picture at all but pattern of tiny black dots.

In some parts of the picture, the dots are quite small and obscure very little of the white surface on which they are printed. To the eye these areas appear nearly white, at most, a light grey.

DARKER TONES

Elsewhere the dots are much larger, actually merging in some areas to obscure the paper surface almost completely. To the eye, these areas appear as tones of dark grey through to black. So the varying proportions of white to black

by **W. N. Williams**

as across the surface of the picture produce the illusion of various tones of grey, corresponding to those in the original photograph. To illustrate the point more clearly, we had our blockmakers enlarge one section of the picture, to a point where the dots appear as a very coarse pattern. In fact, those "flying Irish eyes" are revealed as a grotesque conglomeration of black and white spots.

Look at this enlargement close up, and try again at arm's length. It will prop the magazine up and show the enlargement from a distance of several feet. You will find that the pattern of dots and spots merges into a quite acceptable picture of a young lady's left eye!

Blockmakers do not superimpose a dot pattern (a screen) on pictures for the fun of it, but necessarily. Only by "taking the picture to pieces" and presenting it as pattern of tiny black and white areas, are they able successfully to reproduce a half-tone photograph on a printed page.

PRINTING PROBLEMS

The optimum size and spacing of dots is determined by the kind of paper on which the reproduction must appear, the kind of printing press, the kind of ink and the speed of printing. Illustrations printed on newspaper on high-speed rotary presses normally use a fairly coarse screen, which can be seen quite readily if you look for it.

Magazines printed by different presses on more expensive paper use illustrations with a screen so fine that it defies detection with the naked eye. As a result, the illustration looks more like an original photograph and the detail is far better than is possible using a coarse screen.

But why have we said all this? Simply to emphasize certain basic facts, as under:

1. The pictures we normally look at in papers and magazines are not a single entity but a composite of tiny black and white areas. This is even true of original photographs which are built up from grains or bumps of metallic silver.
2. Our eyes will accept such a composite as a complete, unit picture, provided the components are small enough in relation to the picture area, the viewing distance and the detail which the eyes can resolve.

VALUE FOR TELEVISION

This last observation is just as basic and important to television as it is to printing, because there is no known way at present of transmitting a picture electronically in bulk from one point to another.

Picture transmission relies entirely on the principle of "taking the picture to pieces" and reassembling it piece by piece at the far end. The smaller the pieces into which it can be divided, the better will be the detail in the distant reproduction. It would seemingly be ideal if every picture or scene to be televised could be divided into segments as small and as numerous as the dots in a printed picture; then, each of the areas could conceivably be linked to an equivalent area on a view-

ing screen, so that what looked bright on the original would automatically look bright to the viewer and so on.

Unfortunately, such a scheme is not practical because it would require a separate signal channel for each dot or area in the picture — and there are obviously tens of thousands of them.

To avoid this requirement, the only possible alternative is to analyse the picture in a sequential fashion, sector after sector. By converting this information into electrical signals, suitable for transmission and reception, the scene can be reconstructed at a remote point, using only a single channel.

The usual process of picture analysis is known as "scanning".

SCANNING PRINCIPLE

Let's say that we wanted to "scan" the picture below for purposes of transmission. We might set up apparatus which would shine a small but intense spot of light in the extreme top left corner of the picture. We might arrange a collector lens, facing the picture, to gather the light reflected back from the surface of the picture and focus it on to the cathode of a photoelectric cell.

Since the upper left hand corner of the picture is very dark, little light would be reflected off it and the photocell current would be quite small.

Now let's assume that the spot of light is moved progressively to the right. At a certain point in its travel, it would encounter a somewhat lighter area. The reflected light would therefore increase and with it the cell current.

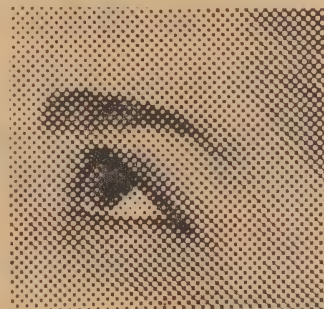


Figure 2.

The picture on the right is an ordinary magazine illustration composed, if you look closely, of a pattern of fine dots. A small sector is shown enlarged above.

Figure 3.

Just as the eye accepts this dot-pattern as a complete picture, so does it merge the lines in a television image.



Approaching the right hand corner of the picture, the moving light spot would encounter a further black area and the photocell current would therefore revert to its original low value.

In other words, the variation in photocell current, as the light spot travels from left to right, would represent a signal proportional to the light and shade of the image.

One movement across the image constitutes a single scanning line.

On completion of the first scanning line, along the extreme top edge of the picture, the spot might well be swung back to the left-hand side to a point just underneath its original position. It might then be moved progressively to the right again, to analyse a second narrow strip of the picture immediately beneath the top line.

So the analysis could continue, line by line, till the whole surface of the original picture has been examined.

Figures 4 and 5 illustrate in detail the path which would be followed by a light spot scanning a complete picture. It is assumed to move steadily from left to right to complete each line, flicking back to the left-hand edge to start the next line.

SIMPLE SCANNING

Because the lines follow one upon the other in simple order, this type of scanning is known as "simple", "sequential" or "progressive" scanning, the terms meaning the same thing.

A familiar and elementary adaptation of this general principle is seen in the equipment currently used to transmit news pictures by telephone or radio.

The original picture is wrapped around a drum and slipped into position in the "picturegram" machine. For purposes of transmission, a bright spot of light is made to travel along one edge of the picture; a photocell assembly responds to the reflected light and generates a signal which varies according to the light and shade of the image.

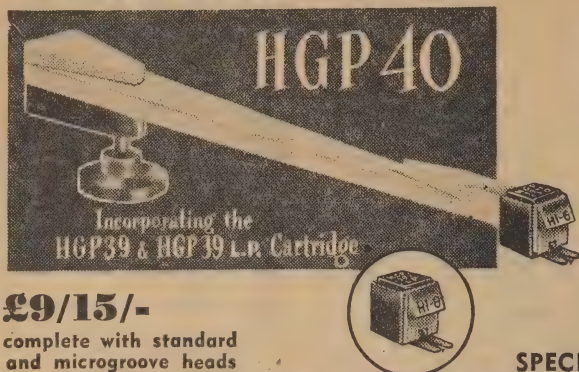
At the end of the line scan, the light moves rapidly back to its starting point, while the drum rotates by just enough to place the next scan alongside the one just completed. So the process continues until the complete picture has been scanned.

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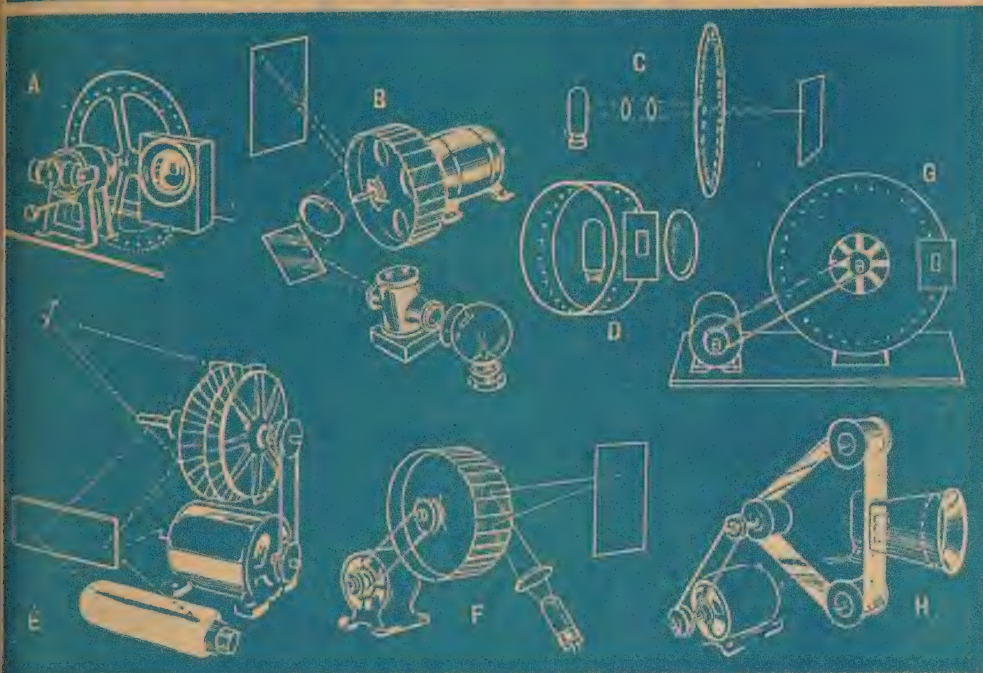


Figure 7: This block, reprinted from our earlier television course illustrates some of the early types of mechanical television scanning apparatus. (A) Receiver using Nipkow disc and lens. (B) Receiver using a drum scanner and a Kerr cell to modulate light from an ordinary globe. (C) Projection type disc scanner. (D) Similar to (A) but using a drum scanner. (E) Disc with inclined mirrors. (F) Mirror drum with mercury light source. (G) Nipkow disc with belt drive. (H) Belt type scanner.

are meanwhile amplified and then fed directly into a telephone line or used to modulate an ordinary radio transmitter.

At the receiving end, the signals are fed to a second equipment, which has been set up to operate as a recorder. Here the signals are used to vary the intensity of a light beam shining on a piece of photosensitised paper.

MOTORS SYNCHRONISED

The driving motor in the receiving device is carefully synchronised with that at the transmitting end, so that the to-and-fro movement of the scanning spots in both equipments is precisely the same.

Thus, the variations in cell output as the beam scans the original picture, control the intensity of the light which is focused at each instant on to an equivalent spot on the sensitised paper in the receiving equipment. After development, the image becomes visible.

By changing the phase of the reproducing signal, it is possible to make the receiver produce either a "positive" print or a "negative" transparency from which any number of photographic copies can be made. Other methods of copying have been devised, but these are not important in the present discussion, which is primarily concerned with the principle of scanning.

Figure 7 (overleaf) is a sector of an early wirephoto, which has been grossly enlarged to emphasise the line structure. The reproduction, as you see it, also carries the dot structure necessary for printing purposes, so that little of the original definition is left. However, it should serve as an illustration of what we have been saying.

It so happens that the lines in this picture run vertically, but this is purely because it was loaded that way on to the drum. It does not alter the principle of what has already been said.

Modern picturegram equipment,

operating under favorable conditions, can produce pictures at the receiving end with a line structure so fine that it is hard to detect with the unaided eye. The definition is far better than is necessary for ordinary newspaper reproduction. But we must pass on:

TELEVISION IS DIFFERENT

The transmission of a single picture by line or radio link is a leisurely operation, comparatively, because it generally does not matter if it takes several minutes to scan and reproduce the said picture. Television is a very different story.



Figure 4: Illustrating how the scanning spot moves across the subject discovering light and dark areas.

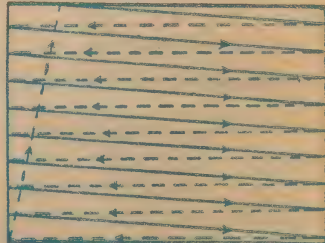


Figure 5: The path traced out by the scanning beam during one simple, progressive scan. Dotted lines are return traces.

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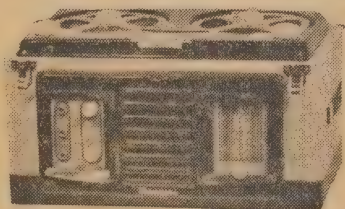
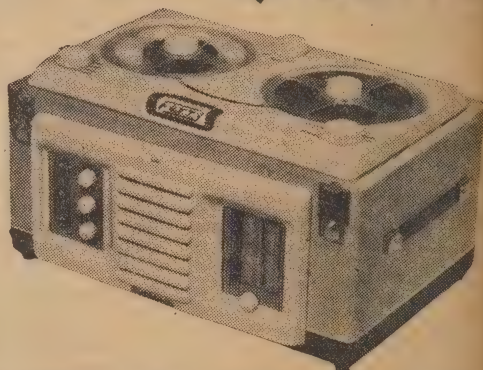
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the first place, the reproduced image must be presented directly to the eyes of the viewer, so that there is no room for any photographic process to intervene. The image must be in the form of a light pattern.

Secondly, since "moving pictures" are required of a television system, it must be capable of presenting to the eyes of the viewer a rapid succession of "still" pictures as happens, for example, in the cinema.

To meet these requirements, a variety of mechanical gadgets were devised for the early television systems (1930 onward). Some of these gadgets are illustrated on the previous page. (Figure 7.)

KOW DISC

Perhaps the best known was the Nipkow scanning disc, illustrated in diagram "A". The viewer looked through a lens system on to a flat cathode in a neon-type glow lamp. Light surrounding this cathode was modulated by the incoming picture signal.

Interposed between the lens and the lamp was a disc, punched with a series of holes having the same pattern and spinning at the same speed as the scanning disc at the transmitting end. The holes were placed so that only one tiny sector of the original image or the glow lamp was exposed at the one instant.

The diagram illustrates a vertical scanning action, as used in some early systems, but this need not cause any confusion.

Figure 8, below, indicates the setting at the transmitting end, where the subject's face is illuminated by light source shining through holes in the spinning disc.

At a particular instant, for example, the scanning disc at the transmitting end might expose a highlight in the original scene in the left-hand corner. It would produce a corresponding picture signal to cause the lamp at the receiving end to glow brightly.

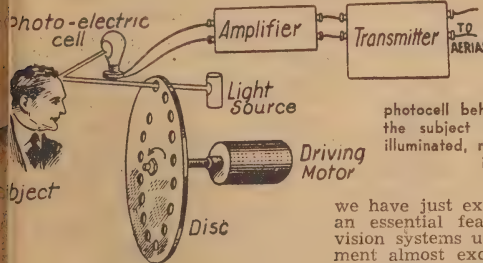


Figure 8: Illustrating the principle of a disc-type television. By placing the photocell behind the scanning disc, the subject could be permanently illuminated, reversing the conditions illustrated.

Assuming that the discs were properly synchronised, the viewer would therefore see a bright spot of light in the corresponding position. The light value would normally vary, however, as the same hole in the disc sweeps along the edge of the original scene and its reproduced image.

As the first hole moves out of the field of vision, the second hole would appear at the top, ready to commence a scan exactly alongside the first just completed. So the process would continue, line following line, until the whole surface of the image had been scanned.



Figure 6: This picture, received by an early type of picturagram equipment, has been enlarged to emphasise the line structure. It illustrates very clearly how an image can be built up, as it is in television, from a succession of lines placed one alongside the other.

At the completion of the picture scan, the first hole would be in the proper position to commence the first line of the next scan, and so the process would repeat itself, line following line and picture following picture in rapid succession.

A variety of other gadgets were devised to give a similar scanning effect and some of these are illustrated in the accompanying diagram. The more elaborate ones used a system of inclined mirrors or even inclined lenses to direct a beam of modulated light on to a viewing screen in the appropriate scanning pattern.

In practice all such schemes are out-dated and there is no point in trying to study them in detail. Although the scanning principle, which

is a "still" representing progressive steps in the action being depicted.

Persistence of vision prevents the audience from noticing the blackout periods between pictures and also smooths out the tiny increments of action into what looks like smooth movement. Only on very rapid movements across the screen is any jumpiness noticeable.

Television presentation makes an even greater demand on the eye than this because it never does present a complete picture at a time. The eye to constitute complete pictures from the flying light spot and then build up from the pictures so retained the impression of smooth motion.

FLICKER EFFECTS

As might be expected, freedom from flicker and a smooth movement of the image are only obtained if the scanning process can be speeded up sufficiently to present to the viewer a certain minimum number of complete pictures per second.

Motion on the most elementary motion picture equipment, this calls for at least 32 pictures per second—in other words at least 32 complete scans per second.

Additionally, of course, the picture can only have real entertainment value if it is bright enough, large enough and capable of showing a reasonable amount of detail.

In general, the mechanical systems illustrated in figure 7 failed to satisfy these requirements. Initially they gave only a very crude picture and attempts to improve definition, and picture size involved more bulky equipment and prohibitive rotational speeds for the scanning disc.

Hence the adoption, as already mentioned, of electronic methods of scanning and picture presentation. We shall not be able to proceed much further, then, without pausing to study the principles of the cathode ray tube.

(To be continued)

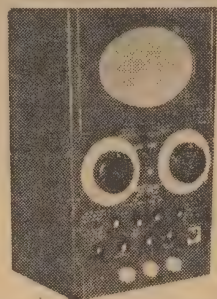
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24V 250V 60MA	1 5 0
12V 270V 100MA	3 15 0
12V 500V 350 MA	8 10 0
12V 1200V 200MA	6 10 0
6V 500V 150MA	6 10 0

THE COLOR CODING OF RESISTORS

Most resistors in use in Australia are color coded according to the system adopted by the Radio Manufacturers Association (USA). At the request of many readers, the basis of this code is explained below.

SEPARATE colors are used to represent the numerals 0-9, and the color combinations are used to express the resistance value directly in ohms. The colors have the following significance: black 0, brown 1, red 2, orange 3, yellow 4, green 5, blue 6, violet 7, grey 8, white 9.

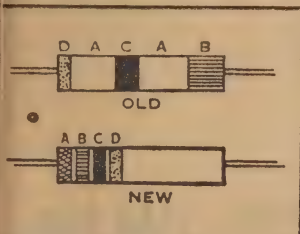
In the older system the first figure the resistance value is represented by the body color (A). Thus if the main body of the resistor is red it follows that the first figure in the resistor value must be "2".

The second figure in the resistance value is shown by the end color (B). The significance of the individual color remains unaltered, that, if our previously mentioned resistor has a green end, the first two significant figures would be "25".

COLOR DOT OR BAND

The color dot or band at the centre of the resistor (C) shows the number of noughts which have to be added after the first two significant figures.

A black dot would indicate no noughts and therefore the resistance value would be merely 25 ohms. With a brown dot, the resistance



value would be 2-5-0 or 250 ohms. In the case of a 2500 ohm resistor, the dot would obviously have to be red, and so would not be apparent in the red body. Hence, if no dot is apparent, it can be assumed that the color of the dot is the same as that of the body.

By way of example, one may encounter a red resistor with a black end. Referring back to the list, the first two significant figures must be "20". The dot must be assumed to be of the same color as the body, i.e. red. This signifies two noughts, so that the value becomes 2-0-00, equals 2000 ohms.

ANOTHER EXAMPLE

To take another popular example, a green resistor with black end and yellow dot or band is 5-0-0000 equals 50,000 ohms or 0.5 megohm.

It will be apparent that the coding system does not lend itself to resistance values requiring more than two significant figures ahead of the powers.

The accompanying table sets out the colors and figures in a form which simplifies the transfer from

RESISTOR COLOR CODE

Table showing popular preferred values of resistors in the R.M.A. color code.

Resistance in ohms	A	B	C
2200	Red	Red	Red
3300	Orange	Orange	Red
4700	Yellow	Violet	Red
6800	Blue	Grey	Red
10,000	Brown	Black	Orange
15,000	Brown	Green	Orange
22,000	Red	Red	Orange
33,000	Orange	Orange	Orange
47,000	Yellow	Violet	Orange
68,000	Blue	Grey	Orange
100,000	Brown	Black	Yellow
150,000	Brown	Green	Yellow
220,000	Red	Red	Yellow
330,000	Orange	Orange	Yellow
470,000	Yellow	Violet	Yellow
680,000	Blue	Grey	Yellow
1 Megohm	Brown	Black	Green
1.5 Megohm	Brown	Green	Green
2.2 Megohm	Red	Red	Green
3.3 Megohm	Orange	Orange	Green
4.7 Megohm	Yellow	Violet	Green
6.8 Megohm	Blue	Grey	Green
10 Megohm	Brown	Black	Blue

color code to resistance value and vice versa. The second table shows the color codes directly for a selection of the most commonly encountered resistors in the "preferred values" range.

To simplify production the older marking system has now been replaced by a new system which presents the colors in a somewhat different manner.

Instead of being applied to body, end, and band, the significant colors are applied as three parallel bands around the resistor and toward one end. The body color of the resistor has no significance whatever.

SAME SIGNIFICANCE

Hold the resistor so that the color bands are toward the left and read off the colors from the left to right. The colors have the same significance as before, so that no difficulty should be encountered on this score.

Assuming that the color bands on a resistor were, left to right, red, green and yellow, the resistance value would be 2-5-0000, or 250,000 ohms. Occasionally a fourth band is added, on the right, of either silver or gold. A silver band signifies that the resistance value is within 10 pc of the marked value, while a gold band indicates a 5 pc tolerance.

The use of color bands instead of body, end and dot colors should occasion no confusion, provided you remember to hold the resistor with the bands toward the left and read off the colors from left to right.

R.M.A. RESISTOR COLOR CODE—Values in ohms

Body Color	First Digit	End Color	Second Digit	Dot Color	Remaining Digit
Black	0	Black	0	Black	—
Brown	1	Brown	1	Brown	0
Red	2	Red	2	Red	00
Orange	3	Orange	3	Orange	000
Yellow	4	Yellow	4	Yellow	0000
Green	5	Green	5	Green	00,000
Blue	6	Blue	6	Blue	000,000
Violet	7	Violet	7	Violet	0,000,000
Grey	8	Grey	8	Grey	00,000,000
White	9	White	9	White	000,000,000

RESISTOR WATTAGE RATINGS

DEPENDING on their size and construction, resistors are able to dissipate a certain amount of heat without physical damage or undue changes in their electrical resistance.

The wattage involved can be calculated by squaring the voltage figure across a given resistor and dividing the result by the resistance in ohms.

Alternatively, the current in milliamps through the resistor can be squared, multiplied by the resistance in ohms and divided by 1-million.

As a general rule it is not ad-

visable to operate resistors in confined spaces at more than about half their rated maximum dissipation. In cases of doubt, greater reliability can be expected if a larger resistor can be installed.

Where the dissipation approaches or exceeds 1-watt, the limit for standard carbon resistors, two such resistors can be used in parallel, each double the resistance value required. Thus two 50,000-ohm 1-watt resistors in parallel give an effective value of 25,000 ohms at 2 watts.

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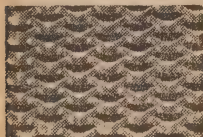
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13 x 7 x 2 4A17	14/-
13 x 10 x 2 4A18	17/6
17 x 8 x 3 4A19	22/6
17 x 10 x 3 4A19	25/6
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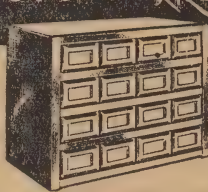
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A.C. Grid Dip Osc. (p. 60)	Grid Dip Meter (p. 8)
JULY ISSUE	SEPTEMBER ISSUE
2 Band S/Wave Converter (p. 48)	High Powered Playmaster
3 Stage Transistor Set (p. 60)	Audio Signal Generator (p. 32)
Clock Radio (p. 64)	1955 Radiogram (p. 94)

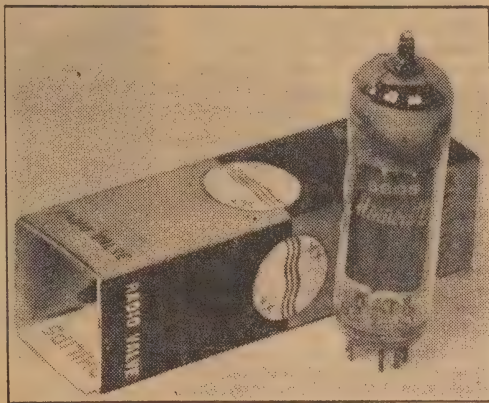
We supply the parts, but cannot enter into any technical correspondence.

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TRADE NOTES AND NEWS

EL84 NOW KNOWN AS 6BQ5



☆
The 6BQ5 medium
power output valve.
It has been known
by the name EL84.

NEW GERMAN MICROPHONES

Among the items exhibited by R. H. Cunningham Pty Ltd. at the recent IRE Convention in Melbourne, was a range of acoustical microphones made by Laboratorium Wennebostal of Germany. These microphones have unique placement of the dynamic moving coil unit. Normally, this is at the top of the microphone and therefore vulnerable to shock and weather conditions.

In the case of the L.W. microphones, with the moving coil unit located in the base, the microphone is rendered virtually unshockable and is waterproof.

The sound is conducted to the unit by a slender alloy tube, built in such a way as to be acoustically balanced from the mouthpiece to the dynamic unit chamber. The result is a very high quality microphone, while unobtrusive in appearance, and possessing a light weight base (in the case of the floor models, approximately 3½lb), which is virtually impossible to tip over when worked under normal circumstances.

In the case of the desk model, the unit housing is not very much bigger than a billiard ball, and the sound column tubing being so slender in dimensions, would pass practically unnoticed in front of a speaker or lecturer.

Three models were exhibited at the Convention.

The Model MD3, which is a standard type with a straight tubular column, has a frequency range of 30-20,000 cycles, with an output impedance of 200 ohms.

THE high slope EL84 output valve which has recently made its appearance in Australia seems likely to become the standard medium power output valve.

Its characteristics make it suitable, under a wide variety of plate voltages, for most purposes, including both standard radio receivers and higher powered output stages and amplifiers.

Philips have advised that in future they will sell this valve in Australia under its RTMA type number of 6BQ5.

There will be no alteration in the valve characteristics as a result of this change.



The MO3T desk microphone.

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CONTENTS...

An outline of the television process
Basic signal and circuit theory
The picture tube and its auxiliary circuits
Scanning (time base) circuits
Synchronising circuits
The video signal circuits
The sound channel
The complete receiver
The receiving aerial system
Receiver test equipment and procedure

Colour television
Mathematical and bibliographical notes

We can highly recommend this publication, but would advise that we hold only a limited number of copies; more will be coming at the beginning of October.

SEND FOR OUR BOOK LIST!

The above books are in addition to those shown on our brochure.

Please note that all the books advertised in the preceding two issues of "Radio, Television and Hobbies" have sold out. We will, once again, have Australia's largest stocks at the end of September.

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COMPANY (AUSTRALIA)

9-11 Cadow Street, Pymble, N.S.W.

BOOK REVIEW

"SIMPLE Electronic Musical Instruments For The Constructor" by Alan Douglas. 72 pages, stiff paper cover.

Interest in electronic musical instruments is very high at the moment and readers wanting to know something about the subject without too much outlay will welcome this book by Alan Douglas.

The approach is essentially practical and, after a brief theoretical introduction, the author sets out to describe the construction of several of the simpler types of musical instrument. These include a couple of monophonic keyboard instruments, an electric accordion, electric guitar and a pedal attachment for pianos or reed organs.

A separate chapter is devoted to percussion, attack and delay circuits. There are plenty of circuits and illustrations to study.

Our copy of the book came from the Electronic Organ Company (Aust.), 9-11 Cadow St., Pymble, NSW. Price quoted is 7/6.

From the same company comes another small book "Transistors and Crystal Diodes" by B. R. Bettridge of the Osram-G.E. Company, London. Price of this 72-page book is also quoted as 7/6.

It should be a helpful little book for anyone wishing to supplement the information already published in this magazine.

BRAMCO OFFERS AUDIO SPECIALS

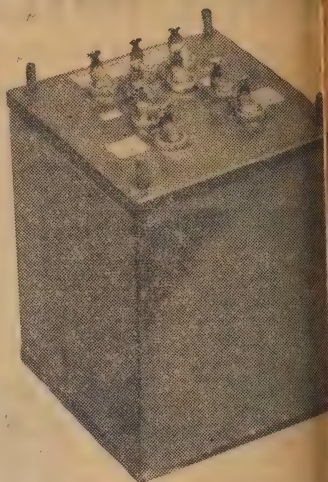
In order to cater for many cases where special audio components are needed, Bramco Radio Components, of Wallsend, are prepared to design and supply, with particular reference to transformers and chokes. In addition, a number of standard lines will be available.

IN the audio field, particularly since the rapid growth of wide range amplifying equipment, a circuit designer needs are not always obtainable "off the shelf".

Many of the larger transformer manufacturers at times have difficulty in handling orders which call for unusual windings, particularly when they are busy with long runs of stock items.

Realising this, Bramco are specialising in looking after such requirements, and are able to give each order individual attention.

This special order department is also able to supply accurate inductances for cross-over networks as used in loud speaker connections and various types of high and low pass filters. These are normally wound on strong, wooden bobbins with a single



A 10-watt Bramco transformer wound for 6V6 valves with 5 per cent ultra-linear tapings.

mounting bolt, and will be impregnated if required.

Bramco Radio Components may be contacted at 83 Nelson St., Wallsend, Phone LL921.

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ACOS RELEASE CERAMIC UNIT

The popularity of the crystal type pick-up cartridge is sufficient evidence of its dependability under average conditions of temperature and humidity. But in tropical areas failures are not uncommon under conditions where many other things suffer rapid deterioration.

For some little time, pick-up manufacturers have been experimenting with a new type of cartridge with a barium titanate element in place of the Rochelle salt used in crystals.

These "ceramic" pick-ups are not susceptible to heat changes considerably beyond the atmosphere temperature, and are virtually impervious to moisture.

The main difficulties have been to obtain sufficient output together with satisfactory mechanical compliance in manufacture.

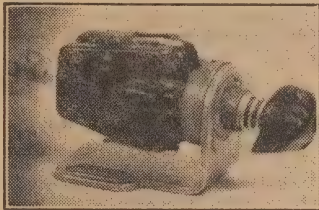
The new Acos ceramic cartridge therefore be greeted with considerable interest as one of the first practical models yet manufactured, the first to be seen in this country.

WILL REPLACE HGP37

It will not replace the crystal type in general use, but is recommended in its stead for areas where failures have shown a high percentage of failure.

Its output is slightly below that of the HGP37 which is its nearest equivalent, but the makers claim it is near enough to be considered a direct replacement.

Its own type number is GP61. The turn-over head has two independent styli for standard and LP records. Each is replaceable at a cost



The Acos ceramic cartridge

of about 12/-, and is fitted with a sapphire tip.

A feature of the head is a lock for both playing positions as well as the mid or "half-turn" position in which the head is left when not in use.

A protrusion on the bakelite housing forms a rest for this mid-position.

The head is complete with a metal bracket punched with standard slotted holes and will therefore fit many popular arms.

Its price is £3/19/6, which is somewhat dearer than the crystal type. Initial shipments will be mainly for tropical areas where the head is most valuable, but eventually it will be universally obtainable.

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FREQUENCIES AND
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WAVELENGTHS

This suppressor unit, manufactured by Belling-Lee of England, is intended for insertion in the power leads of domestic equipment to filter out possible electrical interference with TV programs. It is one of many TV components handled by R. H. Sunningham, of Melbourne. They are available through various radio trade houses although the sample photographed above came from Messrs. Lawrence & Hanson Electrical Pty. Ltd., of 33 York Street, Sydney.



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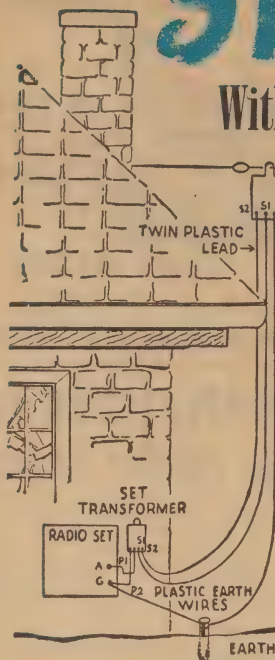
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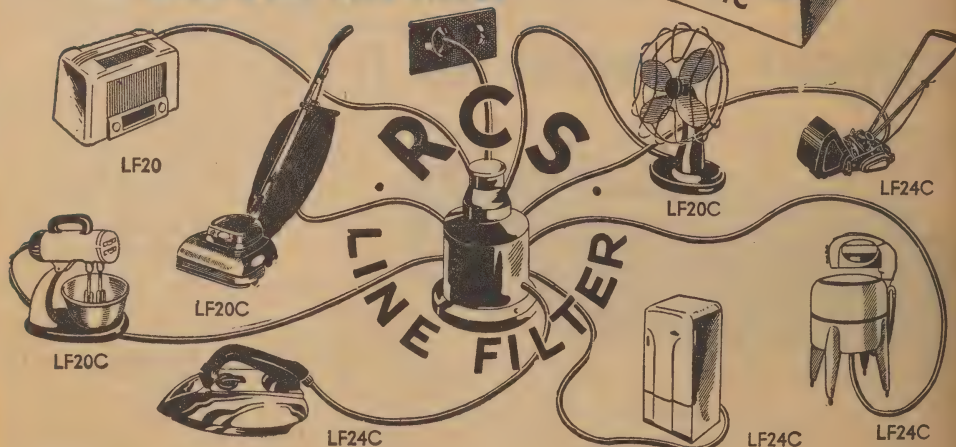
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CONFINE NOISE WHERE IT STARTS — WITH R.C.S. LINE FILTER



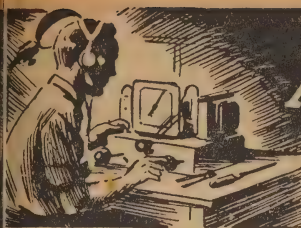
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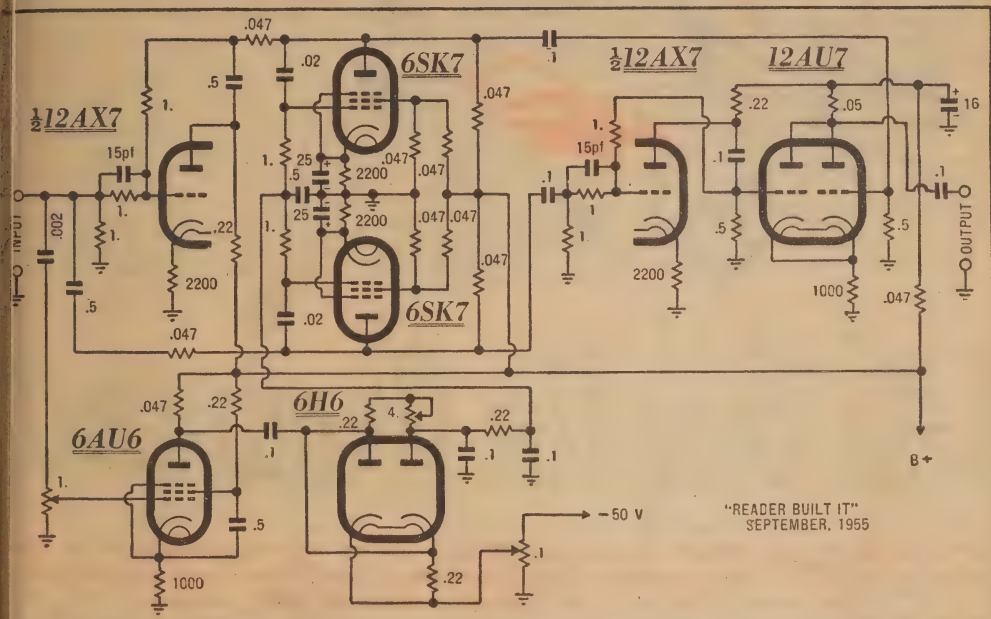
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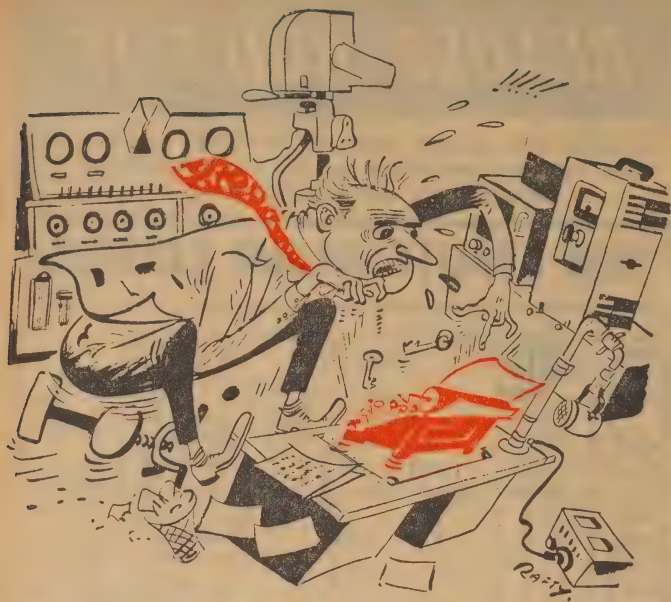


A READER BUILT IT!

Gadgets and circuits which we have not actually tried out, but published for the general interest of beginners and experimenters.

CIRCUIT DETAILS OF HIGH QUALITY VOLUME EXPANDER





audience, but there it was.

Our friend from Hay, whom I shall henceforth refer to as T, takes up the cudgel on behalf of those who can allegedly benefit from improved signal-to-noise ratio in the receiver.

He says that his nearest station is 2QN, 80 miles away. Then follows 2RG, 100 miles away, 2WG, 180 miles and 2CO at 200 miles. There are plenty of more remote places of course, but his problem is bad enough.

RF GAIN

T.S. writes with the air of someone who has been fiddling with radio for a good while. He takes it for granted that an RF stage is essential for good results, but he goes farther.

Having explained that "noise" in receivers is a problem out there, he goes on to say that he has tried twin-triodes in place of the conventional RF and converter valves, and in each case, there was a notable improvement in signal-to-noise ratio. Why don't receiver designers walk up to themselves?

Figure 1 shows the RF amplifier stage, which T.S. substituted for the original pentode in his tuner. It gave about the same gain, judged on an S-meter, but was less noisy than the pentode.

Let's Buy An Argument

Continuing last month's theme about circuit design, I have to hand an interesting letter from a reader in Hay, NSW, who re-awakens the old question of signal-to-noise ratio and the use of low-noise "front-ends" for broadcast receivers in country districts.

IT is one of those subjects, which somebody unearthed, every now and again. Receiver design engineers say "Oh . . . er . . . yes . . ." and then go on to talk about something else. They seem quite contented with their conventional circuitry and quite unconvinced by arguments to the contrary.

The reason for this apparent lack of concern is very simple, in that the inherent signal-to-noise ratio of a receiver is not a problem to the vast majority of present-day set-owners. Why worry about it, then?

LOCAL STATIONS

Most radio listeners live in the cities, anyway, and their sets are seldom tuned to any but the local stations. Interest in other stations is rather fleeting and nobody loses much sleep if they can't be heard properly.

Then another goodly section of the populace lives in areas cursed by power line leaks and other forms of man-made interference. This blankets the weaker stations so effectively that the noise characteristic of the set itself doesn't need

to be anything out of the ordinary.

Just how far this line of thinking has been pursued is illustrated by a statement which I heard some time ago from a prominent receiver design engineer. Cutting right across preconceived notions, he suggested that RF stages were largely redundant in modern domestic receivers.

(a) Because people only want local stations;

(b) Because man-made interference blankets weak stations anyway;

(c) Because modern circuits, valves, and aerial coils in particular, provide the same order of performance as was once available from older sets using an RF stage.

I might say that this claim caused a few raised eyebrows among the

His next step was to restore the pentode RF amplifier and wire the same twin-triode in place of the original converter, a 6J8-GA. This gave an even more marked improvement than replacing the RF stage and that is the way the tuner is wired at present.

FIRST IF STAGE

His circuit is reproduced in figure 1 and T.S. says that he is just waiting for enough time to reinstall the twin-triode RF stage and possibly substitute a similar stage in the first IF amplifier for good measure. Then he'll really have the noise problem licked!

He points out that a noise limiting detector is built in permanently because elimination of periodic static crashes is far more important than an occasional bit of distortion or modulation peaks.

The extra selectivity afforded by two IF stages is well worth having and the built-in line filter is a worthwhile refinement.

In short, his recipe for a countryman's radio tuner adds up to this: Twin-triode RF amplifier, twin-triode frequency changer, twin-

by **Neville Williams**

READER'S 'RECIPE' FOR COUNTRYMAN'S RADIO TUNER

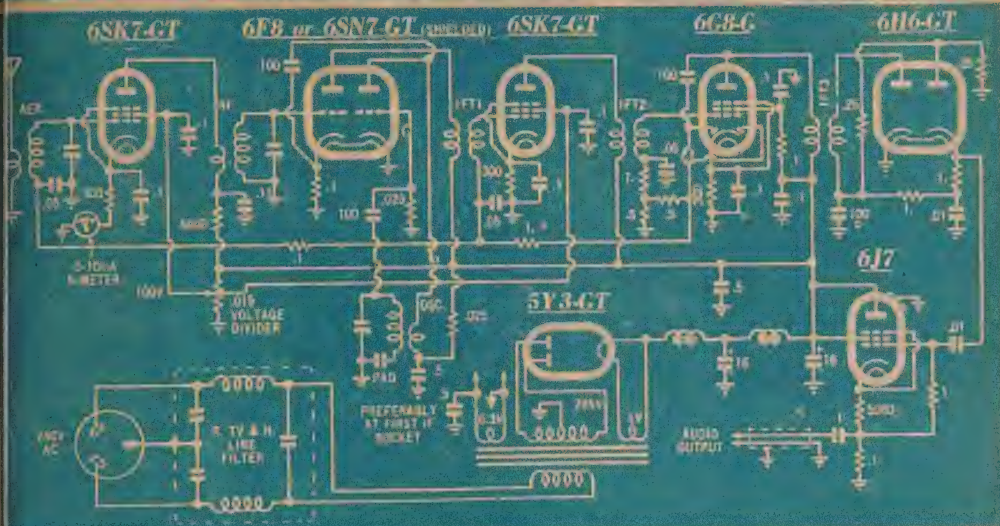


Figure 1: A reader from Hay, NSW, suggests that this tuner can give a much better signal-to-noise ratio than one using a conventional converter valve. A further improvement, he suggests, would be to add the twin-triode RF stage shown below.

de 1st IF amplifier, pentode 2nd. amplifier noise-limiting detector, (possibly) a cathode-follower out valve to the main amplifier. Such a tuner could have no pre-tune to high fidelity. His problem, however, is not to catch the last bit of modulation, but to get any modulation at all! High fidelity listening has to come from his own record playing equipment.

What do I think about all this? Frankly, I take T.S.'s remarks with a proverbial "grain of salt", not because I question his observations, but rather the grounds on which they are made.

RIAL COIL

It would be necessary, for example, to be quite certain that the aerial coil was an efficient, high-Q type, representative of the best modern practice. The point behind this is that the merit of the aerial coil determines the input voltage to the first grid—signal, interference, atmospheric noise, and circuit noise—in.

If the aerial coil is poor, then the loss input to the first grid will be low and the noise content of the following circuits more significant as a result.

Increase the aerial coil gain by five times and the noise probability in the rest of the set diminishes by the same factor. Such a margin might be decisive in determining whether or not a given type of RF stage is worth while.

Then the RF coil comes into the picture because, in association with the valve, it determines the RF stage gain. If the RF stage gain is low, then the noise of the converter stage may be significant; if the RF stage gain is high, then the reverse will most likely be true.

How do our correspondent's observations line up with these remarks?

In the first place, he records some improvement in signal-to-noise ratio when substituting a cathode-coupled twin-triode for the conventional pentode RF amplifier.

One might accept this, but only with reservations. Pentodes are usually credited with being very efficient amplifiers at broadcast frequencies, their noise contribution being completely swamped by external noise fed to them via an efficient aerial and coupling coil.

However, this is the point which T.S. is querying, rightly or wrongly.

Really speaking, the strangest thing about our correspondent's report is that changing the converter valve made an even greater difference than changing the RF amplifier. This doesn't add up at all.

According to the "Radiotron Designer's Handbook", a single pentode

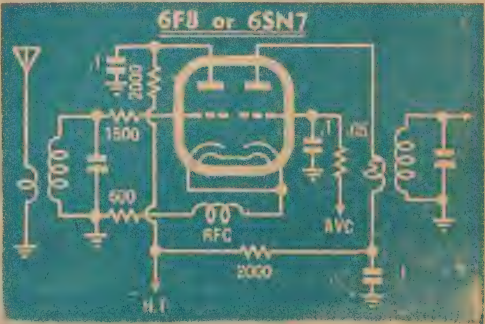


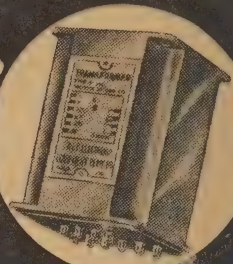
Figure 2: A cathode-coupled twin-triode which our correspondent suggests would give equivalent gain with much lower noise, if substituted for a conventional pentode RF amplifier. He suggests that such a stage could even be used to advantage in the role of first IF amplifier in the above circuit.

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Prim.: 8000 ohms P.P.
Sec.: 500, 250, 166, 125 and 100 ohms.

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Prim.: 6600 ohms P.P.
Sec.: 500, 250, 166, 125, 100 and 83 ohms.

TYPE 892 - 55 watts.
Prim.: 3200 ohms P.P.
Sec.: 500, 250, 166, 125, 83, 62 and 50 ohms.

SINGLE ENDED

+ - 2 db 50-12000 cps.
TYPE 928 - 5 watts.
Prim.: 7000, 5000 ohms.
Sec.: 12.5, 8, 3.7 and 2 ohms.

TYPE 929 - 10 watts.
Prim.: 4000, 2500 ohms.
Sec.: 15, 12.5, 8, 3.7 and 2 ohms.

TYPE 930 - 10 watts.
Prim.: 4000, 2500 ohms.
Sec.: 500, 250 and 125 ohms.

HIGH FIDELITY

+ - 1 db 30-15,000 cps

OUTPUT TYPE
TYPE 763 - 15 watts.
Prim.: 5000, 3000 ohms P.P.
Sec.: 15, 12.5, 8, 3.7 and 2 ohms.

TYPE 920 - 15 watts.
Prim.: 5000, 3000 ohms P.P.
Sec.: 500, 250, 166, 125 and 100 ohms.

TYPE 897 - 15 watts.
Prim.: 10000, 8000 ohms P.P.
Sec.: 500, 250, 166, 125 and 100 ohms.

TYPE 896 - 15 watts.
Prim.: 10000, 8000 ohms P.P.
Sec.: 15, 12.5, 8, 3.7 and 2 ohms.

SPECIAL HI-FIDELITY

+ - 1 db 20-40,000 cps

OUTPUT TYPE
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Prim.: 10000 ohms P.P.
Sec.: 2 or 8 ohms.
(for "Rola" 120X)

TYPE 871 - 12 watts.
Prim.: 10000 ohms P.P.
Sec.: 2 or 8 ohms.

TYPE 872 - 12 watts.
Prim.: 10000 ohms P.P.
Sec.: 3.7 or 15 ohms.

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TYPE 931-15: 20 watts.
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Valve: EL37, KT66, 6L6, etc.
19% Screen Taps.

TYPE 931-8: 20 watts.
Prim.: As 931-15.
Sec.: 2 or 8 ohms.
Resp.: As 931-15.
Valves: As 931-15.
19% Screen Taps.

TYPE 921-15: 20 watts.
Prim.: 6600 ohms P.P.
Sec.: 3.7 or 15 ohms.
Resp.: 10-60000 cps.
Valves: 807, KT66, etc.
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TYPE 921-8: 20 watts.
Prim.: As for 921-15.
Sec.: 2 or 8 ohms.
Resp.: As 921-15.
Valves: As for 921-15.
19% Screen Taps.

TYPE 916-15: 12 watts.
Prim.: 8500 ohms P.P.
Sec.: 3.7 or 15 ohms.
Resp.: 10-50000 cps.
Valves: 6BW6, 6V6, KT61, etc.
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TYPE 916-8: 12 watts.
Prim.: As 916-15.
Sec.: 2 or 8 ohms.
Resp.: As 916-15.
Valves: As 916-15.
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different class because they are frequently called upon to work over long distances with comparatively short aerials. In an electrically "distant" car, it is just possible that all-triode front end would show up advantage.

An interesting thought! In all this, of course, we have been talking only about the broadcast band. On higher signal frequencies the position gradually alters so that, for television sets, the latter is never in doubt. Triode RF stages win all the way; hands down, fact.

WHAT DO YOU THINK

But what do you readers think about all this? You folk who have listened all the time to distant stations?

Do you think an RF stage is necessary or do the people next door just as well with a comparable aerial and a modern set without an RF stage?

Have you ever tried one of these "low-noise" front ends?

We'd like to know!

There is, of course, more to do than mere signal-to-noise ratio. T.S. can ethically take the triode grids to AVC and expect no trouble. It probably wouldn't matter, in his location, if there were no control at all applied to the front end!

The position would be very different in areas where one or more powerful locals had to be dealt with. The conventional triodes mightn't take so kindly to excessive control voltages, and we'd be stuck with all the troubles of distortion and cross-modulation that preceded the release of super-control pentodes.

Such a prospect would be enough to daunt any designer. An expensive tuner which wouldn't work close to powerful stations would be a bad proposition indeed.

The same correspondent raises another question relevant to distant radio reception.

Despite the selectivity of his tuner, he says that his night-time reception is marred by "monkey chatter", caused by the modulation components from an adjacent channel riding through with the signal to which he is trying to listen.

DEBAND PROBLEM

He is quite sure that the trouble is due to this effect, because tuning upward the interfering station gradually turns the monkey chatter into recognisable musical overtones and speech syllables.

T.S. wants to know why these "stray" sidebands do not beat with the carrier to which the set is tuned rather than the carrier to which they elong. This latter carrier is largely unappressed because it falls outside the pass band of the receiver.

Here I quote from the original letter:

"Put it this way. I tune in a station and say 1000 Kc. Now a station on 1010 Kc is modulated by a 7 Kc note. This gives frequencies of 1017 and 1003 Kc. This latter is only 3 Kc off resonance with the 1000 Kc station and have tuned in and should beat with it to produce a 3 Kc note. But no, it produces 7 Kc in the output!

Why don't I just get distortion instead of a scratching noise sounding or all the world like a speaker fault

IN SUPPORT OF DUAL FEEDBACK

Dear Sir,

At the risk of protracting this correspondence unnecessarily I should like to refer further to the matter of dual feedback loops as used in W.P.'s circuit (June issue) and in my own circuit which you did me the honor of publishing in the May issue.

The explanation for the poor results obtained by W.P. from the use of dual feedback loops would of course require detailed analysis and measurements of every relevant section of his amplifier, and without this I can only agree that the output transformer used by him may not have been as good as expected.

However, as some form of vindication of my own circuit, I determined on reading W.P.'s letter to run off a set of performance figures for comparison and



for my own peace of mind! These are not as full as W.P.'s, but I think they serve the purpose.

At the time of taking the measurements given below, a first-rate English (Partridge) transformer was in use in my amplifier. Like W.P., my own laboratory gear is limited but I happen to know a fellow who... &c. and I was able to get the use of the gear at one of our technical institutions for an afternoon.

In the course of making these tests and before the final figures were taken the balance of the feedback was altered slightly by

increasing the plate-cathode feedback resistor to .2 Meg—this gave a slight improvement on square-wave.

Measurements were made into 18 ohm resistive load at 10.89 watts:—

Frequency Response

Flat to 50 Kc		
60 Kc	plus	1.2 db
70 Kc	plus	1.5 db
80 Kc	plus	1.5 db
90 Kc	minus	.9 db
100 Kc	minus	3.4 db
Total Distortion		
50 c/s		0.22%
400 c/s		0.19%
10 Kc		0.33%

I am also including a rough trace of a 10 Kc square-wave response taken on a Grainger type GRC 5A oscilloscope.

These figures are reasonable I feel. However, with the plate-cathode feedback disconnected and about 20 db feedback in the main loop there was chaos!

There was no static instability but the frequency response started to rise at about 60 Kc and kept on rising to 100 Kc, beyond which it was not possible to measure at the time. The square-wave was anything but square at the output, looking rather more like a ragged picket fence!

Reducing the feedback to 14.5 db brought the amplifier back to sanity but gave distortion figures about double those for the dual-feedback condition, viz.

50 c/s	0.43%
400 c/s	0.48%
10 Kc	0.69%

This much at least is in accord with the results found by W.P. Whether any conclusions at all can be drawn from these sets of largely contradictory findings I'll leave to you and the world at large.

Yours faithfully,
C.H.

—until the offending station is properly tuned in?"

Alas, T.S., I am afraid you have become the victim of your own eloquence. Have you ever observed the offending station when radiating a 7 Kc tone and noted that it remained 7 Kc when tuned to an adjacent carrier? The chances are that you haven't and are merely assuming that such would be the case.

In point of fact, the detector in your receiver is not at all fussy and will demodulate and produce results from each and every frequency component present, irrespective of where the said components come from. This includes "stray" sidebands from the interfering station along with (possibly) a faint trace of its carrier.

The main output from the detector (fortunately) is the product of carrier and sidebands of the desired station—in other words the wanted program. However, there will be a resultant also from the stray sidebands, beating not only with the carrier of the desired station but with each of its numerous sidebands.

In the process (and contrary to T.S.' suggestion) some frequency inversion does take place. The higher the modulating frequency on the interfering carrier, the closer will its sidebands approach the desired carrier. Thus a rising cadence in the adjacent signal becomes just the reverse when it appears as interference on the wanted signal.

This basic principle is actually used in telephone channels to invert or "scramble" speech signals, thereby rendering them normally unintelligible.

RANDOM PRODUCTS

In the case of interference, however, the result is far more complicated than simple inversion. Mixed in with it are all the random products of the two sets of modulation. No wonder that it earns the title of "monkey chatter".

The only recognisable thing about the chatter is that it has the rhythm of the interfering signal and it therefore isn't hard to pick a dance band from a talk on fruit flies, even though the exact details may be a trifle obscure.

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station gradually restores the
al to its correct proportions, till
program can be enjoyed or
ured in the normal fashion.
o get away from RF problems
reproduce, on the preceding page,
tter from C.H. who, you may
ember, was involved in the re-
discussion about amplifiers with
feedback loops,
somewhat worried by the con-
y findings of another reader, he
nged a detailed test on his
lifier, with the results set out in
letter.

is hardly necessary for me to
ment at length, because the
r is more or less self-explan-
y. As he says, the results are
asonable". More than that, I'd
they're very good and probably
inside the limitations set by
r items in the reproducing chain.

W DISTORTION

t lower power levels, the distor-
figures would probably be very
ll indeed.

hile this might set C.H.'s mind
est in regard to his own amplifier,
n't help but feel that his dis-
sal of the single-loop condition
been very summary.

rom his statement that the re-
se is starting to rise at 60 Kc and
ill heading upward at 100 Kc, it
quite evident that the feedback
not properly compensated.

er such conditions, it is quite
uitable that a square wave should
reproduced like a "ragged picket
ce".

hese days, one shouldn't even
t to test such an amplifier until
response had been levelled off so
t it did not rise anywhere appreci-
y above reference. I find it hard
believe that such a condition could
be achieved with what is
cribed as "a first-rate" trans-
ner.

educing the feedback would
aturally temper such effects but
uld not eliminate them nor put
amplifier in a fair condition to
unless the phasing capacitor
oss the feedback resistor (or else-
ere in the circuit) were adjusted
eliminate peaks and obviate ring-

ME RESERVATIONS

on these grounds, we might accept
l's verdict on his original hook-
but not on the single-loop version
which there was "chaos" or some-
ing a little short of it.

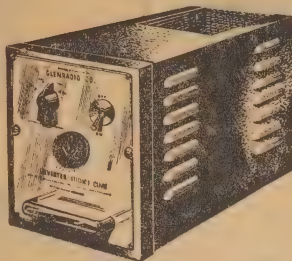
ut even as I write these words,
ind myself wondering how long
will be before someone gets
und to measuring or assessing
practical significance of all these
h frequency peaks and ringing
ects. We've already suggested
t, with the best pickups and
akers, an amplifier sounds vague-
cleaner without these effects but
ere does imagination end and
lity begin?

ow closely do transient wave-
ms on a good orchestral record-
approach the rise time and
plitude of our "square" wave?
ere important, how much of the
ershoot and ringing in the ampli-
survives propagation through
oudspeaker and a pair of ears to
duce a significant stimulus?

Until we know the answer to these
estions, we are in danger of
oming slaves to a CRO pattern.

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6F8	6SC7	6C8-G	6AG5	3Q5-GT
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49	76	81	84/6Z4	47
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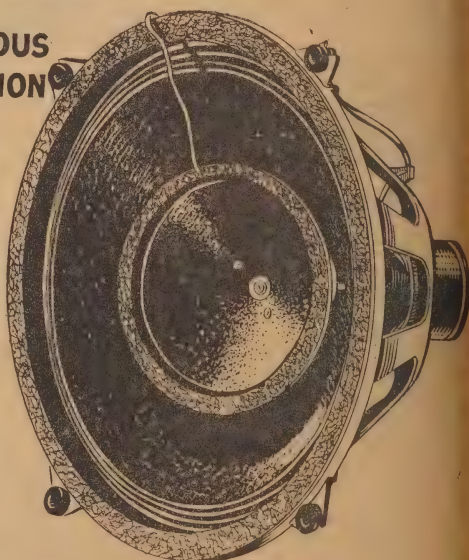
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AN 8-VALVE RADIOGRAM

From Page 71

he usual practice, therefore, is to make this part of the set "on trust" the moment and attack the aerial, and oscillator stages. Trimmers would have been mounted across a section of the gang and these adjusted at the high frequency end of the band. The coils will be adjusted with adjustable iron cores and are adjusted at the low frequency end.

Make sure that the dial pointer is to coincide with the "set dial" mark at the low frequency end of dial when the gang is closed. If dial has no set mark, set it just on (about 1/4 in with the type glass used) the 550 Kc mark.

Now tune in a station on about 1000 Kc and note its position relative to the dial calibration marking. If necessary, adjust the core of the oscillator coil until the calibration is correct. Follow this up with adjustment of the aerial and RF coils for maximum signal strength.

Now tune in a station at the high frequency end, between 1200 and 1500 Kc. Use the oscillator trimmer bringing this into line with the dial markings. Follow up with aerial and RF trimmer adjustment to give maximum signal strength.

TEST

Check again at the low frequency end and correct any slight error that may be apparent, then again at the high frequency end. Intermediate stations should now line up with the dial calibrations. If they don't, it is probable that the dial is not correctly calibrated relative to the gang and you may have to repeat the procedure with a slightly different setting.

Weak but steady stations are best for sensitivity adjustments, though a strong local is often more convenient for dial calibration, if only because they are more easily identified. Keep the volume out from the speaker low, as the speaker is more sensitive to changes at low volume.

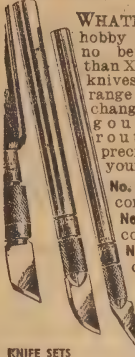
When this section is completed to your satisfaction you may tackle the speaker channel. Once again choose a weak signal, tune it in carefully and keep it at low volume. Give each adjustment a half turn or so, noting the final position before disturbing it. When an improvement is noted, keep adjusting until the loudest signals are obtained. Repeat with each adjustment until all are peaked.

If a multimeter is available it may be set to the 10 mA range and connected in the 6N8 cathode circuit to serve as a sensitivity meter. Increasing the sensitivity will decrease the meter reading, due the AVC action, and is much more accurate than judging level by ear. It will not operate on the secondary adjustment of the second IF, the AVC being taken from the primary winding.

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OFF THE RECORD — NEWS & REVIEWS

It is often very difficult to select a "recording of the month". It is doubly difficult for a middle-brow release to head off so many good discs of weightier music. In giving the palm to the "Land of Smiles", I do so because of its easy and universal appeal, for its high quality of musical worth, and for an almost faultless performance by all who made it.

LEHAR—Land of Smiles, Romantic Operetta featuring Elisabeth Schwarzkopf, Erich Kunz, Nicolai Gedda, and Emmy Loose, with the Philharmonic Orchestra conducted by Otto Ackermann. Columbia 33-OCX-1114-5.

To record a romantic operetta such as this, so full of sentimental traps which could fall into bathos, without the support of an actual performance, is not easy, particularly one which is linked so closely with the incomparable voice of Tauber.

To do it as successfully as Columbia has done on these two discs, is something of an achievement. Very rarely do we hear four complete sides of this type without blemish, technical or musical. "Land of Smiles" deserves high praise because it does so completely what it set out to do.

WELL KNOWN SONGS

Nearly everyone knows some of the songs from the score. "You Are My Heart's Delight" is sung by almost every popular tenor of the day. But there are plenty of other numbers just as good if not so well known, and they are doubly delightful when they appear in their full sequence.

All the songs and dialogue are in German, but the story isn't hard to follow. If you have a few German phrases at your command you will have no difficulty in picking out many of them, for the diction is crystal clear.

Elisabeth Schwarzkopf has been heard in other operettas of this type.

by John Moyle

I doubt whether she has an equal at the present time. And once we have overcome our surprise that anyone else but Tauber could sing the tenor songs, we realise that Nicolai Gedda might fit his role even more appropriately—certainly he sounds more the youthful, eager lover than the late Tauber.

The recording is first class. Every voice is clear, quite free from any sign of strain or distortion. The orchestra gives a star performance in itself, perfectly balanced against the singers, always adequate and warm in support, but never obtrusive. The amount of reverberation is just right. It avoids a strictly studio atmosphere, but allows every detail of the superb scoring to be heard.

And finally the surface is as good as Columbia have ever produced. What a difference a noiseless background can make!

My five-star award is shared equally by performers and recording engineers. If you don't like these records you are either very old or you have no music in you.

SCHUBERT—Symphony No. 6 in C major. Played by the Bamberg Symphony Orchestra, conducted by Joseph Keilberth. Radiola-Telefunken NLB6082.

This is an early symphony of Schubert's, often called the "Little"

symphony. It certainly is well named in comparison with No. 9, written in the same key of C major and known as the "Great".

It is a pleasant and bright work but has nothing very much to hold it together. Schubert, who relies so much on material rather than method in his orchestral work, doesn't unfold the same grand melody which shines through his better known symphonies, and in this respect the average listener might be disappointed.

Joseph Keilberth plays it with sense of "hurry", which certainly brightens its already bright mood but also tends to make something of a scramble here and there. The orchestra is a bit behind him on or twice.

TREATMENT SUCCESSFUL

At the same time this treatment is more successful than any attempt to invest a stature the music does not possess, although if anything Keilberth has overshot the mark.

I missed the roundness weight one associates with a good orchestral disc of today, but it may have been part of the plan to build lightness into the music.

I haven't any other recordings for comparison, and I doubt whether there are many, so that if you would like one of the sixth, this seems to be it.

The surface, as with most Radiola discs of today, is smooth and lent. It is good enough to take an AES curve, which gives a welcome lift to the top, and one note of bass boost, which adds body to it.

HANDEL—Double Concerto in F major (No. 28). Played by the Berlin Chamber Orchestra, conducted by Hans von Benda. Radiola-Telefunken NLB6079.

No one could easily resist a cord of this calibre.

The music has much in common with the "Water Music", and "Royal Fireworks", which have been recorded many times.

It is a 10-inch disc, despite eight movements—quite a long work for those times. In it we hear Handel at his brightest and best.

It's date is not known, but it is almost certainly one of Handel's last compositions.

The recording is not exactly mote, although the amplitude is high. It has more-than-average reverberation which gives it a concert-hall atmosphere, fully in keeping with the full scoring and consistent body of sound.

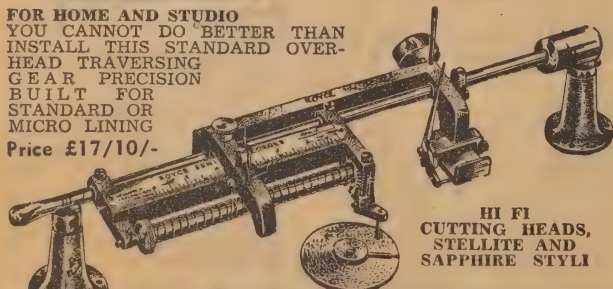
Occasionally this does concern some of the parts, but on the whole I would say the music is the better for it. The free use of ho-

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wood-wind gives a richness to texture and the "grand manner" beautifully preserved.

The performance itself is first class. The "grand manner" has no trace of pomposity—it is always firm and human. The horn players deserve special mention. They are bravely laden, but play their part without a break in tempo or technique.

Technically the disc is good. Everything has turned out well, and it plays cleanly and consistently from start to finish. There is no surface noise that I could hear—except on the run-off at the end is subdued.

This is one of the month's best discs. Despite the pile which awaits me, I played it through twice, just for the pleasure it gave me.

RAVEL—Pavane pour une infante défunte, A la maniere de Chabrier, A la maniere de Borodine, Sonatine, Mirois. Played by Robert Casadesus, pianist, Philips ABL3012.

This is the first of a set of records in which Casadesus will present the complete piano works of Debussy, on the whole a very good idea. It is inevitable that with so much on a single disc there should be an uneven quality in performance, and with music of this type not everyone's reactions are the same.

In general, I thought Casadesus tends to exploit the dynamics of the piano with the loss of some sensitivity. But his playing is crystal clear, and there are many occasions on which this is an overriding virtue.



ROBERT CASADESUS

In the Pavane, for instance, I thought his desire to avoid pale colors gave him a rather matter-of-fact approach which could have been softened with advantage.

In the Alborada del gracioso, on the other hand, this treatment is very much more successful.

His right hand is particularly vivid in Une barque sur l'Océan, but the effect would have been even better with more effective support from his left. "La vallee des oches" is good, although the Sonatine, an early work which won a competition organised by a music

magazine, I thought the best of them all.

In this, Casadesus shows that he does not look at Ravel as a kind of earthy Debussy, as do so many pianists.

Neither the Chabrier nor the Borodin interludes made any impression on me—either the music misses the mark or Casadesus doesn't know what to do with it. Ravel is probably to blame.

The piano recording is if anything a bit remote, but is mostly convincing, and at times extraordinarily good. The surface is almost noiseless.

In brief, a good record. It would be necessary to pick over individual recordings of these pieces to better them, and that would mean many records instead of one. Plays best on an EMI curve with extra bass—the NAB would be ideal.

RIMSKY-KORSAKOV—Scheherazade Symphonic Suite Opus 35. Played by the Minneapolis Symphony Orchestra conducted by Antal Dorati. Mercury MG50009.

Regarded purely as a recording, this is in the highest class.

Mercury's single microphone technique produces a distinctive brilliance, unmatched in its way by any other studio.

"Scheherazade" is an ideal vehicle for it. Not only is it a show piece with few equals, but it provides a succession of vivid passages for almost every instrument.

Whereas the extremely forward recording might not suit everything, it is an outstanding success here. Something in the creation of solid color may be lost in sections such as the Young Prince and the Young Princess, which would have flowed a little more romantically from a greater distance.

On the other hand there is an opportunity to show off some fine string tone, and the wood-wind does not make the mistake of trying to compete with it.

WIDE RANGE

The dynamic range of the disc, as with all these Mercurys, is a vast thing, and makes such passages as the final storm quite tremendous in their force.

No opportunity is lost to show up the quality of the orchestra, which comes through the ordeal without a falter. Dorati handles it with an almost razor-like control, and its flexibility and response will delight you.

The wide dynamic range means that often the music is playing well down into the noise level, and I would have liked to hear a smoother surface. The tendency—and indeed the advice—to "turn up the wick" means that the surface must stand extra scrutiny, and wide range equipment will show that it is not completely quiet. Elsewhere, of course, the volume swamps it out.

The frequency range is wide, but the temptation to overdo the bass has been admirably withstood. At lower volumes, a notch of extra bass will be in order, but I thought the balance in every way was admirable.

I can't imagine a recording of Scheherazade with more brilliance and impact than this one.

Although AES curve is recommended, I dropped it down to EMI.

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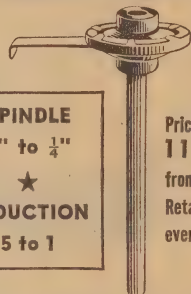
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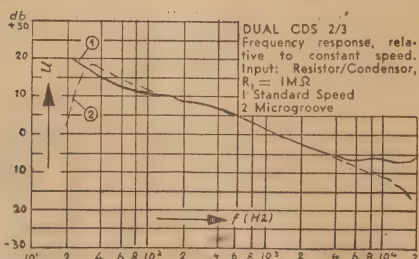
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RAVEL — Bolero: RIMSKY-KORSAKOV — Capriccio Espagnol. Played by the Detroit Symphony Orchestra conducted by Paul Paray. Mercury MG50020.

Both these can be regarded as display pieces, and therefore legitimate material to show off an orchestra.

But I thought that here the exhibition is made at the expense of the music.

Bolero, of course, is little more than calculated mental torture.

With the little boy who insists on hitting himself with a hammer many consider the best part is where it stops! On the other hand, plenty of people love every note.

In the Capriccio Espagnol I thought Mercury's single microphone had descended much too far into the orchestral bowels.

It did something to the string too, making their tone far from pleasant—or are they really there?

Plenty of it is very good, of course. Large sections are vivid, the extreme, and very, very forward.

But there is a good deal of music in this piece, and very little of it remains after the devilish Paul Paray has sprung upon it, and with his cohorts, torn it to shreds.

Then it becomes just rowdy. The surface on this side is almost silent, but there is some to be heard through the Bolero.

A record more to be prized for a brilliant noise than for a performance.

PUCINI — Operatic arias from Manon Lescaut, Madame Butterfly, La Bohème, Suor Angelica, Gianni Schicchi, and Turandot. Sung by Maria Meneghini - Callas. Columbia 330CX1204.

During the last five years, Maria Meneghini-Callas has become one of the most famous dramatic sopranos of the day.

She has done this by the amazing manner in which she has handled roles as different as those of Brunnhilde and Mimi.

Few singers of the past or present have managed to cover such a wide emotional range with success. But Callas has the artistry and the personality to make everything she sings sound convincing, sincere and alive. Everything she does is touched with authority.

Her dynamic range is quite exceptional. When she sings Mimi and Butterfly in a half-voice, beautifully produced and controlled, you will easily be deluded into thinking it to be her natural tone.

But, at an approaching climax her whole personality and vocal texture will change into a rich, thrilling crescendo of almost incredible power.

Frankly I found this somewhat disconcerting, despite its spectacular effect. One just can't imagine Mimi about to die of consumption, singing like that, or Butterfly either. Moreover, any woman with such a robust psychology would be out of character in either part.

As a performance, therefore, every one of these arias is a jewel. Considered as portions of opera, they are not completely consistent.

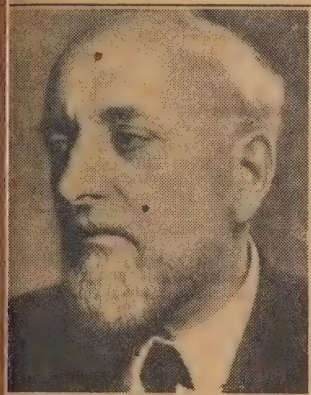
It is no wonder that such a voice should show a change in quality at

e extremities of its range. This true of Callas. Her full capacity, demonstrated in the excerpts from *Andant*, show distress, and elsewhere a peculiar husky tone creeps in which mars its sheen.

Nevertheless, this is a thrilling piece of recording by a magnificent singer.

The recording has few flaws. Rarely are there any dubious notes, though with such a voice there is plenty of opportunity. The orchestra isn't named, but it does well enough to deserve a mention.

Surface is first rate. EMI curve OK.



ERNEST ANSERMET

STRAVINSKY—The Fire Bird Suite, played by L'Orchestra de la Suisse Romande. The Symphony of Psalms, by the London Philharmonic Choir and Orchestra. Both conducted by Ernest Ansermet, Decca LXTA2916.

This record sounds like an early masterpiece of Ansermet and the Suisse Romande. It has all the definition and brilliance we greeted with delight in the early Decca's, but the touch of excitement seems less than might have been.

A more forward recording would probably have made a difference. Maybe that of recent years we have become used to more successful recording with the close microphone. True or false, I had the feeling that the colors were rather flat in this record.

There is, however, some exquisite playing. The Berceuse I thought particularly fine—first grade performance if ever I have heard it. There is plenty of top response, and the bass is improved with some boosting.

The Symphony of Psalms is a most unusual work, written in 1910 for the fiftieth anniversary of the Boston Symphony Orchestra. It is for orchestra and choir, the latter singing in Latin excerpts from the Book of Psalms.

The orchestra has no violins or cellos, being composed of woodwinds and brass, supported by string basses, tympani and two pianos.

It comes from Stravinsky's later period, in which he was deliberately striking out into new orchestral country, avoiding at all costs anything that sounded like conventional treatment.

For this reason, the symphony is an important work, particularly to

students and listeners who like to analyse just how it has all been done. It may well be the first LP release.

The recording, however, is only average. It is rather remote, and the voices suffer from some distortion on both loud and soft passages, which is characteristic of earlier LP's, even though the amplitude is not large.

I would rate the disc as interesting more for the music and the performance than for the recording. I'll leave you to judge.

SCHUBERT—Symphony No. 1 in D major, Symphony No. 2 in B flat major. Played by the Royal Philharmonic Orchestra conducted by Sir Thomas Beecham. Philips AO1138L.

These are Schubert's earliest symphonies, the First being written in 1813, and the Second in 1814, when Schubert was aged 16 and 17 years respectively.

We do not, therefore, find the Schubert of more mature years, although any young lad who produced such work today would be a sensation.

It is highly interesting, and somewhat amusing, to hear Schubert struggling to emerge from a pattern based on earlier composers with whom he undoubtedly became familiar during his student days.

We hear, too, many musical ideas which Schubert used in expanded form in his later works. There is a good deal of honest padding, but there is also tunefulness, vigor, and bright color which make both symphonies easy listening. Maybe there is good reason to talk of structural weaknesses in Schubert's orchestration, but it has never yet clouded the lovely music built upon it.

The composer's development between the two symphonies is quite marked. For that reason, the Second, I think, is the better work, and some of it as good as anything Schubert ever wrote.

Beecham proves an excellent conductor for these symphonies. The orchestra plays them with typical grace and charm. The recording, too, is bright and well-balanced, with a smooth, quiet surface. The EMI curve sounds best.

BACH — Brandenburg Concertos, No. 2 in F major and No. 5 in D major. Played by the Berlin Chamber Orchestra, conducted by Hans von Benda. Radiola-Telefunken LE6503.

This is a record of real quality. The Brandenburgs, six in all, are familiar to almost every lover of music, and certainly to those with a knowledge of Bach.

They are so called because they were written for the Elector of Brandenburg to whom they were dedicated in 1721.

In the No. 2, the concertino is made up of a trumpet, flute, oboe and violin playing with a *repieno* of harpsichord and strings. In the No. 3, the concertino is a violin, flute and harpsichord.

The Berlin Orchestra gives a bright, clear performance with a refreshing air of authenticity.

Particularly good is the unnamed harpsichord player, whose solo work in the No. 2 is worth special mention.

He may have been given a separate microphone, for as he proceeds with his part in the first movement of No. 2, for instance, someone has either swung a microphone into position or turned up its gain control.

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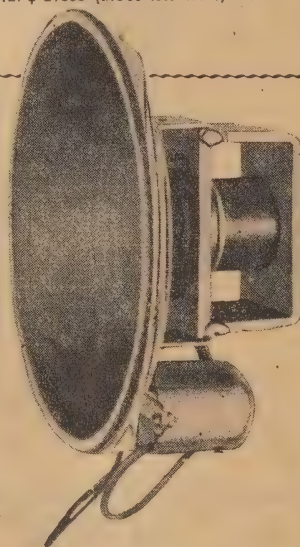
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At any rate, it is as full-toned as an instrument as I have heard of quite a time. Too many harp chords in music of this type a thin and unimpressive. But here we have the real thing, and unless you have heard such a one before you will be surprised how much weight can be struck from it.

The No. 5 is perhaps the most popular of them all, and I need say no more than that its performance is as good as I have ever heard on a record.

Technically, both sides sound round and full in tone, well balanced, and with good instrument definition quite essential in such work. There is no background surface noise—something which is becoming a habit with Radiola.

Thoroughly recommended for Broadcasters. The EMI curve is best.

BEETHOVEN—Symphony No. 9 in D minor, Opus 125, played by The Hague Philharmonic Orchestra with the Amsterdam Toonkunstchoir and soloists, conducted by Willem van Otterloo, Symphony No. 8 in F major, Opus 93, played by the Berlin Philharmonic Orchestra, conducted by Paul van Kempen. Philips A00221L-A00222L.

This is the same recording as was used by Philips for a release some time ago, and which I reviewed when it first appeared here.

The difference is that an entirely new set of masters have been cut from the original tape.

The first cutting was a straightforward LP job, with regularly spaced grooves. It also split the second movement, simply because a single side wouldn't hold two of them.

But this one has been made with the latest techniques, including the use of micro-grading, and with stylus which cuts an infinitely quieter groove. And all the movements are in one piece!

GREATER RANGE

As a result, the dynamic range is much greater than that of the earlier version.

At the same time, unless I am mistaken, the bass has been boosted to give an added resonance, which has deepened the general pitch.

It is clearly to be heard in the drum beats of the second movement.

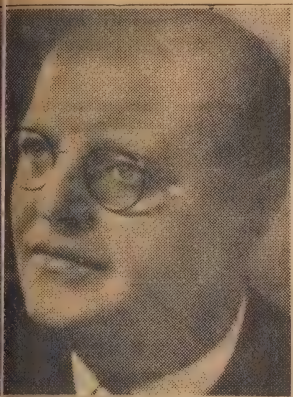
In this new recording they sound rounder and fuller than in the original. If there is a loss in authenticity, however, it is quite minor against the richer sound this reinforcement has given.

I always liked this Ninth, and in some ways it has the most successful vocal movement of them all. The recording is more remote than in some others, but largely avoids distortion and other queer effects which appear to lie in wait for engineers when they try to record choirs. The soloists, too, are very good.

What it may lack in the spectacular, therefore, it gains by being more playable than any of the others. And that's the thing that matters.

At the same time, this last movement is a devilish thing to record and I still live in hopes of hearing some day a miracle performance in which sopranos neither shriek nor

ral fortissimos disappear into a
idy mess.
he fourth side is taken up with
extremely good performance of
Eighth symphony, again a some-
it remote recording with a little
e-than-usual echo which isn't in
way objectionable, nor does it
the general orchestral definition.
is played with great vigor and
re—a most impressive perform-
e.
particularly attractive jackets in
or set off this very fine set of
s.



JOSEF KRIPS

SCHUMANN—Symphony No.
in D minor, Opus 120. Men-
delssohn—Symphony No. 4 in A
major (Italian). Played by the
London Symphony Orchestra,
conducted by Josef Krips.
Decca LXTA2887.

is only recently that I reviewed
Schumann symphony as played
the Philharmonia Orchestra, con-
ducted by Cantelli.

his Krips version is not as
ent. It seemed to me that, aware
the weaknesses of the work, and
tendency to lose one's interest in
my passages, Cantelli tried to
pe it more tightly than usual,
I thought he did succeed in giv-
life even when there was preci-
little to be discerned.

Krips on the other hand endeavors
build more stature into the music,
does probably as well as it is
sible to do.

but I fear his impressive build-
at the commencement of the last
vement, for instance, only serves
accentuate the anti-climax which
us as the movement proper
aks forth in all its banality.

ter may be significant that I thought
of the work after listening to
ntelli, but no differently after
ps.

his recording is quite as impres-
sive as Cantelli's, however. The
chestra sounds clearer and more
ward, although it has no greater
ght.

The Mendelssohn on the other
nd is not only bright and interest-
ing, but is played that way. Its
mediate plunge into action against
background of staccato horns
er fails to shine for me.

It was written during a tour of
y, but appears to have little other
ociation with that country. Its
odies and orchestration are un-
tably Mendelssohn as we hear

him in the Hebrides and the Scotch
symphony, although no doubt he
attempted to strike a light and grace-
ful line. Some can see allusions to
Italian scenes in the music, but they
do not greatly convince me.

I thought it easily the better side,
and it is on the whole a very satisfy-
ing performance.

The surface noise is a little higher
than usual, although by no means
bad. It played a bit edgily on the
Decca curve, so I suggest you try
the EMI which I found the best.

PROKOFIEFF—Symphony No.
7, Opus 131. Played by the
Philadelphia Orchestra conducted
by Eugene Ormandy. Philips
AO1614R.

One of the month's most interest-
ing and beautiful records. I have
never heard the symphony before,
which isn't surprising as its first per-
formance was given in 1952 in Mos-
cow, the year in which it was com-
posed, and a few months before Pro-
kofieff's death.

It was first performed in America
by this orchestra and conductor in
1953. There is nothing outlandish
about it, either in musical ideas or
in treatment. It is illuminated by
a fresh imagination, clear musical
thought, and almost classical orches-
tration. It has a distilled atmosphere
—the product of concise construc-
tion and clearly connected musical
thought.

Of it, and its traditional four
movements, the Russian paper Pravda
wrote—"The first movement ranges
from a children's fairy tale through
romantic dreams to the first active
aspirations of youth. The second
is a symphonic waltz; the third is
a brief but deeply lyrical and ex-
pressive movement. The fourth
combines the moods of a gay dance
and an energetic march, spiced with
humor and droll wit which appears
so often in Prokofieff's music."

You may not extract all this at
first hearing, but there isn't a bar
which is unintelligible.

FINE PLAYING

Apart from the music you will
undoubtedly be impressed by the
magnificent playing of the Philadel-
phia Orchestra.

Magnificent I think is just the
right word. Right from the start
there is smoothness and power, and
complete appreciation of the music.
As usual the strings are particularly
fine. They have a sheen, precision
and vitality really good to hear.

The tone is firm and full, the
balance sure, and every part plays
clearly and well. Add to this a
silent surface and you have a par-
ticularly fine record.

Not a big work, but no assess-
ment of Prokofieff is complete with-
out it.

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—A collection of songs of ardent
affection, wails and plaints, as
well as joyful songs and dances
sung and performed on recorders
and suitable stringed instru-
ments by the Trapp Family
Singers. Columbia 33 OSX7529.

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built around themselves a world of
folk music, both vocal and instru-
mental. Not only do they give re-
citals in various centres, but operate

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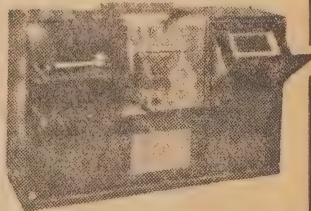
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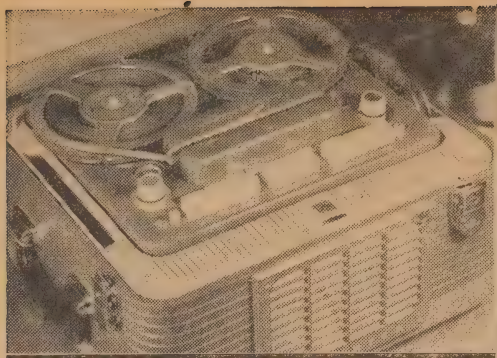
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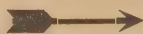
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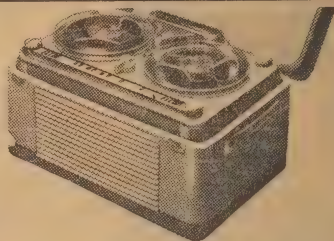
Apology

Magnetic Sound Industries wish to apologise for any inconvenience caused to their clients by their advertisement last month announcing that the new GRUNDIG Tape Recorders would be here. We understand now from the manufacturer that, owing to the shipping strikes in England, the machines will not be arriving till late September or thereabouts. The price will be announced in a later advertisement.

In the same advertisement, when announcing the release of the brand-new, twin-speed, twin-track ELCON, the price was mistakenly quoted. The correct prices for the two models are now: ONLY £140 for the 7-valve deluxe Radiocorder and ONLY £119 for the standard Elcon Tape Recorder.



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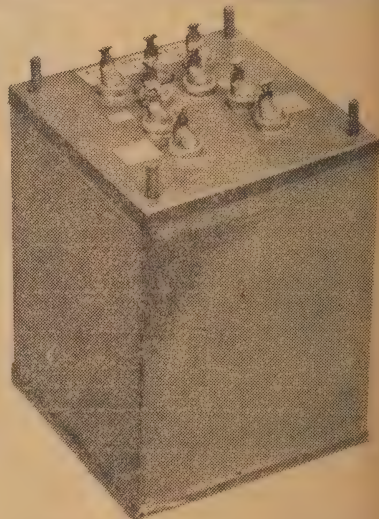
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BRAMCO RADIO COMPONENTS

83 NELSON STREET, WALLSEND, N.S.W. Phone LL9211.

music camp devoted to the revival family music. On this disc they sing a number folk songs from Austria, Germany, England, and even include a Texas cowboy song.

interspersed are items played on order flutes with string bass accompaniment (or so it sounds), all with a dedicated air and considerable charm.

lost arrangements are by Dr. Franz Wanner, a musician and priest who accompanies the family.

Mostly its members sing as a choir. Though in several songs there is every pleasant baritone soloist. All arrangements are good, and mostly they are beautifully sung. Of the instrumental work the Trio recorders alone I thought the

recording is most effectively done, and the surface a good one. The Trapp Family is bound to attract a large audience here in Austria, and this disc should be a popular memento of a unique musical combination.

MOZART—Concertos for violin and orchestra in G major, K216, and A major, K219, played by Jean Fourier and the Vienna State Opera Orchestra, conducted by Milan Horvath. Westminster WL-5187.

This disc has the authentic West-ster sound about it—clean, crystal-clear outlines, a forward, full-range viola tone, and a frequency range which puts up a brilliant wing on wide-range gear.

In fact, it is very hard to fault. Both concertos are early works. The conductor and violinist have clearly been satisfied to let the music speak for itself, which it does most gently. The tempo is steady, the playing relaxed, and the sound constantly good.

Everything about Mozart is so precious that it is little more than usual to say that these concertos were written when he was barely years of age. Of the two, the A major is probably the best known, though there are few recordings in circulation. Fournier's playing of the exquisite third movement perhaps the best thing on the disc. The violin tone seems to be better this side than in the G major, and the recording seems a little better at times.

One would also have liked a somewhat brighter tempo, particularly in the final movement.

The Vienna State Orchestra plays the Vienna Konzerthaus and is provided with its usual fine balance. Horvath conducts it in perfect sympathy with the soloist and maintains the balance between them at first rate.

I found the NAB curve best—it needed an otherwise sharp edge to the violin and gave an admirable boost to the orchestra.

The surface is extremely good

BRUCH—Concerto No. 1 in G minor Opus 26. (MENDELSSOHN) Concerto in E minor Opus 64. Played by Campoli (violin) and the London Philharmonic Orchestra conducted by Eduard van Beinum. Decca KTA-2904.

In all, it is very hard to resist the claims of this as being the best recording of both concertos.

I cannot say whether it is the same version of the Mendelssohn as was issued some years ago, on a 10-inch disc. There is little reason to discount it if it is.

Campoli isn't the most brilliant of violinists, nor the most powerful. But he has a sincerity, charm, and musicianship which are just right for these works.

Even the Bruch concerto is invested with this sincerity, enough to discount over-purple sentiment.

As most people who like the one will also like the other, this disc looks a winner musically and financially.

NIXA DANCE DISCS

Nixa continue to make a name for themselves through a series of excellent dance releases with authentic music covering the popular sambas, rumbas, mambas, &c., which are the key to youthful entertainment today.

Some of them include the more conventional foxtrot, which seems to have taken over all the rest.

In the four records mentioned below a high standard is maintained. Not only is the playing good, but the rhythm dances have an air of the real thing.

Compared with them, some routine 78's of the same music are characterless and tame.

On LPY121 Pepe Nunez and his Orchestra Typique play four tangos on one side and four paso-dobles on the other.

On LPY123 Ben and his Tropical Rhythm Kings play eight typical dances (baiao, guaracha, mambo, samba-lente, samba and bolero)—a very good disc.

On LPY122, M. Philippe-Gerard and his Ensemble are more conventional in eight dances modernes.

All these discs sound most impressive on good equipment and technically they are first rate.

On SLPY143, Red Camp plays on his concert grand a number of popular numbers including Summertime, Tenderly, Laura, and What Is This Thing Called Love. This is a Cook original, but I found Red Camp very free with his material, and somewhat hard of tone in his piano. He has a big reputation overseas.

Vital and authentic Flamenco music is played by Carles Montoya in a Fiesta Flamenco. This is another Cook record, and it is more a faithful account of musical and dancing sounds than a Flamenco recital. It may be sounds of our times, but not as purely musical as some other Nixa Flamenco records.

ALBUMS

Record albums seem to be on their way out.

Instead, it is becoming standard practice to house each set of two or more records in a combination box-folder. The discs retain their individual envelopes, and the whole thing sits on a shelf more conveniently than an album.

The back of the box bears the name and identification of the recording it contains.

This method of packing will be adopted for all EMI releases in the future. Where appropriate, descriptive leaflets or booklets will go with the records.

The Land of Smiles, reviewed in this issue, is treated in this way.



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SHORT-WAVE NOTES BY ART CUSHEN

NEW STATIONS FROM VIETNAM

Several new transmitters have been heard operating from both North and South Vietnam, while stations in the States of Laos and Cambodia have also been heard.

STATIONS in the communist area of North Vietnam have been broadcasting from Hanoi. The most consistent signal is that of "The Voice of Vietnam" which is also the slogan of the Government broadcaster over the border in Saigon, both stations therefore claiming the same slogan.

The Hanoi transmitter which appears to have been taken over from the evacuating French Forces some months ago has been operating with lower power on both 11995 and 9555 Kc. It has also commenced broadcasts on 7320 Kcs varying to 7420 Kcs, and on this frequency provides much better signal strength.

The transmitters all carry a programme of English news and commentaries, followed by music, from 10.30 to 11.00 pm daily.

Not much information has been gathered about stations in North Vietnam and we are hopeful that a verification will soon be received and this information passed on to our readers.

SOUTH VIETNAM

The recent change of time zones in this country has reverted to three hours behind AEST, instead of the former two hours. "The Voice of the Vietnam National Army" broadcasting on 258 and 41 metres broadcasting from "Saigon" is the announcement given during the English news broadcasts from 10.15 to 10.30 pm daily.

This station was formerly in Hanoi and as the Voice of the French Army, known as Radio Hironelle. A move was made to Saigon, and transmission conducted on 7180 Kc, 8.30 am-2.00 am.

The Vietnam National Army station appears to have replaced the French Army station and is now using the new frequency of 7255 Kc, and is being well received at present.

CANADA ADDS CKNK

THE Canadian Broadcasting Corporation at Montreal has added a new frequency to the International Service. It now operates CKNK on 11945 Kc along with CKLP on 9585 Kc.

Both these transmitters carry the North-West Territory transmission in English 12.55-1.35 pm daily. The transmission consists of messages to people in the Far North who are isolated for much of the year and are dependant on the CBC broadcasts to keep them in touch with the outside world.

The transmission to Australia and New Zealand is broadcast 10.55-11.15 am on CKCX (15190), CKLO (9630) and 6.45-7.20 pm on CKLO (9630) and CKNA (5970).

BELGIUM CEASES FOREIGN BROADCASTS

THE Belgium National Radio Station ORU at Brussels, has ceased to carry any foreign languages for its Overseas Services. These are now broadcast only in the native tongue of French and Flemish, and are still broadcast on the former schedule of these languages.

The announcement of this cut in overseas broadcasts from ORU due to restricted budget came as a blow to the many friends of the station overseas.

The DX session, and the very popular "Amongst Friends" were programs much in favor with listeners.

The Belgium National Broadcasting Service first came into prominence during the war years when the station commenced to broadcast from its temporary home at Leopoldville, Belgium Congo, the temporary home of many of the Belgium activities which were evacuated before the German invasion. It was also the home on the opposite bank of the Congo River of the Free French transmitters at Brazzaville.

The headquarters of OTC, "The Goodwill Station", remained at Leopoldville, and the world-wide popularity poll of the ISWC, London, in 1950, found OTC the most popular station.

During this period the Belgium National Broadcasting Service were building a

News from readers and enquiries should be sent to Arthur Cushen 212 Earn Street, Invercargill, NZ. All times are Eastern Australian.

new 100,000 watt transmitter at Wavre. In 1951 the programs were broadcast from the Belgium station ORU, the Leopoldville transmitter acting as a relay station. Its situation was ideal for broadcasts to North and South America.

In 1953 the ISWC Poll found that the new ORU had slipped to fourth place, the main reason being the station's poorer coverage for European listeners, due to the change in proximity to the Continent.

So far we have had no news of the use to which the Wavre transmitters are to be put during the hours in which they were normally employed broadcasting in foreign languages.

The fate of OTC Leopoldville has already been noted. This station has joined the barrage of transmitters of the Western Nations in the three daily broadcasts in the Russian language. It is a far cry from the former Goodwill broadcasts to its new role.

FLASHES FROM EVERYWHERE

CANADA'S salute to the 25th anniversary of the International Show W. Club, London, will be broadcast on Monday, September 5, 6.45-7.15 pm on CK (9630) and CKNA (5970).

The transmission on Sunday on the frequencies has a very interesting Let-Box program, and during the answer of listeners' mail, mention is made of a monthly program booklet which is obtainable by listeners simply by writing to Radio Canada at PO Box 60 Montreal Canada.

LISBON's transmission to the South African area is now relayed on the frequencies, 11996, 15125 and 17835 3.30 to 3.30 am.

PEKING'S English broadcasts at 11 pm are now on 1130, 11690, 11960, 15015, 15130, while at 7.00 pm the 9555, 111690, 15060, 15105 are used. Peking third transmission in English broadcast 12.30-1.00 am is carried on 9025, 9611300, 11690 and 15060 Kc.

BAGHDAD'S 85 metre transmissions, 3297 Kc carry Arabic on all transmissions 2.00-4.00 pm, 1.50 pm-6.00 am and ISV reports that they are verifying with new card.

VOICE OF AMERICA relays in Korea are relayed by Korean Broadcasting System stations Pusan (7935), Pusan (251), Taegu (4775) between midnight to 12 am and 8.30-9.00 am. The Mandarin programs are carried by the Taipei Taiwan station BED7 (7130) 1.00-1.30 am a BED4 (11920) from 7.00 am to 8.30 am.

FORCES BROADCASTING SERVICE at Benghazi, Libya, has been heard good strength both in Australia and New Zealand, and George Hughes of Adelaide states best reception with him is on Sunday morning when sign off is 8.00 am. The station closes other days at 7.00 am with a goodnight Light Out on a bugle then the National Anthem. The frequency of 4940 Kc is used, and though this is very close to the Brisbane transmitter, on 4920 Kc, the interference not very severe. The station uses on 250 watts, and was verified some months ago when the transmitter was located in Tripoli.

JAPAN'S short wave commercial transmitters operated by the Nippon Short Wave Broadcasting Company, Tokio, have ended the test broadcasts on JOZ3 9595 Kc which we mentioned last issue. The broadcasts on JOZ3 were well received at Marrickville, NSW, by Edwa Williams, who reports good signals at pm.

The transmitter has not been received over the past few days, and one report has it that an announcement heard recently mentioned that tests on 9595 had been concluded in the meantime JOZ (3925) and JOZ2 (6055) are still being heard with English news at 7 pm.

DELHI'S transmission to South-East Asia with English news at 10.30 pm 10200 and 9525 Kc, these new channels replace 11875 9700 Kc.

CANADA'S CFRR broadcasting from Toronto on 6070 Kc has a fair signal 8 pm when a broadcast of news is presented. This 1000 watt transmitter is relaying the broadcast band transmitter 1010 Kc using the call sign CFRR.

The station which is now on Eastern Daylight Time, also has been heard closing at 3.00 pm. The station is operated by the Rogers Broadcasting Company and verifies with a bright card which shows a map of Canada imposed over the skyscraper skyline of Toronto.

NEW FREQUENCIES FOR ALL-INDIA RADIO

ALL INDIA RADIO, is using new frequencies, and the English News broadcasts are as follows—

12.30-12.45pm	Delhi 4990, 5955, 7285, 9720, 11920; 15400.	Bombay: 6150.
	Calcutta, 4880, 6010, Madras 6085, 4920, Mysore 4800.	
6.00-6.10pm	Delhi, 7920, 9620, 11705, 15290, 17760.	Bombay 9550. Calcutta; 7210. Madras, 6085.
10.30-10.35pm	Delhi 6190, 9720, 10200, 15330.	Bombay 9550. Calcutta, 7210. Madras, 4920, 6085.
1.30-1.45am	Delhi 4990, 5990, 7210, 9510, 9720, 11925.	Bombay 6150 Calcutta, 4880, 6010. Madras 4920, 6085, Mysore, 4800.

from World Radio Handbook.

RAMBLES WITH BILL MOORE

tional Field Days are always well supported overseas, but for some reason they have never attracted much attention in this country. This is strange in a country where open air life is so much part of our everyday life.

ATIONAL FIELD DAYS are very popular events in the US, and last year some 8000 radio amateurs were in field.

Some interesting rules are incorporated in the event, run annually by the ARRL, to ensure that the varying power inputs by competitors are allowed for in the compiling of scores. The scope of the test is wide enough to allow all stations interested to compete.

Stations are divided into five classifications:

1. Club or non-club group portable stations (three or more operators).

2. Station or individual portable stations (one or two operators).

3. Mobile stations.

4. Home stations operating from emergency power supplies.

5. Home stations operating from commercial power sources.

Stations using portable equipment must put their gear within a 1000ft radius. All amateur bands may be used but the ratio of more than one transmitter per one time in the same band is not used. Transmitters on different bands may be operated simultaneously. Cross band contacts are not permitted. The test period is for 24 hours.

Scoring is one point for each contact with varying multipliers. They are as follows:—Multiplier of three for power outputs of under 30 watts, two for power outputs between 30 and 100 watts, one for outputs between 100 watts and 1 Kw.

Further multipliers are three for all stations using equipment independent of mains, one for stations using commercial power and an additional multiplier of two for stations using battery power. These multipliers do not apply to home stations. The operation of home stations using emergency power supplies provides an excellent exercise for amateurs in areas likely to be affected by emergencies, in that the event is a simulated emergency situation.

These US events are dedicated to emergency communications preparedness, and every opportunity is given stations to compete.

TV INTERFERENCE

THE initial meeting of the combined VHF and HF, BCI and TVI committees of the NSW Division was held on August 2 under the chairmanship of Dr. J. Black, VK2QZ, the division's BCI and TVI officer.

It is the desire of the combined committee that every possible avenue is explored to ensure that early action is taken on possible TVI. The meeting was an important venture in amateur radio activity and their work will be followed with interest by all amateurs.

Dr. Black, VK2QZ, acted as secretary to the committee.

The meeting discussed and planned early on many aspects of BCI and TVI. It was decided to work first on BCI and then to establish a procedure for approaching the authorities for the forwarding of problems of TVI. It is hoped that early solutions will arise from this experience.

It was decided to set up an organisation to train at least 40 amateurs on the correct recognition of types of TVI. These amateurs should form the nucleus of any committees set up in all areas for TVI work.

They also hope to work in close liaison with the PMG's Department and form of an Australian-wide organisation for BCI and TVI. Meetings will be held monthly and it is planned that the scheme will be operative before the end of TV in this country.

CONTEST ON 144 MC

THE 144 Mc mid-winter contest of the NSW UHF section run in July was well supported with 30 stations operating on the first evening.

VHF contests are conventional from the point of passing numbers only, and personal exchanges are infinitely more interesting.

Stations farthest afield were VK2JX, Wentworth Falls, and VK2RU, Gosford. During peak operating periods the band was extremely congested. 39 different stations were active during the two four-hour operating periods.

The winner of the event was Ted Howard, VK2XX, with 54 contacts. In second place Peter Adams, VK2JX, with 40 contacts. VK2HE, and VK2ADY, Mobile Station of the Gladesville Radio Club tied with 53 contacts. A further tie was recorded for third place between Perc Healy, VK2APQ and John Thornthwaite, VK2ATO.

VHF LECTURES

THREE lectures were presented at the August meeting of the NSW VHF section. Dr. Bob Black, VK2QZ, lectured on VHF equipment, Barry Goodman, VK2ZAG covered specialised components for VHF amateurs, and Bob Winch, VK2OA Class C Modulators.

Some extremely interesting lectures have been arranged for future VHF meetings.

Neville Williams, VK2XV will repeat his lecture on "Outline of Television" previously presented to the NSW section of the IRE.

Dr. Bill Davies of the CSIRO will lecture on Transistors, and Max Sobels, VK2OT, will continue his discourses on Television.

VHF IN THE WEST

WALLY HOWSE, VK6ZAA, contributed the following notes on VHF activity in the West.

The July meeting of the VHF group was held at the residence of Don Graham, VK6HK. A motion was passed expressing concern at the proposed changes to the 50-54 and 144-146 Mc/s bands. Despite the advantages of the harmonically related 56-60 Mc/s band, it was felt that as the change is not universal, it will preclude any further investigation of DX propagation and the effect of the increased solar activity.

While the cross-band contacts overseas would theoretically be possible the operation of TV transmitters on Channel 1 in Australia and channels overseas in the 56 Mc region would eliminate any chance of a repeat of the DX contacts VK5GL to WTACS/KH6 and VK6HK to VK2CG.

The group was disappointed that the 50 Mc band will be lost and that use may be made of Channel 1. Sporadic-E-caused interference is likely to occur with any TV signals on this channel.

A check of only three VK6 logs showed that there was interstate reception for at least 29 days each summer every year since 1951. Every year since 1949 has seen VK6/ZL contact all with 100 watts, not 100 Kw.

Bello Everingham, VK6BO, gave a very informative lecture on the design and operation of valve testers and illustrated it with circuits of his own.

Again an offer is made to help any amateur in WA to get going to 144.

Members will only be too pleased to arrange a portable expedition to a country QTH. Contact should be made with Wally Howse, VK6ZAA, 53 Ellen St., Fremantle.

ALBURY CONVENTION

THE 1955 WIA South Western Zone's (NSW Division) Convention will be held at Albury over the long Six Hour Day weekend with a programme covering Saturday, October 1 and Sunday, October 2.

The venue, central to many amateurs in both NSW and Victoria, should assist in assuring a record attendance. Twenty-six amateurs attended a preliminary meeting held in July at Albury to make arrangements for the convention.

Fuller information will be available from zone members or direct from zone officer, Jim Edge, VK2AJO, of Coolamon, or from Don Haberecht, VK2RS, of Albury. Programmes will be distributed to interested amateurs.

The arrangements include a tour of the Hume Weir on the Saturday afternoon, a dinner in the evening with films, pick-a-box, scrambled tunes, and other competitions.

Field events will be featured on the Sunday.

They include transmitter hunts on the 144 and 3.5 Mc bands and an additional blindfolded search on 144 Mc. A one-hour scramble will also be conducted. Latest details will be presented over the Sunday morning VK2WI broadcasts. Albury should see an influx of amateurs in early October to attend the SW convention and enjoy the fraternity of these events.

ANTARCTIC LECTURE

LECTURER at the July meeting of the NSW Division of the WIA was rare DX, Bill Storer, VK2EG, ex VK1EG, recently returned from Antarctica. Bill displayed interesting color films of the Mawson Base, Antarctica, and the surrounding area.

The films taken by members of the expedition were later edited for general display. Bill also showed a number of color slides. He regretted he was unable to spend as much time as he would have liked on the amateur bands.

Bill was still able, however, to supply some hundreds of stations with a new country. The films and the explanations provided were well received in a capacity house, 120 members attended.

Short wave listeners interested in the formation and supporting of SWL section in the NSW Division of the WIA should contact the secretary Harry Hicken, VK2ACH, Box 1734, GPO, Sydney. A number of persons have suggested the formation of the group but the real necessity is to obtain SWL's keen enough to conduct the section.

SILENT KEY

IT is with deep regret the passing is recorded in late July of Reg Anthony, VK2TR, who was an active amateur since the early 30's.

Originally signing VK2HR he lost that call to the B/C station. His next call was VK2AEC and later VK2TR.

Active mainly on the 14 Mc band where DX was the attraction and relaxation, Reg was for a period a councillor of the NSW Division of the WIA.

He assisted the division on many occasions with gifts of equipment for conventions and similar events. VK2TR was perhaps best known for his work with the Lakemba Radio Club and Experimental Radio Society of NSW.

The sympathy of all amateurs is extended to his wife and family.

Radio, Television & Hobbies, September, 1955

REPORTING CODES

TLE has been heard of the RSM ode, a system for reporting Telev signals, since it was voted upon the National Societies comprising the national Amateur Radio Union.

was originally sponsored by Euro-societies and favored by the major- IARU members. The ARRL did use the system and this factor will oubtedly affect its universal adop-

M section of the code from M1 5 was only a partial answer to a report on quality.

LIST OF 50-54 BAND

LOWING approaches by the Federal xecutive of the WIA the PMG's rtment announced that the 56-60 Mc ould become available from mber 1 and that operation to cease e 50-54 Mc band on January 31. The gement allows an uninterrupted d for the Ross A. Hull Memorial ay to be run during December and ary.

QSL ADDRESSES

3 following are the changes in ad- dresses in QSL Bureaux since the shing of the list in the March issue. w addresses are as follows:—British na: Desmond E. Yong, VP3YG, PO 325, Georgetown, Dominica; VP2DA, 64, Roseau, Dominica; Windward ds, Nicaragua; YNIRA, Apartado Managua, Uganda; PO Box 1803, pala.

TVI FIGURES

L RAND, WIDBM's survey of TVI n the New England section of the throws some light on the extent of caused by amateur stations.

e figures are based on a 50 pc return questionnaire. The question of in- rrence experienced is as follows: pc of the stations replying caused TVI, 32 pc had slight TVI, 7 pc medium TVI and 2 pc had bad

result of the poll indicated how ern TVI reduction techniques are eg dividends.

DX CONDITIONS

NOTICEABLE improvement was re- corded in the 14 and 21 Mcs condi- tion during July, better than those rience here in June and a vast rrence to those of the winter of 1954.

appears that our sun-spot worries over and the DX fraternity can e down to serious business.

cellent openings occurred both in mornings and afternoons on 14 Mcs all continents appearing at times. ra, Europe and South America in AM, and all continents except South rica in the PM.

st DX heard was CR4AL and FF8AG TU was making the most of the itions and keeping check on the l for his "Month on the Air" fea- appearing in the RSGB Bulletin. ing propagation conditions on 14 next summer should prove ex- ely interesting.

ome extremely strong signals* from West Coast of the US were still ing S8 to S9 hours after the peak. ZL's signal was a case in point, result it would appear from mucu and many elements, he could not VK replies to his CQ's.

October will be a busy month. First t is the VK/ZL DX contest, fol- ed by the international DX contest the weekends, October 22 and 23 October 29 and 30.

ve, Y1DL reports that 14 Mc is the useful band at Port Vila. He is he lookout for VK's, especially those whom he worked in Sydney. Gener- active in the late afternoons on 14 Mc, Dave would appreciate call- s home-made QSL cards have been ived by many stations—his wife pro- ges them.

he journey of P. J. Mullock (G3HPM)

of the Cambridge University Wireless Society, to Gough Island will be of considerable interest to the DX fraternity. The Gough Island Scientific Research Expedition left England recently and has been licensed to operate an amateur station under the call sign ZD9AR. G3HPM will be active from there on all bands from 1.8 to 21 Mcs.

Gough Island is 260 miles south-east of Tristan da Cunha in the South Atlantic.

In the June issue mention was made of Terry Tatham, who is confined to an iron lung at Cherrywood, Pacific Highway, Turramurra. Terry now runs a

receiver, has books on amateur radio, and obtains much pleasure from his delving into amateur affairs, especially on the 40-metre band.

The Marconi School of Wireless has arranged a special course to assist Terry in his quest for further knowledge in the radio field.

Dr. Adrian Rofe, VK2HE, a regular visitor, reports that Terry has a new interest with his ability to listen on 40.

Amateurs who could possibly visit Terry at the hospital would be very welcome. It will allow him to see in person the amateurs he listens to for hours on end.

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29/6

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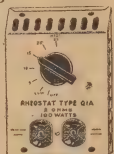
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39/6

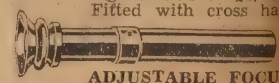
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AC-DC 45
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Eng. 0-500 Micro Ammeter, M/coil 37
Eng. 0-20 amps, 2 1/2 in dial, M/c 25
Eng. 0-15 Milliamps, 2 1/2 in dial, M/c 19
Eng. 0-200 Ammeter, M/coil 27
Eng. 0-20-20 Ammeter, M/coil 37
Eng. 0-30 Amps AC-DC 2 1/2 in dial 42
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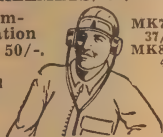
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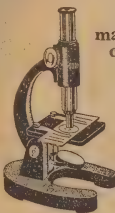


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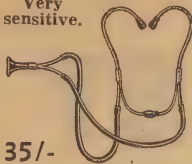
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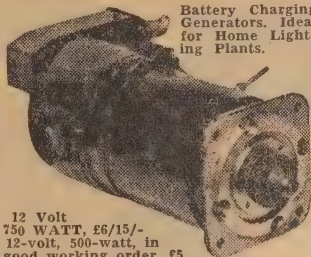
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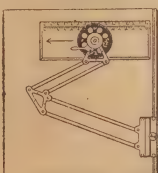
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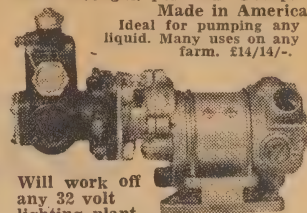
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watt projector globes, 32/6. 1 1/2in
Black and Decker 230 volt electric
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PV12A-55

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FROM THE SERVICEMAN WHO TELLS

(Continued from Page 63)

had been soldered to the chassis. In addition one of the lugs was acting as an earth point for the V7; the central shield, the cathode, the filament all being returned this point through a common earth. This was all very well—except that both the negative lugs were giving only intermittent connection to the chassis, both being classic examples of a dry joint. As a result the second filter capacitor was earthed through the six-filament winding, thus injecting volts AC into the HT line. In addition, the 6AN7 was rendered inoperative by reason of its open bottom circuit. Little wonder that all it would have been hum. Some emery cloth, a little paste flux, and a really hot soldering iron soon rectified this state of affairs and the set was as good as new. The owner was particularly pleased to learn that a definite fault had been discovered and that I could give him assurance that the trouble would not occur again. Apparently it had been getting him down.

WELD AS NEW

These two dry joints raise a rather interesting point regarding commercial wiring practice. The use of steel chassis and the soldering of appropriate connections directly to them is standard commercial practice—and there can be no quarrel with it provided it is done properly.

However, that qualifying statement "provided it is done properly" is important because there are a number of reasons why such joints frequently are not "done properly."

The majority of soldered joints in a set involve only small masses of metal, in most cases already finished. As a result a lightweight iron with a minimum of low activity flux will do all that is required to make a reliable joint.

By contrast a chassis joint is a deal more difficult. The very much larger mass of the chassis presents a problem, since the ordinary 100 or 75 watt iron is really inadequate for the job. It is not always fully appreciated, even by experienced solderers, that the purpose of the iron is to raise the temperature of the job to the point where it (the job) will melt the solder.

Unless this requirement is fulfilled, the solder will not flow into the pores of the metal and a reliable joint is impossible. To achieve this a larger than normal iron is necessary and should be used for all such joints.

In addition, steel is notoriously harder to solder than copper or brass, plus the fact that it is not presented to the operator already cleaned. On the contrary, it is usually covered with a coat of lacquer, which is certainly no help.

First job; therefore, is to clean the metal with some abrasive to remove the lacquer and natural

oxides. Then, because steel is harder to solder, it needs a more active flux than the resin used in cored solder. The activated resins which are becoming more popular are better, but by no means ideal.

The paste type fluxes appear to be the best proposition, and the fact that they are more corrosive than may be desirable for fine wires is of little consequence where a chassis joint is involved.

All this adds up to the need for a somewhat specialised approach to the making of chassis joints in factory production. The operator who is to make these joints must be supplied with a heavy duty iron, means of cleaning the job, and a suitable flux; as well he should have some skill over and above those who have never joined anything larger than a resistor pigtail and a solder lug.

Most factories do, in fact, approach the problem in this way, but it is not surprising if, on odd occasions, all these special requirements prove too much for the operator and one or two dry joints slip through.

Of course, it shouldn't happen or, if it does, it should be picked up in the inspection department. But operators, and inspectors, are only human, so that an occasional faulty joint gets into the field. It is just as well that it is only occasionally because, when it does, it can cause plenty of trouble.

Thrust spoiler

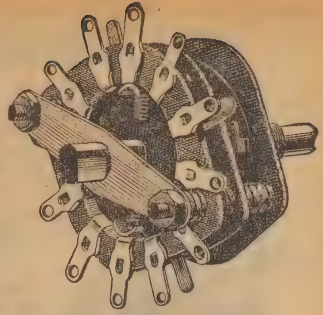
A NEW device produced by the General Electric Co.'s jet engine department, and known as the "thrust spoiler" is expected to provide greater control of jet planes during landing and thus increase the safety factor.

The device is quite simple to install and service and functions by deflecting the gases before they reach the exhaust nozzle. It is thus possible to keep the motor running at full power in case of emergency and to apply this full power without delay should it be needed. This is much safer than having to wait for an idling motor to come up to full power.

X-RAY SHOWS ENGINE IN MOTION
(Continued from Page 13)

beam, the crystal emits visible light. If the flat faces of the crystal are perpendicular to the x-ray beam a visible replica of the x-ray image may be observed along the beam axis. When the pattern amplifier is used in conjunction with a high-intensity, high-energy x-ray source such as the NBS 180 Mev synchrotron, it can continuously display images of parts hidden by as much as 18in of steel or 7½ft of concrete.

The visual image may be detected in several ways. It may be observed directly by eye, photographed with an ordinary camera, or observed with a remotely controlled television camera.



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(World Patents pending)

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CONTACTS—
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TEMP. RISE ON CONTACTS—
(with 10 Amp. Conductors)
at 10 Amperes 10° C. rise
at 20 " 30° C. rise
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DECKS—1 to 8 max.

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3 Pole—max. 4 "
4 Pole—max. 3 "

OVERALL DIAM. 2-1/16 in.

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- High output level — 50db.



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NOW 20/-

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£5/17/-

NEW VALVES CAN BE SUPPLIED AT £3/10/- EXTRA

Postage and packing on chassis extra. NSW 17/6, interstate 25/-.

NEW 5 VALVE D.W. BATTERY CHASSIS

This D.W. battery mantel chassis which is made by leading manufacturer is fitted with heavy duty Rola 6in speaker, tone control, etc., and gives excellent reception on local, interstate and overseas stations. Ideal for building into existing furniture, boats, caravans, etc. Valves used—two 1T4, one 1R5, one 1S5, one 3V4.

MIDGET GENEMOTOR

Input 28 to 32v at 1.1 amp. Output, 250v. at 60MA. New in carton.

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Used but in good order.

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Input filter supplied
with genemotors

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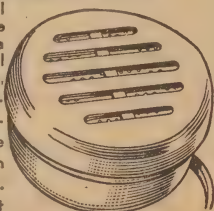
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New Creed relays complete with original cartons.

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Special price for quantities.

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Bakelite mounting base for above 4/6

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NEW 5in AND 6in PERMAG SPEAKERS BY LEADING MANUFACTURER

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Latest Model at almost $\frac{1}{2}$ price
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all microgroove and standard records —
In original cartons £14/17/6 F.O.R.

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Output 6V, output 230V, at 50 MA. These
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and hash. Supplied complete with standard
synchronous vibrator. £3/15/0 F.O.R.

ELECTROLYTIC CONDENSERS

2mfd 525 V ----- 3/9
100mfd 12 V ----- 2/-
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100mfd 350 V ----- 2/-
100mfd 40 V ----- 1/6
(Plus Postage)

2-inch P.M. SPEAKERS

Heavy duty 12in per-mag
speaker by well-known manu-
facturer. 10T, C.T. or 5,000
transformer. NOW 47/6
POSTAGE NSW 5/6, Interstate 7/6.

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These New Vernier Dials
are ideal for test equipment,
receivers, etc
(as used on AR8 sets)
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A.W.A. standard six pin syn-
chronous vibrators in original
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Plus postage.

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1T4	11/6	VR105	15/0
1S5	15/0	957	7/6
3V4	15/0	VR150	15/0
1R5	15/0	2050	15/0
6SA7	10/6	955	7/6
6SQ7	10/6	9001	7/6
6SN7	10/6	9004	7/6
6SL7	10/6	717A	7/6
6AG7	10/6	7C5	7/6
6AC7	10/6	7C5	7/6
6AG5	12/6	EF50	7/6
6J7G	10/6	12SR7	2/6
6K7G	7/6	1K5	2/6
6J6	15/0	VR6A5	2/6
EL33	12/6	12SQ7	2/6
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ALL PLUS POSTAGE

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in values of 100 ohms to 5 megohm. In
1-watt, $\frac{1}{2}$ -watt and 1/3-watt. All resis-
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values comprising 50 1-watt, 25 $\frac{1}{2}$ -watt
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Price 8/6
Post 1/6.

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New midget power trans. Upright
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Sec. 225 x 225 at 50 Mill. and 6.3V. at
3 AMP.

17/6

Plus postage 2/6 NSW 3/9 Interstate

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866	15/0	1616	£1/10/0
832	£2/0/0	828	£2/10/0
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I.R.C. RESISTORS

I.R.C. carbon resistors, $\frac{1}{2}$, 1 & 2 watt.
in values 50 ohm to 5 meg. including
many popular sizes, 3T, 15T, 20T, 25T,
50T, 100T, 250T, 500T, etc.
(Standard resistor color code supplied).

20/-

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6 volt A.W.A. gas-filled vib-
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NOW 7/6 or 70/- per doz

NEW 1T4 BATTERY VALVE

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Rothermel high fidelity pick-up
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Rothermel sapphire needles
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7in Dynamic speakers by lead-
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1,500 ohm Field coil,
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Ovaltone Dynamic Speaker
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Field, 5,000 or 7,000 ohm
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NOW 20/- EACH

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PHONE LM3610

NEW H.F. TRANSCEIVERS

RT 34-APS 13C (Tail-end-Charlie) Freq. 420 mcs. contain 16 valves 9-6AG5, 5-6J6, VR150 and 2.2D2. Also midget 24v Genemotor.

Less valves—£5/-/- **£10**

FULLAPHONES

Containing pair headphones, morse-key buzzer, key switches, etc.,

20/-

Post NSW 6/6 F.O.R. Interstate 8/6

NEW H.F. RECEIVER—R3118

(RESPONSE UNIT)

The ideal receiver for the 144 M.C. Band uses 13 6.3v valves, including two tuned R.F. stages. Supplied complete with valves, plugs and A.C. power supply. (240v.)

£9/17/6 F.O.R.

ENGLISH I.F.F. MOTOR

English I.F.F. motor complete with gearbox. 18v D.C. operation but suitable for conversion to A.C.

Were £2/10/-, Now 37/6

Postage extra — N.S.W. 5/- Inter., 8/6



75 ohm CO-AXIAL CABLE

75 ohm Coaxial Cable 1/9 per yd. Minimum quantity 10 yards on drums each containing 110 yards. £7/10/- F.O.R. Co-Ax. Plugs & Sockets (Pye Type) 3/- Pr. American type 4/- pr.

Heavy Duty Genemotor

Suitable for conversion to A.C. motor (approx. one sixth H.P.) Fully laminated. Can be used as 6 or 12 volt generator at 20 or 13 amps £2/17/6 f.o.r.



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A.T.5. Transmitter covering 140 K.C. to 20 M.C. in two separate tuned circuits. Provision for crystals. Complete with valves. Three 807 and two 6V6.

£4/17/6 F.O.R.

A.C. AMP METERS

A.C. Amp Meters (ex-Country Council). A necessity in any electrical workshop.

RANGE. 0.5 amps. (can be extended by shunts).

MOVEMENT. 300 degrees.

SCALE LENGTH. Nearly 15 inches.

DIAMETER. 7½ inches.

28/6



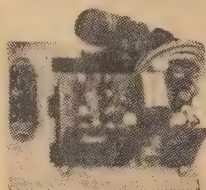
Postage extra — N.S.W., 6/6 — Interstate, 11/6.

NEW AMERICAN INDICATOR-UNIT

These indicator units contain the following valves:

Six 6SN7GT, one 6G6, one 6H6, one 6X5GT, one 2X2, and 3BP1 C.R.O. tube which is fitted in a separate shield on a 4ft shielded lead and supplied with control box and plug; case and shield are finished in black brocade. In original cartons.

TRANSFORMER TO CONVERT THIS UNIT FOR 240 VOLT OPERATION AVAILABLE AT £3/15/- EXTRA plus postage.



£8/15/- F.O.R.

A.M.R. 300

COMMUNICATION RECEIVER

This first class 10-valve receiver made by S.T.C. has a band spread coverage of 1.5 to 24 mcs in switched bands—240v AC operation—supplied complete with valves, crystal, S meter & speaker, air tested.

£47/10/-

F.O.R.

New 12 volt vibrator supply for above complete with leads, spare valve and vibrator 3-6 x 5 & 2 vibrators.

£5/15/-

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OIL FILLED CONDENSERS

(Working voltages stated)

20mfd. tapped	600v.	17/6
2mfd.	1,750v.	12/6
3mfd.	2,000v.	17/6
4mfd.	500v.	6/6
4mfd.	200v.	4/6
8mfd.	400v.	8/6
5mfd.	200v.	2/9
.25mfd.	750v.	2/9
.01mfd.	3,000v.	5/-

(all above plus postage)

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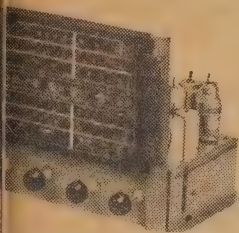
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NEW RADIOGRAM - CHASSIS KIT - SETS

5 VALVE
DUAL-WAVE



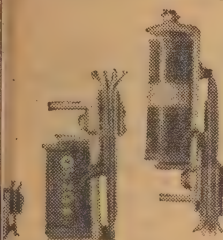
Complete kit of parts including 12in Magnavox or Jensen Speaker, five valves (1 6J8, 1 6K7, 1 6SQ7, 1 6V6 and 1 6X5) and all other parts to the last nut and bolt to complete the five valve dual wave chassis illustrated.

These chassis when completed give excellent overseas, local and interstate reception as the coils supplied and intermediate transformers are high gain Permature iron cored. Pick-up switch and volume control with A.C. switch supplied. Suitable for use with any crystal or high impedance magnetic pick-up.

LIST PRICE OF PARTS £25

SPECIAL PRICE £14/17/6 F.O.R.

WIRED - AND - TESTED £2/- EXTRA



AMERICAN RELAYS

1 Miniature relay 300 ohm
S.P.D.T. contacts, 10/-
2 Standard relay 250 x
0 ohm coil 4 pole S.T. 7/6
pole S.T. 6/6
3 Standard relay, 15,000
ohm coil, 2 pole D.T. 12/6
All relays suitable for
rewinding.

New dynamic mike inserts	8/6
Bakelight fuse boxes	4/6
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Shielded hook-up wire, per yd.	8
Morse keys	4/6
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3 gang standard condenser	18/6
3 gang midget condenser	18/6
2 gang standard condenser	15/-
2 gang midget condenser	15/-
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Fuse holders, bakelite, single hole mounting	2/6
Lifeboat transmitters	22/6
Teletron octal sockets, doz.	3/6
9-pin loctal sockets, doz.	5/-
6-pin wafer sockets, doz.	3/-
5-pin ceramic sockets, ea.	2/-
Acorn sockets, ceramic, ea.	3/6

RELAY-TYPE COUNTERS



("Mercury" American Made)
These relay counters register
from 0 to 99,999. Can be
supplied with 250ohm, 500ohm
or 5,000ohm coils.

29/6

plus postage

P.M.G. TYPE RELAY-COUNTER

0-9,999. 22/6
1,300 ohm coil

50-CYCLE A.C. AMMETERS

Range 0-5 Amps.
Scale Size 9in Dia.

Price, each.

37/6

Packing and postage: NSW, 7/6;
Interstate, 12/6.



AMERICAN ANTENNA SWITCHING MOTORS

Complete with 8 Pye-Type Co-ax Bases, R.P.M. 1750, Ball
bearing, 24 Volt.

D.C. GENERATORS

500 watt, Ideal Home lighting, Battery charging, etc.
Price £3/10/- F.O.R.

TRICKLE-CHARGER KITS

For trickle-charger as described in R. & H. June issue.
Comprising transformer with 18V winding tapped at 12V-3
mA rectifiers and 50 ohms control.
Price: NSW, 5/-;
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39/6

PEDAL-GENERATING SETS

These units in new condition will generate 12
volt at 5 amp. or 6 volt at 8 amp. Could be
motorised if required. Complete with generator,
reduction gear, stand, meter (3in) etc.

£8/17/6 F.O.R.

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Nylex hook-up wire 10,010 in 100 yard coils, each
coil consisting of five 20 yard lengths in 5 different
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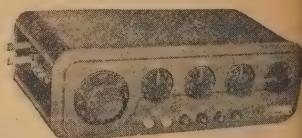
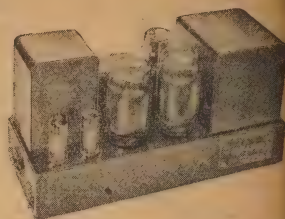
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Hi Fi NEWS from THE SOUND CENTRE

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	Armstrong A10	74 10 0
PICKUPS:	Ferranti	45 0 0
	Goldring 500	7 10 0
	B.J. Arm	5 19 6
	Acos	9 15 0
LOUDSPEAKERS:	Rola 12UX	21 0 3
	Goodmans Axiom	
	150 Mark II	22 16 10
	Barker	29 11 7
TEST RECORDS:	D.G.G. LP. Test	
	Records, ea.	2 4 6

LOUDSPEAKER ENCLOSURES:

Loudspeaker enclosures are available to suit Rola, Goodmans, Baker, Wharfedale, Barker and Leak loudspeakers, including the famous Wharfedale 3-speaker sand-filled corner enclosure. These cabinets are solidly constructed of $\frac{3}{4}$ " timber fully lined with suitable hair-felt and highly polished to match existing furniture. Vented enclosures are also available for Wharfedale and Goodmans 8" loudspeakers.



The distinguished Acoustical QUAD II Amplifier and Control Unit £108/3/0.

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HIGH FIDELITY SOUND CENTRE

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YOUR BRAIN CANNOT THINK!

It is merely the vehicle through which YOU direct every action of your life

Like an electric motor, it has to be activated by an outside energising force. Your thoughts are but the *inner* expression of your will directed through your brain to the *outer* achievement of your desires and your ambition for greater achievement in life. You can learn how to direct your thought energy towards a specific objective to produce positive results. Learn how to marshal your mental powers to improve your business and social career.

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ANSWERS TO CORRESPONDENTS

D. (Bowden, SA) sends us a further 2 months' subscription and common sense of the articles published past 12 months. The articles on music are among those found interesting. He also expresses the view that the coming electronic age will produce some startling developments. We send us a couple of stories for review as well as some very nice pictures on these articles.

Many thanks for your subscription. We and we are very glad to learn you find the magazine so interesting and informative. As you say it is likely we are on the threshold of some new electronic developments, many which have already been visualised and merely require the necessary reversal to bring them into practical use. However, if we may be permitted to have an open mind, we would point out that most competent authorities cast considerable doubt on the accuracy of the contents contained "Flying saucers landed". On the other hand the article itself can be quite convincing and difficult to say just where fact ceases and fiction takes over. Many thanks for your contributions to the Section and we will pass these on together with your kind comments.

E. (Lilvale, V.) wants to know if we can fit AVC to the SW Converter built in the July, 1955, Radio, Television & Hobbies.

It should be possible to extend the system of the main receiver to the stage of this converter without too much difficulty. The earthy end of the AVC would be disconnected from the chassis and connected to the AVC winding. The function would be by-passed by a .05 capacitor and common to ground. The existing AVC line through a decoupling resistor of about 500 ohms.

(Roseville Chase, NSW) wants to know if we have a wiring diagram for the Set For Young's OX'er's described in October, 1954, issue.

Sorry, D.S., but we do not produce wiring diagrams unless for publication. It involves a lot of work and there is no point in producing them unless intended for publication. This means, unfortunately, that we cannot help you in this matter. We have no data other than that which has already been published. We can only suggest that one of our pamphlets on circuit symbols might be of help to you to follow the actual circuit diagram which, once you have the hang of it, is really a lot easier than the wiring diagram. This is available through our query service 1/-.

H. (Meridin) is a keen reader of Radio, Television & Hobbies and has one of the smaller receivers which comes with a car aerial mounted inside. With this simple set-up he has received many interstate stations. He has built the Junior Multi-meter of December, 1954, with considerable success.

Many thanks for your letter, J.R.H. We are glad to learn that you have had so much success with your various projects. It is truly remarkable what can be done with some of the simpler types of receivers when they are handled correctly and they provide considerable interest and training.

M.deG. (Claremont, WA) has a problem with his hands in the form of a receiver as built for 32V operation. To obtain the required HT, he bought a 240V converter, and would like to know how to connect it up to the set. It has standard power supply.

We are afraid, M.deG., there is no way out of your problem. Your converter actually supplies 240V AC, and it would be necessary to provide the set with a normal AC power supply in order to make it work properly. However, in this set-up would be considerable and may place too much drain on the battery bank. It would have been

easier to wire the filaments in a series-parallel arrangement, making sure that all filaments receive their correct voltage and current, and connect them across 32 volts. DC HT could be supplied from a 32V vibrator supply. If this is too expensive to do now, the only thing to do would be to obtain a standard power transformer for 240V AC, and a suitable rectifier, and operate the set as a normal AC receiver.

N.R. (Georgetown, SA) would like to know if it is possible to use a two or three-gang tuning capacitor with a one-valve set. When he tried to connect one up in his set, it would only tune one station all over the dial.

A. Standard tuning capacitors usually have a capacitance of approximately 450 pf. when fully closed, and most coils are designed to give optimum performance and coverage with this amount of maximum capacity. A two, or three-gang, tuning capacitor actually consists of three of these standard capacitors mounted on a common shaft. If one is on hand, it would therefore be possible to use it with a one-valve set, simply by connecting only one section into the circuit, and ignoring the other two. We have a faint suspicion, however, that you connected all three sections together. This would mean that you have 1350 pf in circuit, which would completely upset the performance. A one-valve set would have only one tuned circuit, and therefore only one gang section is required. Multiple gang tuning capacitors are normally only used with receivers having several tuned circuits, such as TRF sets, or superhets.

B.A.P. (Bartleigh, Vic.) sends in a request for a list of S/W call signs, transmitter wavelengths and locations.

A. Unfortunately, B.A.P., our only list of S/W stations appeared in the Short-wave Handbook, which has been out of print for some time. We have never published the data in other form except the references in Art Cushen's series of articles on S/W reception. We suggest that you look up copies of back issues, and refer to the articles in them.

R.E.L. (Theodore, Qld.) is at present studying for his AOCP examination and would like to join the WIA. He asks how he can go about it.

A. Your best proposition would be, R.E.L., to write to the secretary of the Queensland division of the WIA, Box 6387, GPO, Brisbane, who will be able to give all the details about joining the institute.

G.R.W. (Glen Innes, NSW) would like to see more about Radio Control of models in our magazine. He also states that commercial models, which are expensive, very rarely give more than one-mile range.

A. For a long time we have intended to publish some articles on radio control, but there are still difficulties to be overcome, before we can go ahead with publication. As regards range of control equipment, it is very doubtful if a range of over one mile can be realised, as such transmitters are limited by law to an output power of only 2 watts.

J.D. (Hobart, Tas.) sends in a circuit for a battery powered shaver for electric shavers. To get over the difficulty in obtaining a 50 c/s vibrator, he used a synchronous unit, driving the shaver with DC.

A. The idea is certainly very neat, J.D. We do not know of anybody who has used high voltage DC supply for shavers, although it is expressly stated on most models that they do work on DC. We have filed your diagram for possible future use in our Reader Built It Column.

F.J. (Windsor, NSW) has amplifier trouble, and as he is not yet familiar with the finer points of the game, he would like us to give some suggestions on how to cure "motorboating".

A. To start with, may we point out that it is very unwise to operate a push-pull amplifier with one of the output valves removed. Doing this removes a major part of the load from the rectifier, the voltage rises and the other valves may be subjected to voltages far in excess of their rating. The output from the other output valve will also rise, masking the effect of reduced power output and distortion, particularly at lower levels. Secondly, what is motorboating actually? Nothing more than instability, or oscillation, at a very low frequency, caused by feedback from the output valve into the early stages

(Continued on Page 127)

The Radio, Television and Hobbies Query Service

All queries concerning our designs, to which a POSTAL REPLY is required must be accompanied by a postal note or stamps to the value of TWO SHILLINGS.

For the same fee, we will give advice by mail on radio matters, provided the information can be drawn from general knowledge. UNDER NO CIRCUMSTANCES, however, can we undertake to answer problems involving special research, modification to commercial equipment or the preparation of special circuits.

Whatever the subject matter, we must work on the principle that a letter is too involved if the reply takes more than 10 minutes of our time.

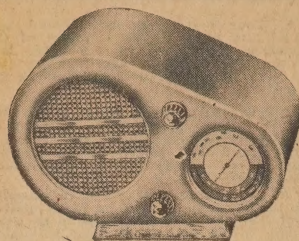
Queries not accompanied by the necessary fee will be answered FREE in the columns of the magazine and presented in such a way as to be of interest to other readers.

To those requiring only circuit reprints, &c., we will supply for TWO SHILLINGS diagrams and parts lists from our files covering up to three constructional projects. Scale blueprints showing the position of all holes and cut-outs in standard chassis can be supplied for 5/-. These are available for nearly all our designs but please note they do NOT show wiring details.

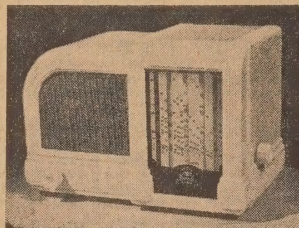
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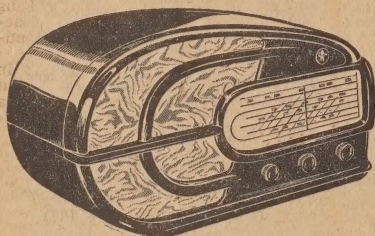


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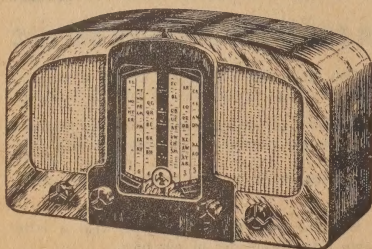
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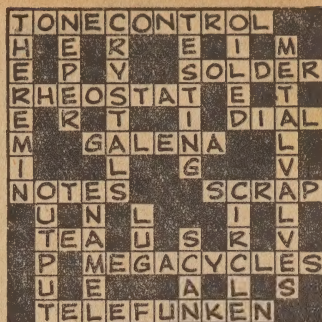
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Last Month's Solution



ACROSS

1. Reciprocal of reluctance.
8. Radio location.
9. Superintendent (slang abbrev.)
10. A tag or label.
11. Organ of hearing.
12. Positive electrode.
13. Allows interchange of certain valves.
14. To treat with heat.
16. Pertaining to nature.
17. Face.
18. — coil.
20. Solid water.
21. To depart from original.
23. Electro-magnetic switches.

DOWN

1. When a substance
3. Advantage on small receivers
4. Used for wiring.
5. Type of coil winding.
6. Triple.
7. In shunt connect.
15. Phonograph pioneer.
19. Type of current.
22. Soldering end of an iron.

Solution and further crossword next month

ANSWERS TO CORRESPONDENTS

the amplifier. Any small signal, even itching noise, causes a small variation in the voltage available from the plates. This variation is in turn converted to the plates of the other valves, where it is amplified and fed back to the output valves. To avoid this, the output valves are inserted into the HT line, bypassed by large capacitors. These capacitors charge up and tend to equalise the voltage applied to them by releasing some of their charge, if the voltage rises, or absorbing a higher voltage, if the signal is prevented from reaching the early stages. If the capacity of these capacitors, called "decoupling capacitors", is insufficient, some of the signal may reach these stages, causing instability. Now the two output valves have signals, one of which is in phase with the input to the amplifier, the other out of phase. Removing the output valve allows the out-of-phase signal to reach the first stage, thereby preventing instability. Removing the second valve allows the in-phase signal to be fed back and the amplifier "goes off". Instability, however, will take place, if the gain of the amplifier is high enough to produce a signal bigger than the original signal at the grid of the output valve. This explains why the value of one particular valve cuts out motorboating, and also why the other will not motorboat with the coil unit disconnected. The remedy would be to check the decoupling capacitors, if their capacity is high enough, to a combination of circumstances may be necessary to replace the valves with higher values, particularly in control unit. The use of D/W sets in Playmaster tuners was connected, but rejected, because no suitable bracket could be obtained. However, quite good results can be obtained from the front end of a D/W receiver.

if wide band B/C reception is considered unnecessary.

E.E.A. (Deception Bay, Q.) writes to tell us that he is making the electric guitar described in the August, 1948, issue of R and H and asks if we have details of the one described in the August, 1941, issue.

A. We regret that issue requested is no longer available, neither are any reprints available. However, it may be possible to obtain a copy through your local technical library or by advertising in our "Wanted To Buy" columns.

G.C. (Springvale, Vic.) writes to tell us that he has had very good results with the Porta-Player and would like to know if it would be possible to make it into a tape recorder by adding the No. 2 Tape Adaptor described in the July, 1953, issue.

A. We are pleased to hear that you are pleased with the Porta-Player but it is not sensitive enough to be used with the Tape Adaptor and will require an additional stage in front of it. As regards the most suitable oscillator coil to use, we suggest that you contact the manufacturer of the particular heads that you intend to use.

R.J.H. (Carlton, N.S. Vic.) would like to extend his range of instruments by adding a small 455 Kc oscillator. He inquires if we intend publishing such a circuit in the near future, preferably using transistors.

A. If the number of inquiries warrant it, R.J.H., we may publish such a circuit in some future issue. However, it is not likely to use transistors for some time yet, as these devices, at least the ones available locally, do not have the required RF characteristics. Also, if one goes to the trouble of providing several calibration frequencies, it may be as well to cover the whole range of frequencies encountered in the servicing of broadcast receivers.

READER BUILT IT

(Continued from Page 95)

The amount of expansion available is about 20db—more than is needed. The expansion is controlled by the 1 meg and .1 meg potentiometers. Advancing these together will increase the available expansion while maintaining the overall gain at about the same level.

With a little experiment these could probably be ganged, but I did not find it necessary to do so. The 50V bias for the .1 meg pot. can be obtained from a separate power supply if necessary or from a "B" battery.

In my case it was obtained by sacrificing 50V. from the existing pre-amplifier power supply by placing a suitable resistor in the secondary centre-tap.

A little experience is necessary in the best setting of the controls, but I think the results fully justify a few hours of preliminary experimenting.

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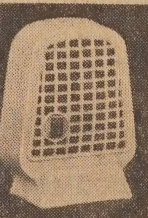
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Cost of Classified advertisements in this section is 2/- per line, approximately five words to a line. Closing date for October issue of Radio, Television and Hobbies is Wednesday, September 14.

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ORGANS (Electronic). Do you want to build an organ or other electronic musical instrument? Contact us for help. We have a complete range of books on the subject, and can supply any parts you may require. We are particularly interested in having your name and address for our mailing list. See also our advertisement on page 55. The Electronic Organ Company (Australia), 9-11 Cadow Street, Pymble, NSW.

SELL: All back issues R. & H. Many early copies in stock, 4/- per copy, incl. post. Write now to T. Weir, 73 Gibson Ave., Padstow, for prompt service. UY8056.

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